

Shear-Reinforced Concrete Breakout Failure



CCAPS Structures Engineering Webinar Series

02/20/2024

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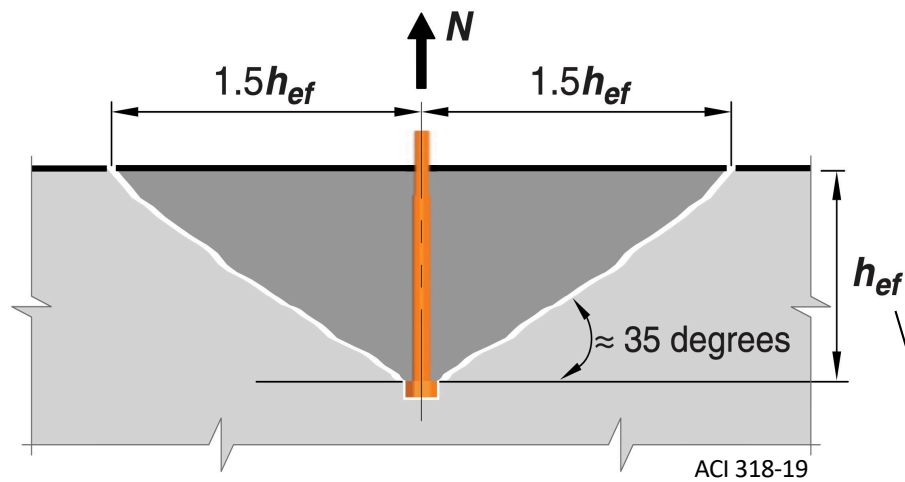
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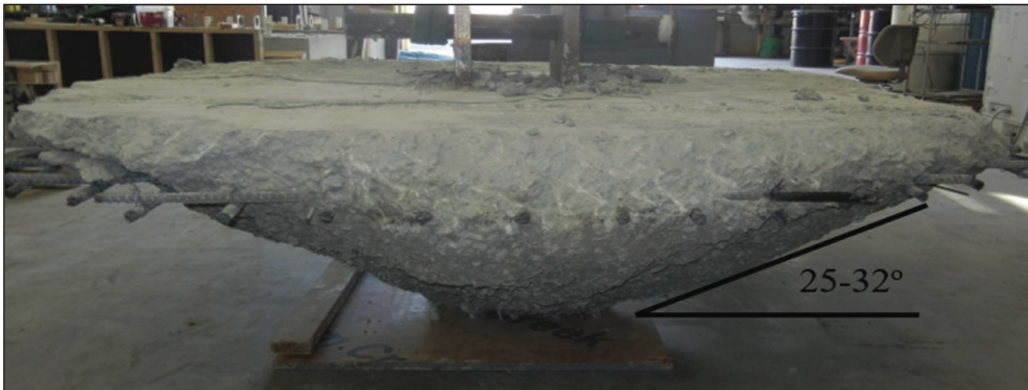
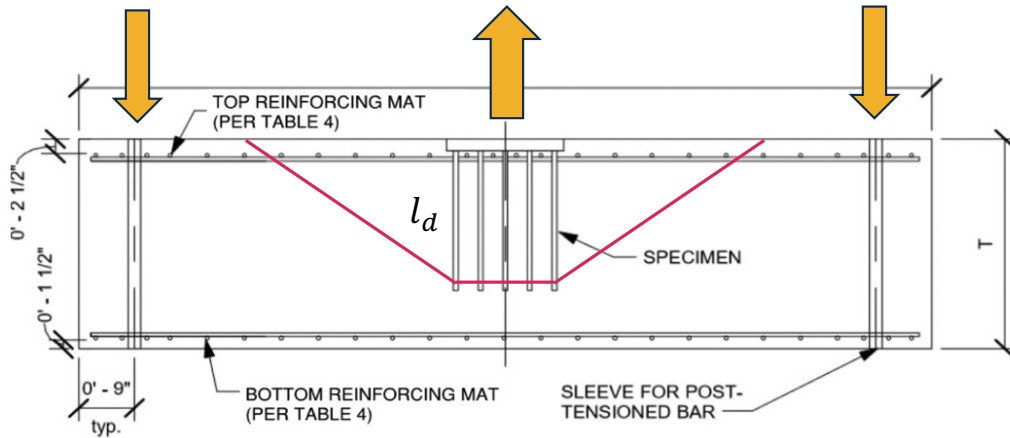
Concrete Breakout Failure Cone



Can breakout failure govern in large-scale connections? (groups of anchor or rebar)

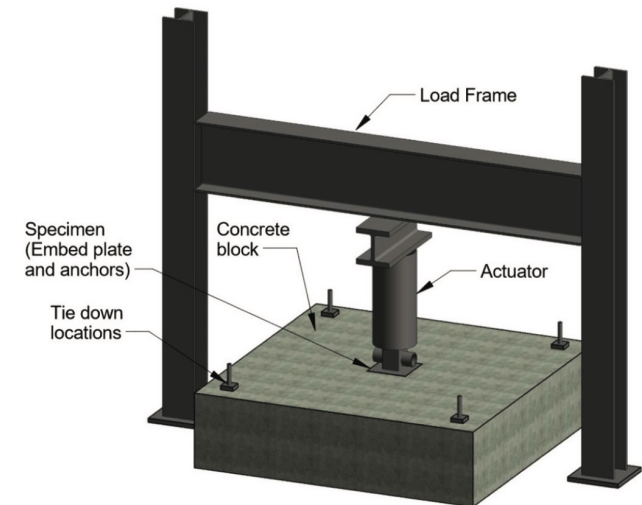
Effective depth

Premature Breakout Failure Examples



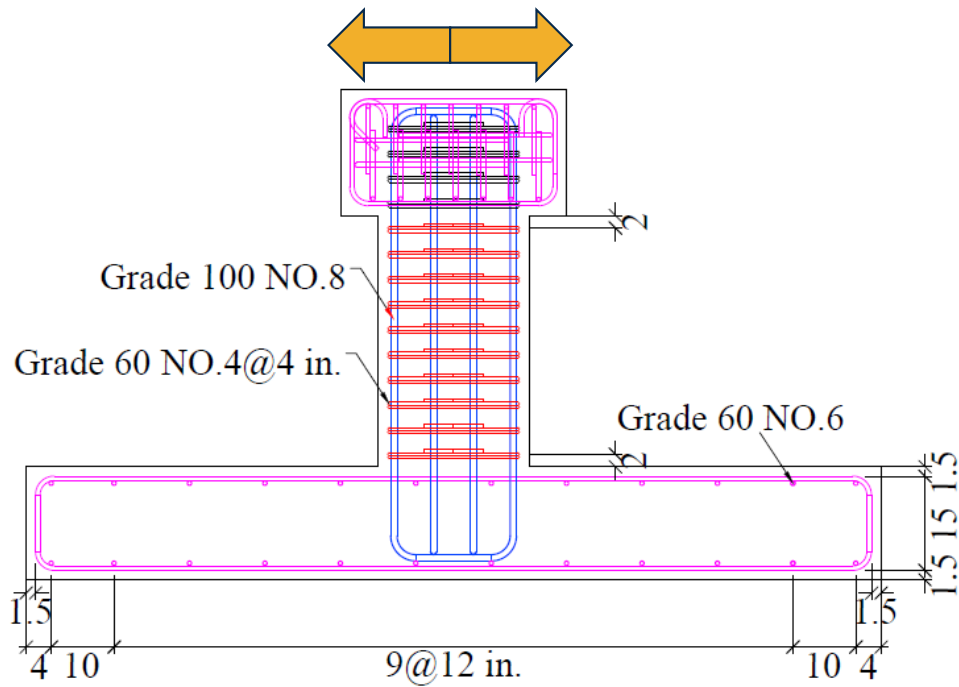
Chicchi et al. (2020)

- Purdue
- Groups of straight bars (up to 5x5 groups)
- 8 Specimens
- Developed length
- Breakout failure governed before nominal bar yield



Premature Breakout Failure Examples

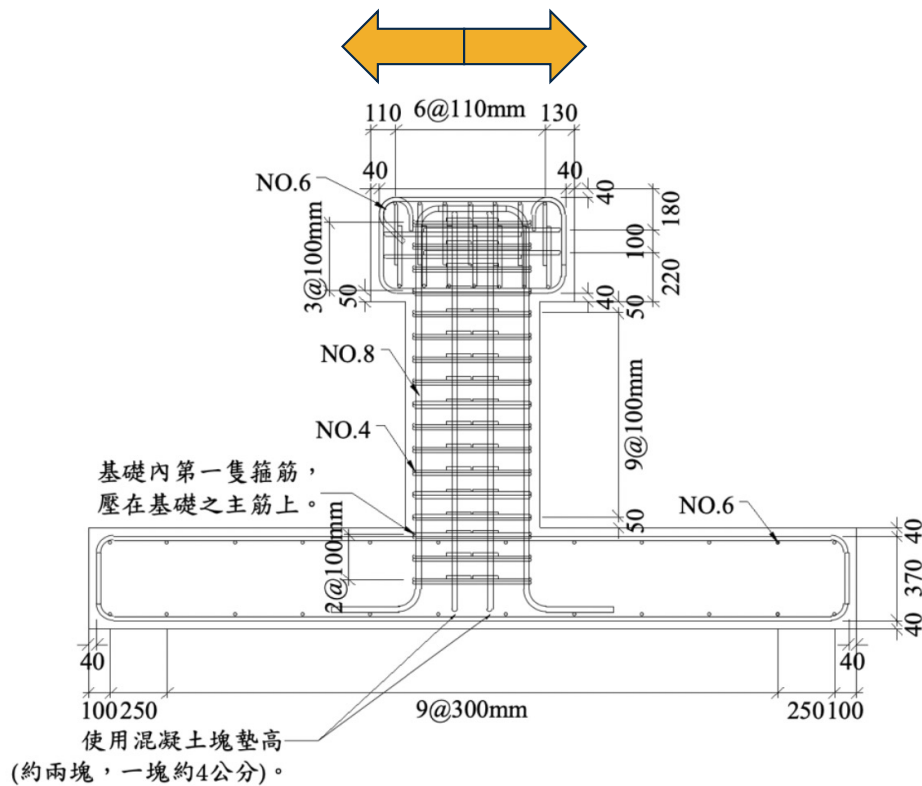
- Taiwan National University of Science and Technology
- Breakout before nominal bar yield



Chen (2021)

Premature Breakout Failure Examples

- Taiwan National University of Science and Technology
- Breakout before nominal bar yield



Chen (2021)

Observations from Physical Tests

1. Breakout failure can govern for large-scale connections even when development lengths are provided.

17.1.6 Reinforcement used as part of an embedment shall have development length established in accordance with other parts of this Code. If reinforcement is used as anchorage, concrete breakout failure shall be considered. Alternatively, anchor reinforcement in accordance with 17.5.2.1 shall be provided.

ACI 318-19

2. Breakout equations can be overly conservative.

- Example breakout strength specimen M01:

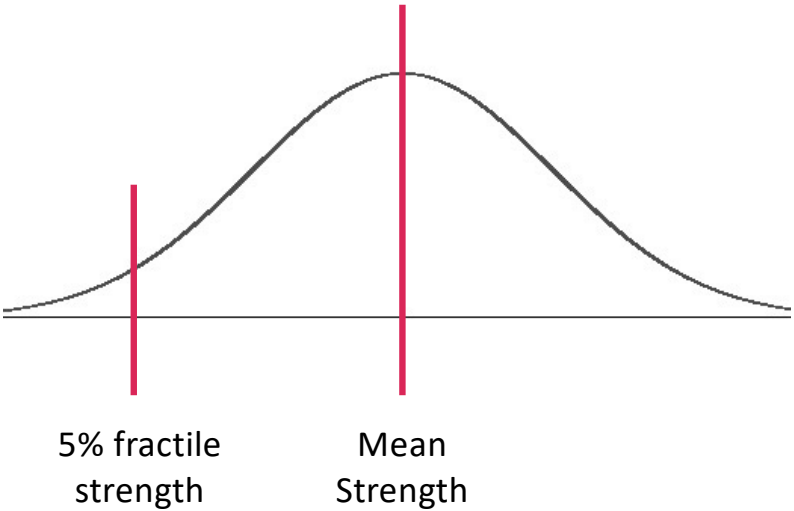
$$N_{test} = 253 \text{ kip}$$

$$\Phi N_{cbg} = 77 \text{ kip (cracked)}$$

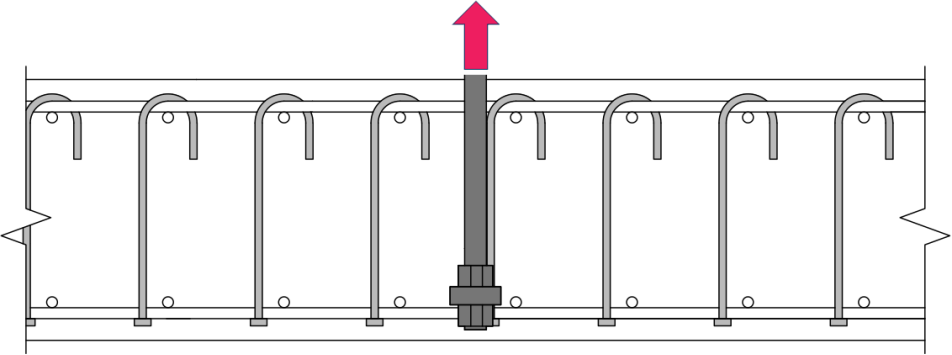
$$\frac{N_{test}}{\Phi N_{cbg}} = 3.3$$

Sources of Breakout Conservatism

1. 5% Fractile Strength



2. Reinforcement ignored



ACI 318 Anchor Reinforcement

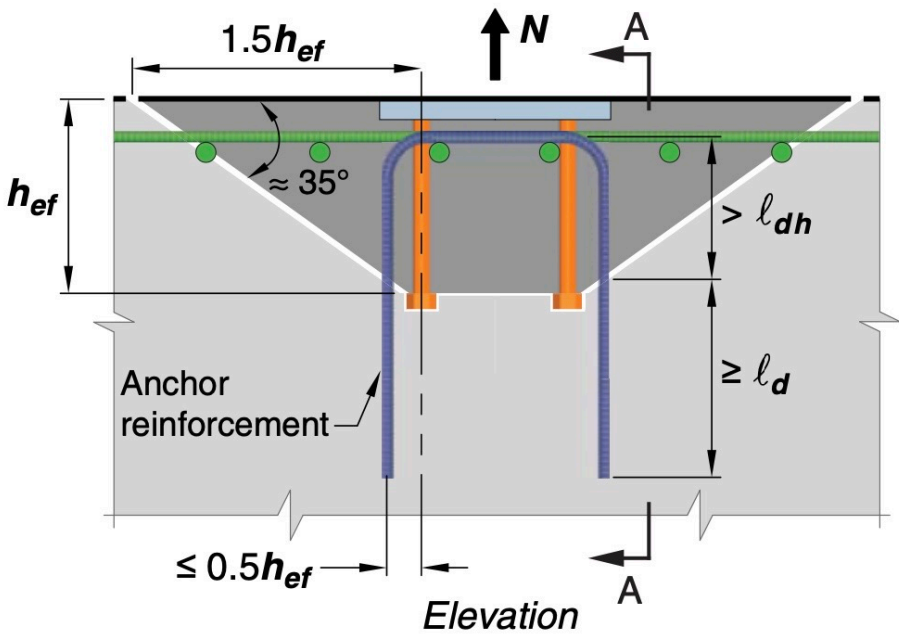


Fig. R17.5.2.1a—Anchor reinforcement for tension.

Concrete strength is ignored

Shear-Reinforced Breakout (SRB)

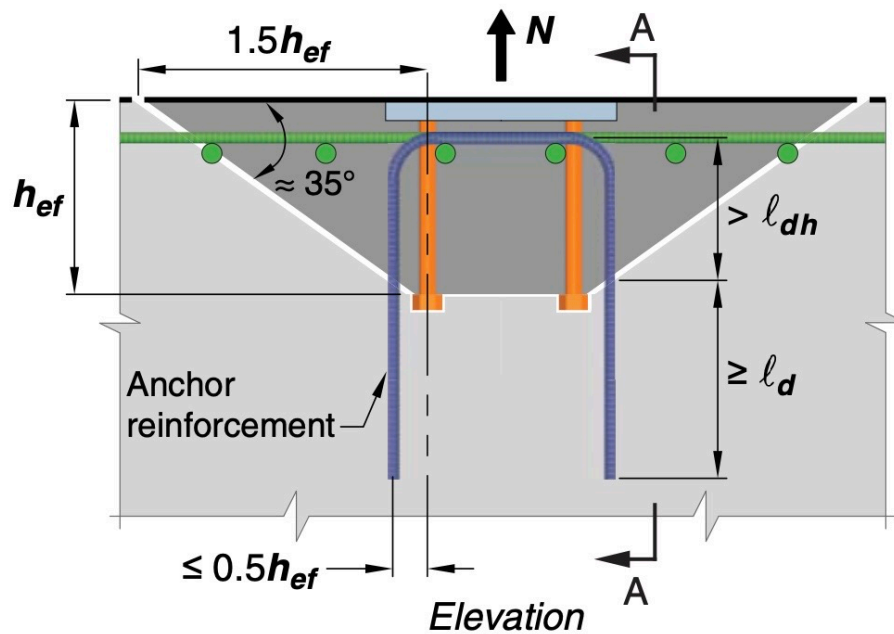


Fig. R17.5.2.1a—Anchor reinforcement for tension.

$$N_{n,SRB} = N_c + N_s ?$$

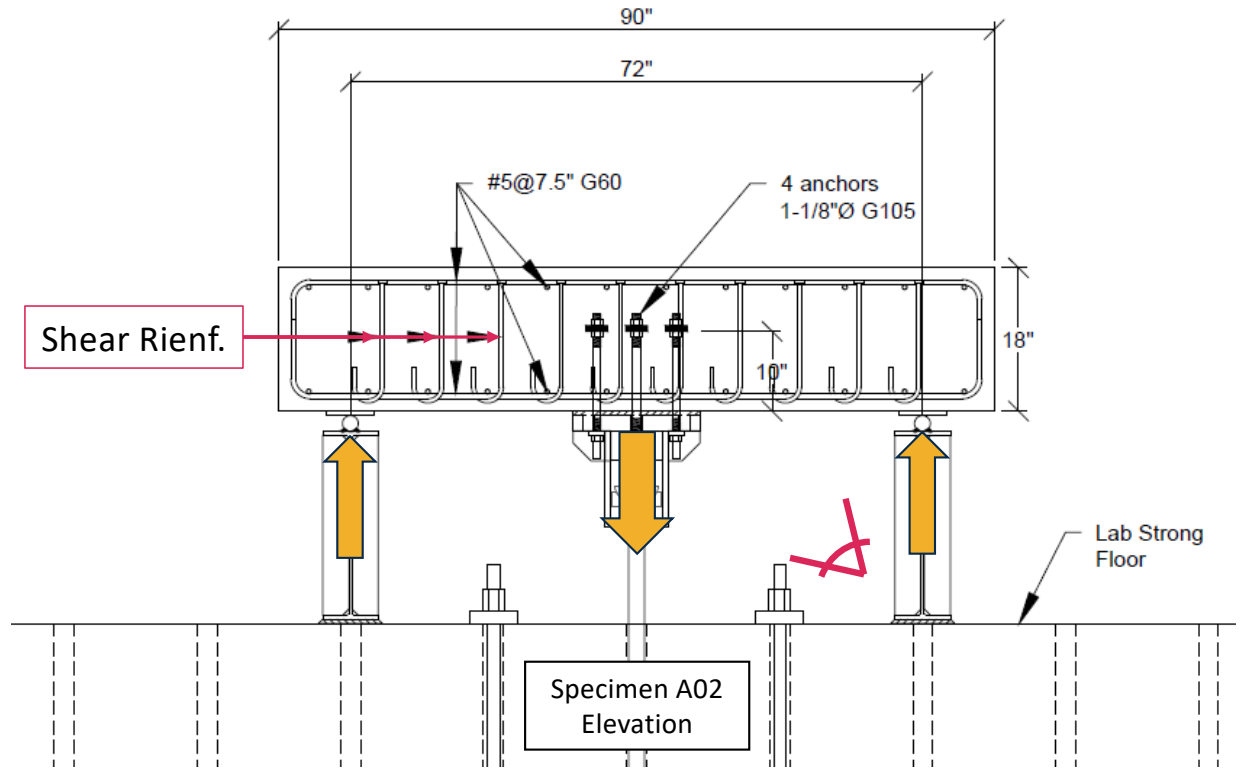
Question:

- Detailing requirements?
- Size of reinforced region?
- Upper limits to steel strength?

Shear-Reinforced Breakout Tests

- UC Berkeley
- Four monotonic axial loading tests
- Breakout failures for all specimens
- Longitudinal bars did not appear to yield

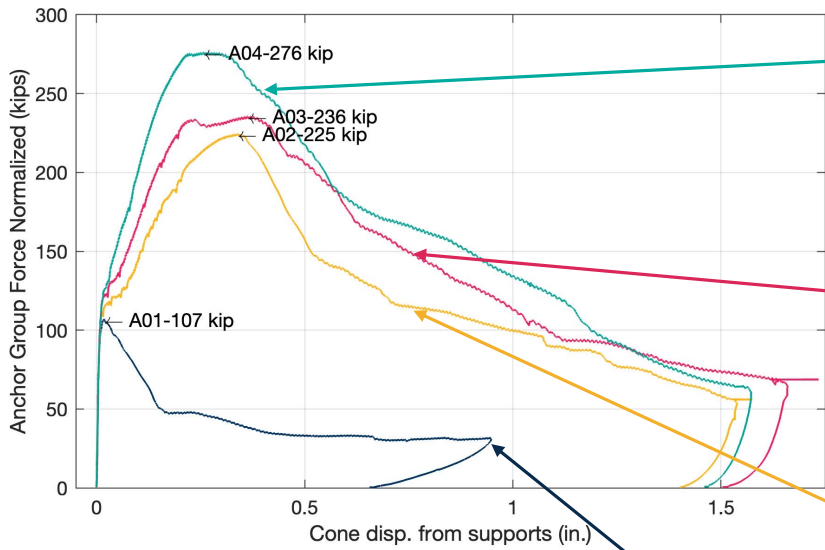
Specimen	Shear Reinforcement	Reinforcing ratio, ρ_{tr} (%)
A01	N/A	0
A02	#4@7.5in.	0.36%
A03	#5@7.5in.	0.55%
A04	#4@6in.	0.56%



Karać (2022)

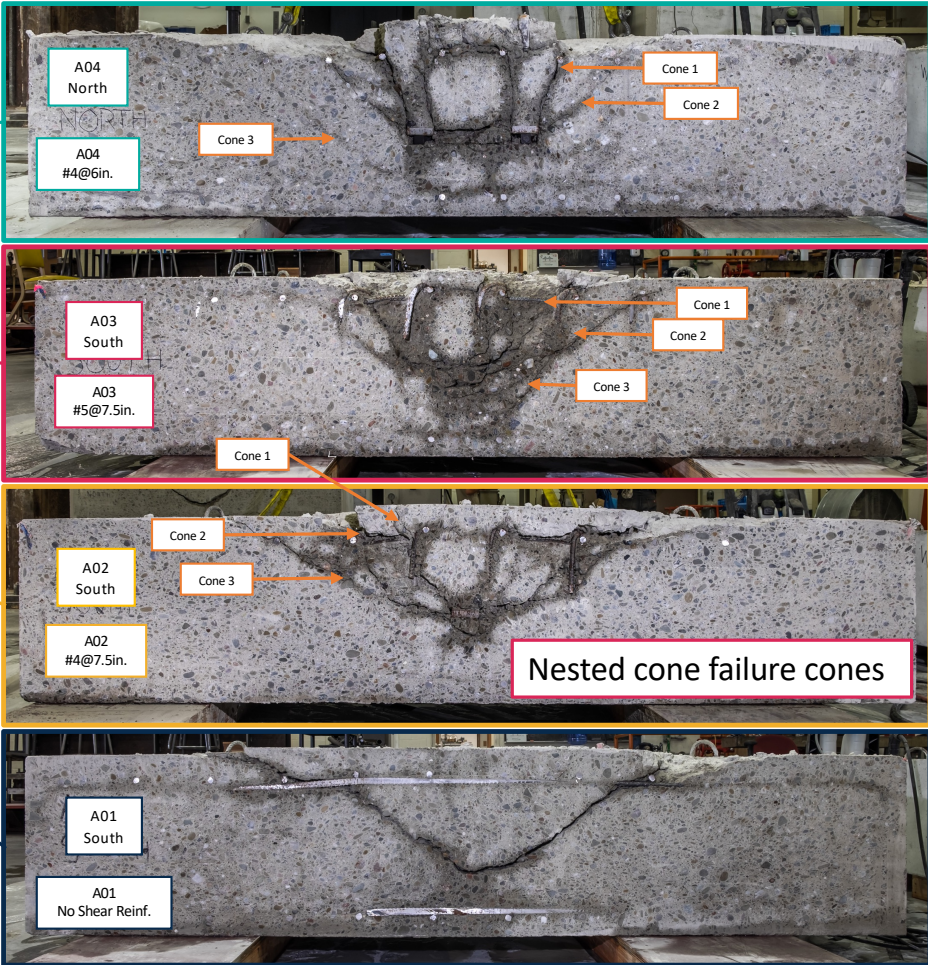


Shear-Reinforced Breakout Tests



Increased

- Peak strength
- Displacement capacity

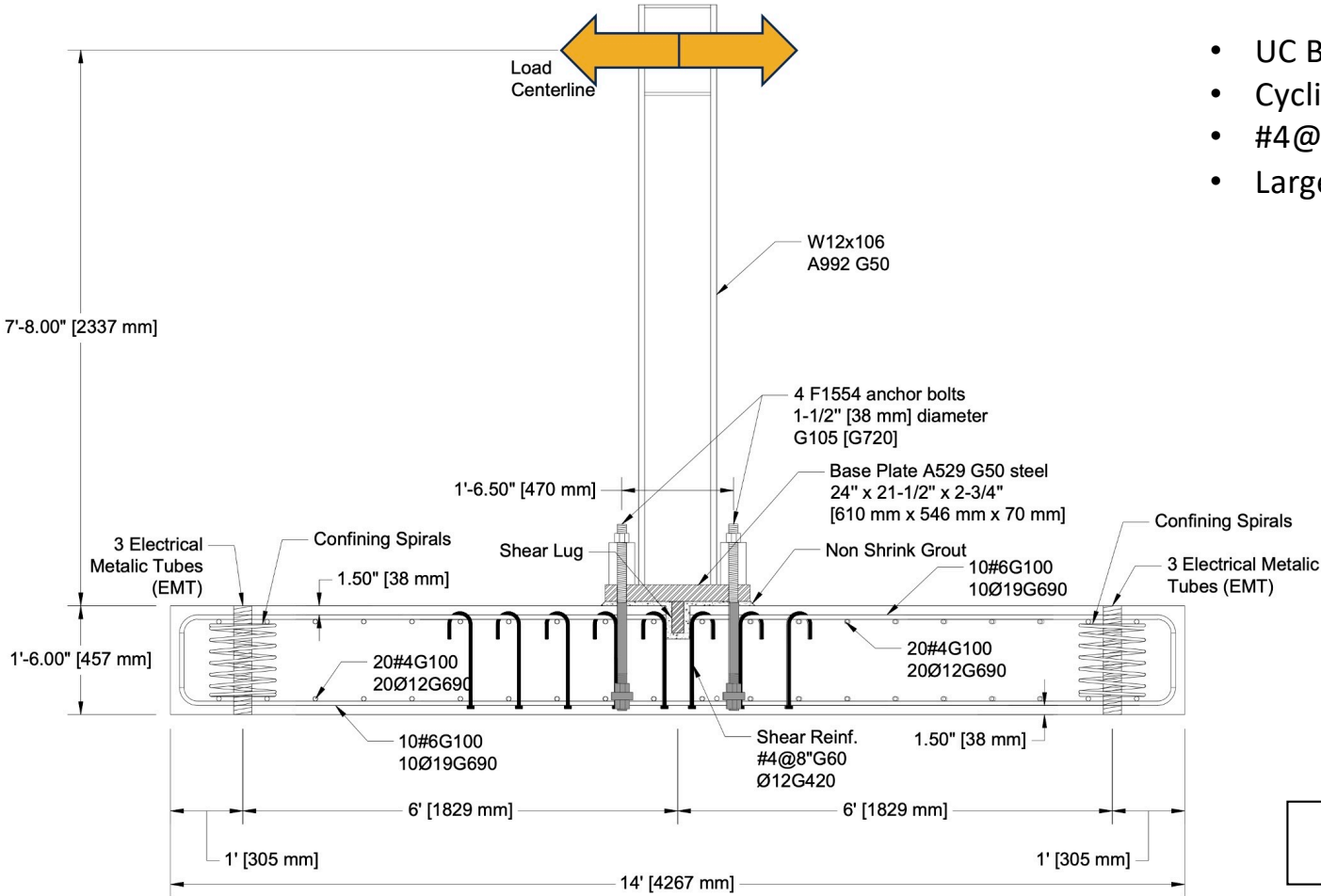


Nested cone failure cones

Karać (2022)

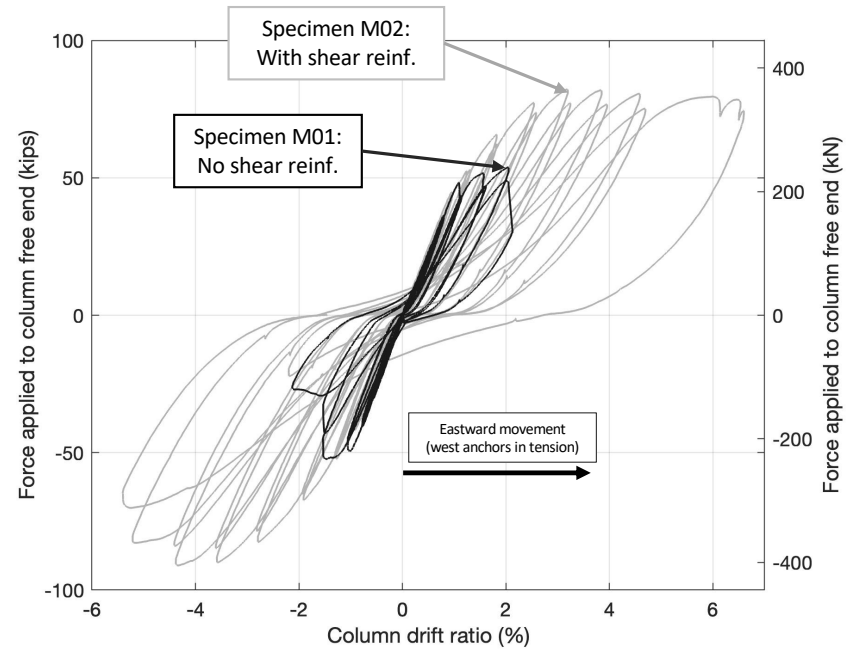
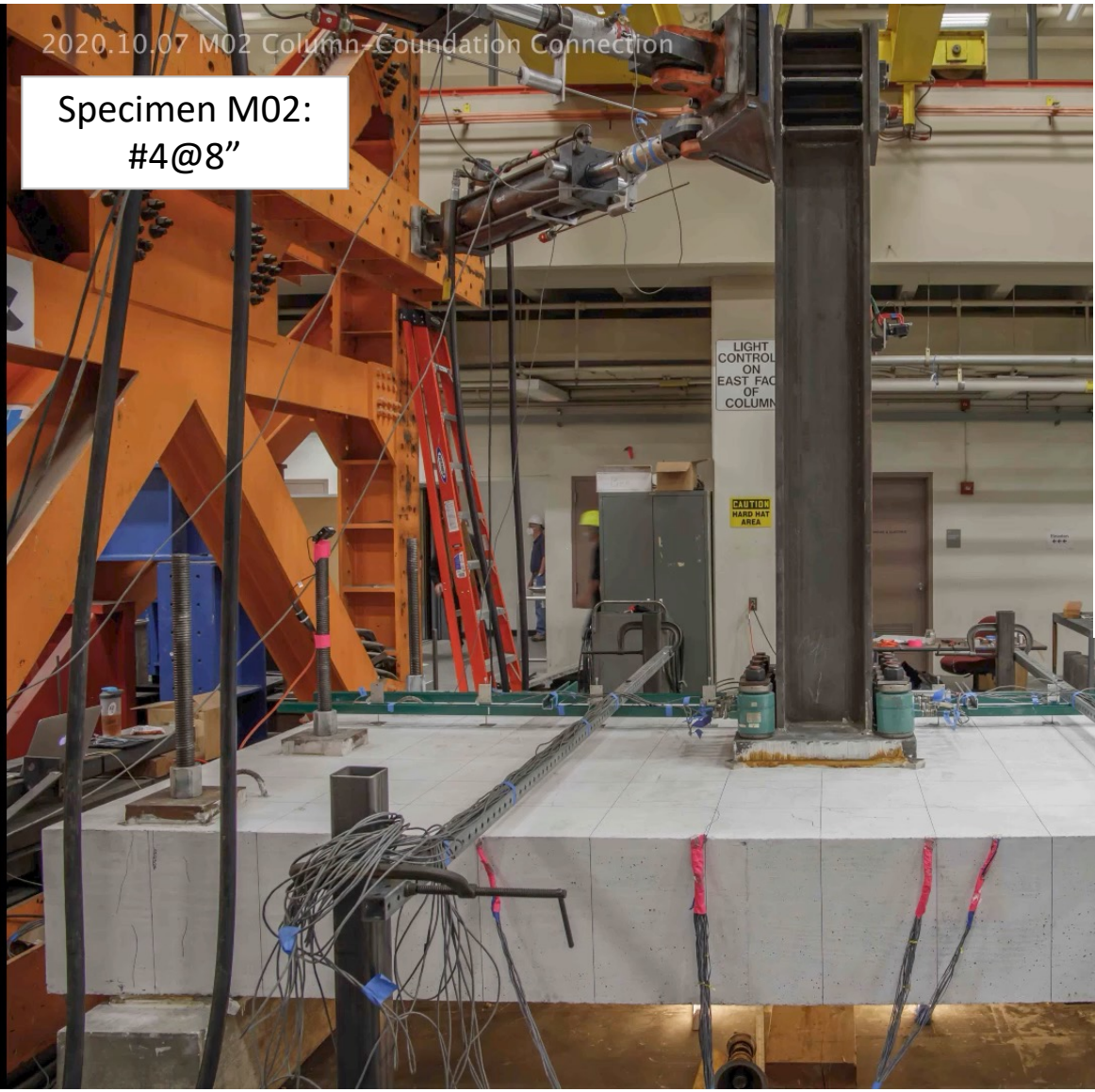
Shear-Reinforced Breakout Tests

- UC Berkeley
- Cyclic loading
- #4@8" G60
- Larger reinforced region on one side



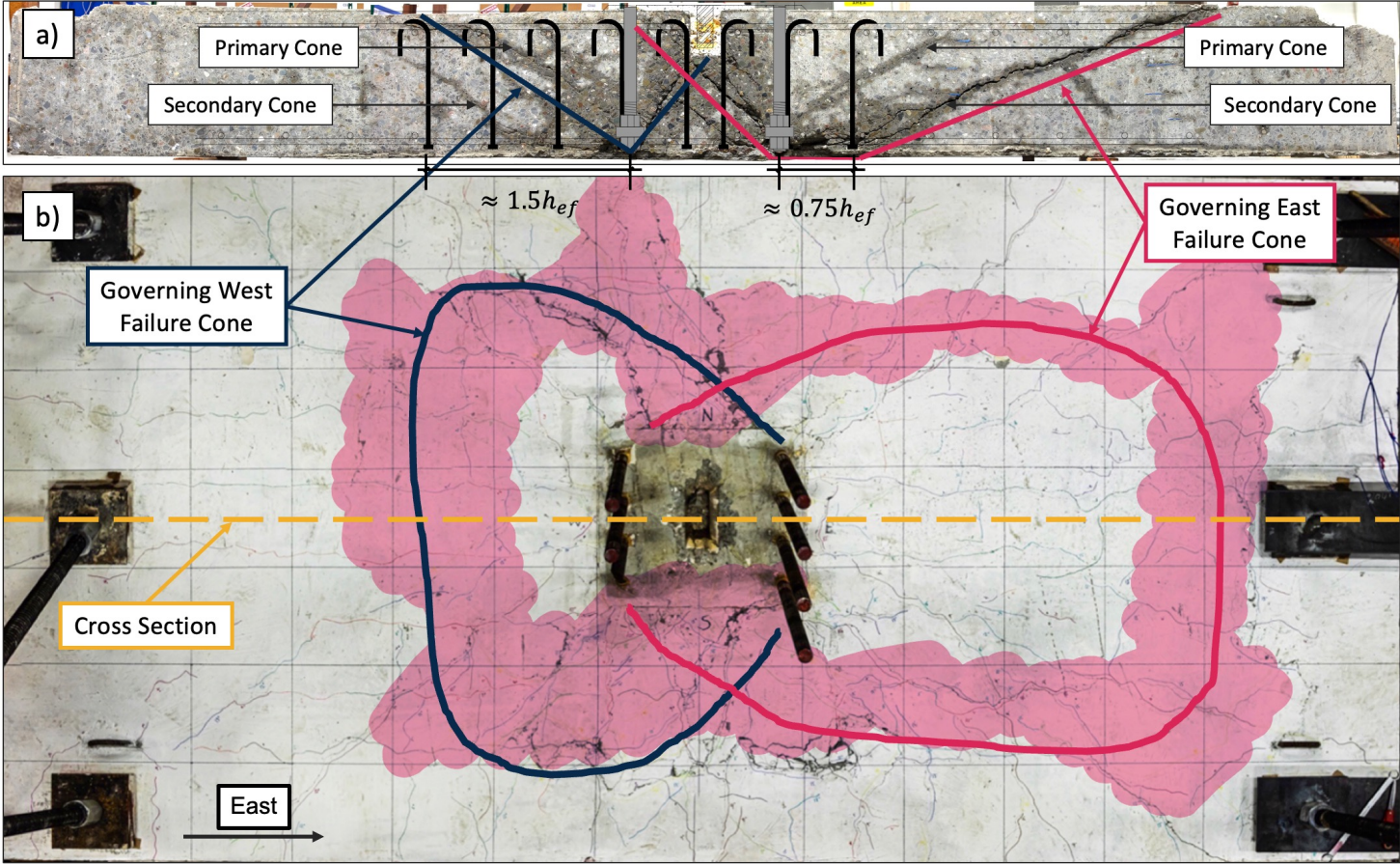
2020.10.07 M02 Column-Column Connection

Specimen M02:
#4@8"

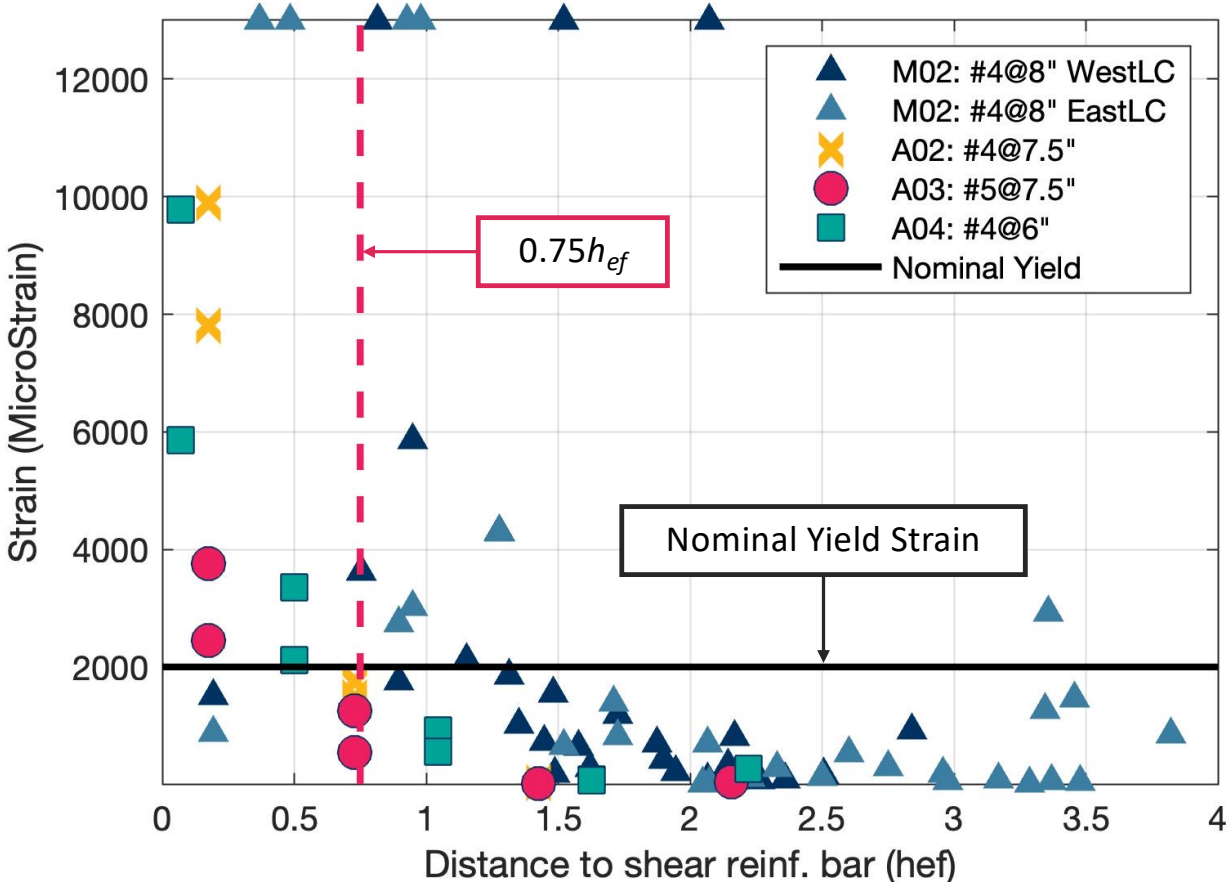


Cycle 1
 $\delta = 0.14$ in

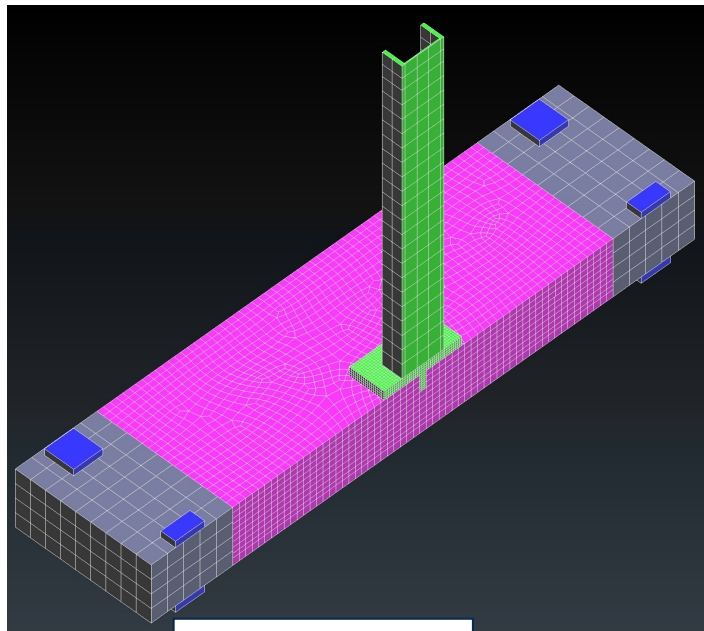
Shear-Reinforced Breakout Tests



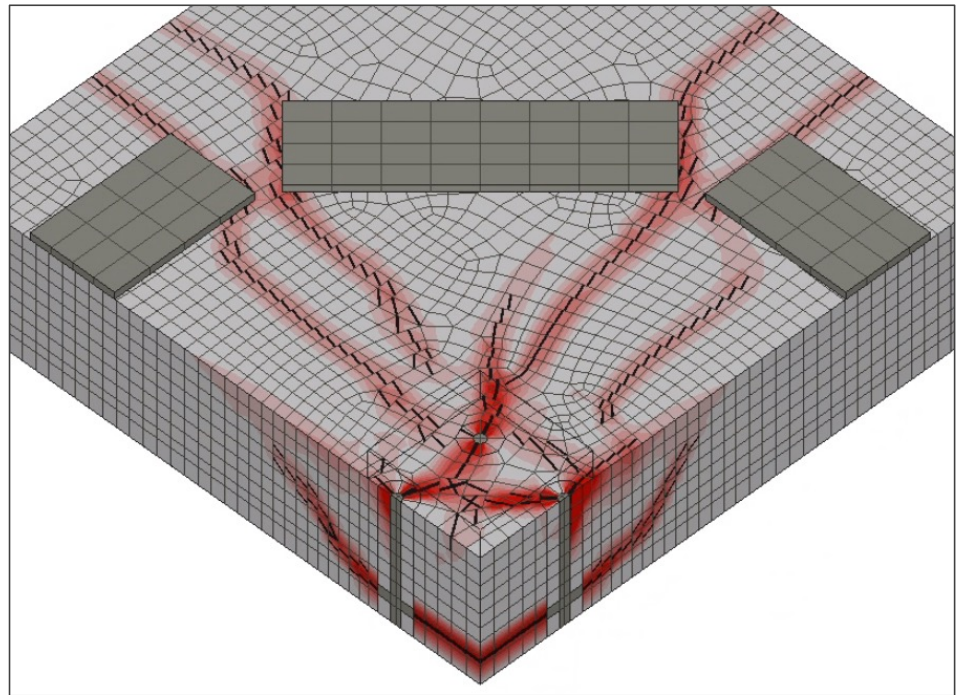
Shear Bar Strains



Finite Element Studies



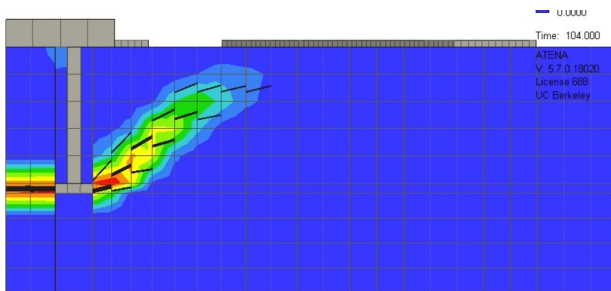
M01 Model



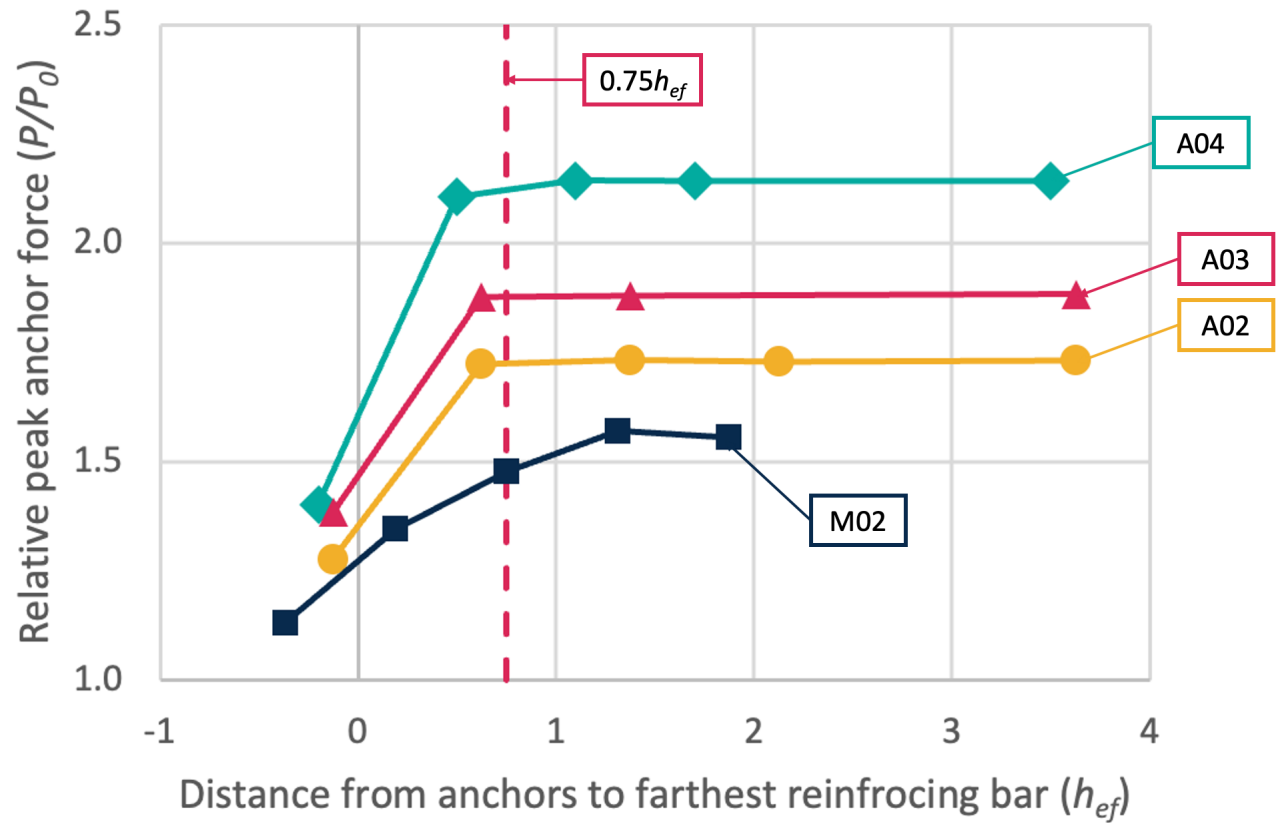
FE Crack Pattern

Finite Element Studies: shear-reinforced region

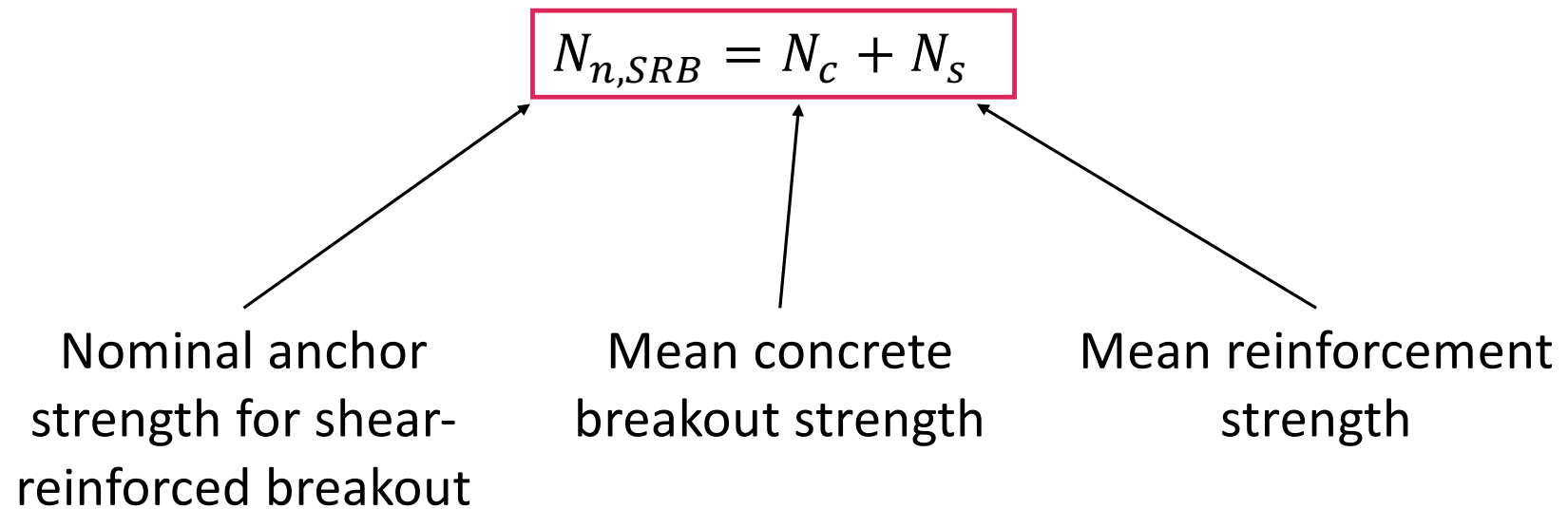
- Shear reinforcing beyond about $0.75h_{ef}$ does not seem to increase peak strength



FE Crack Pattern



New Shear-Reinforced Breakout (SRB) Design Equation (ACI 318-25)



Shear-Reinforced Breakout (SRB) Design Equation

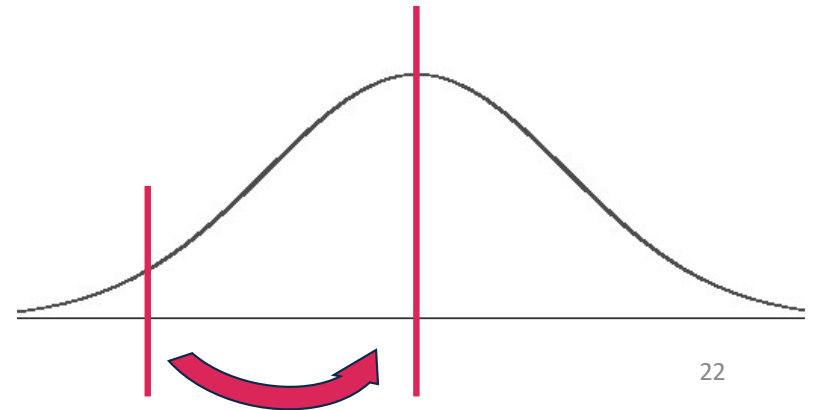
$$N_c = 1.33N_{cbg}$$

Mean concrete
breakout strength

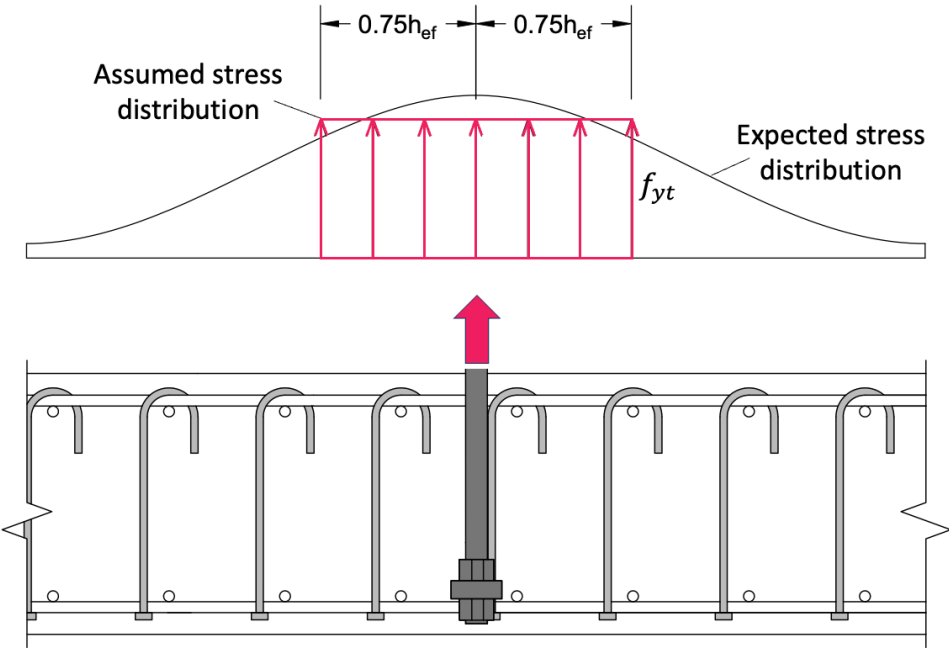
5% fractile strength
ACI 318-19 Chap. 17

$$\frac{1}{1 + z_{0.05} * CV} = \frac{1}{1 + (-1.645) * 0.15} = 1.33$$

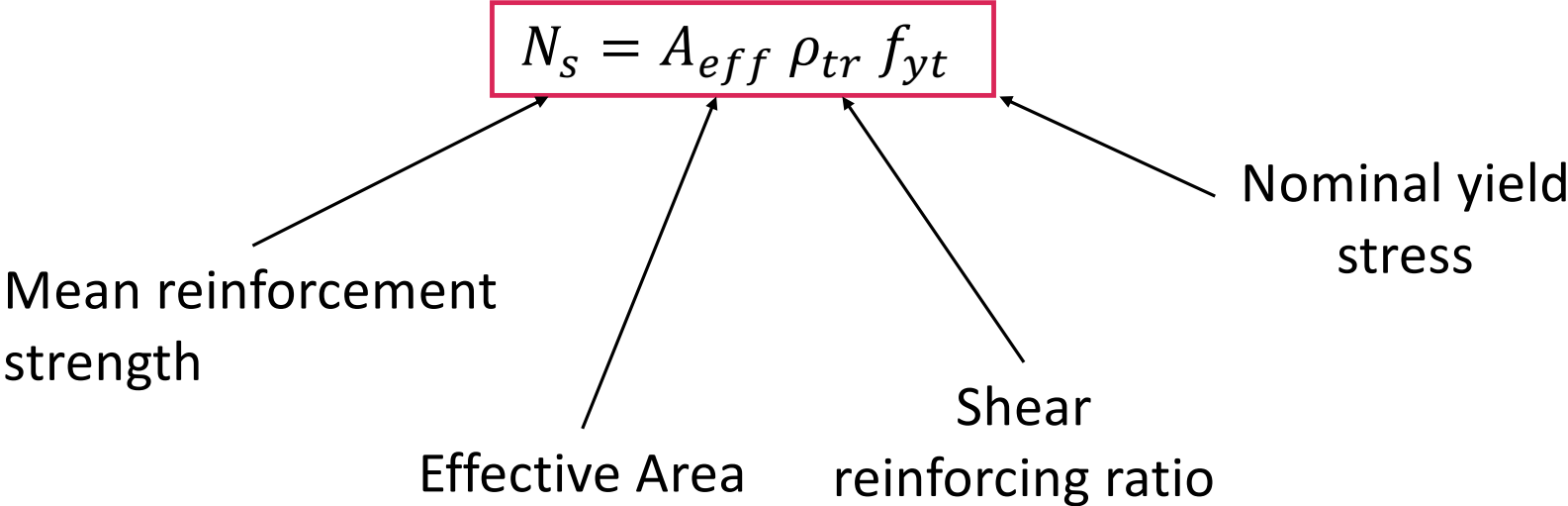
Fuchs (1995)



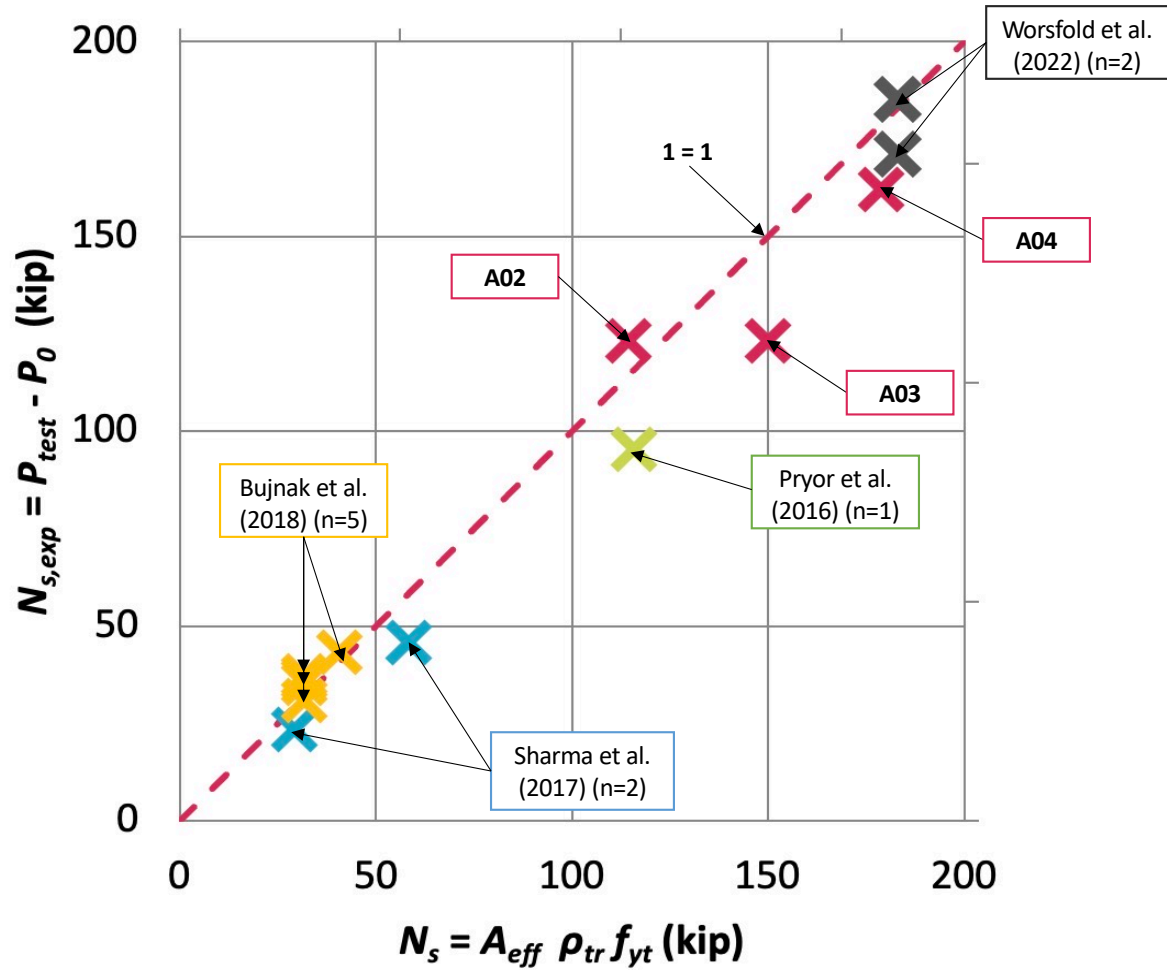
Shear-Reinforced Breakout (SRB) Design Equation



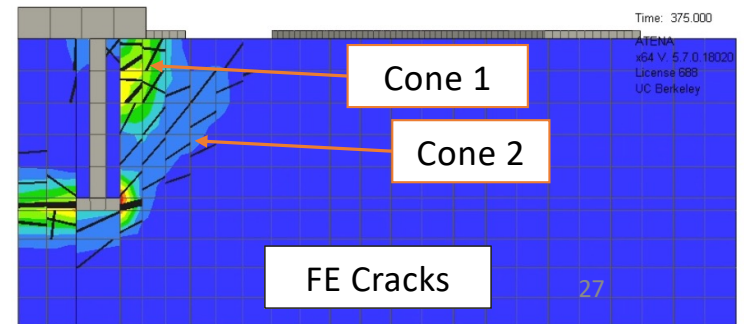
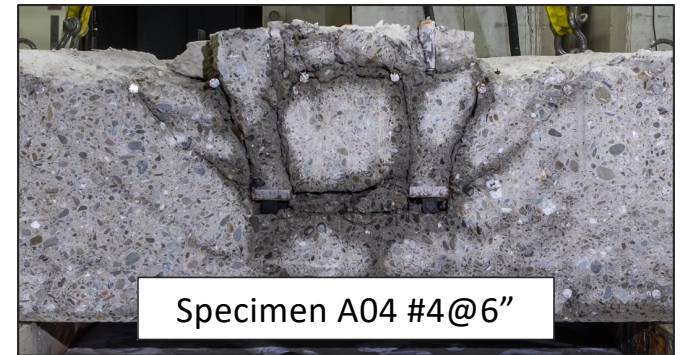
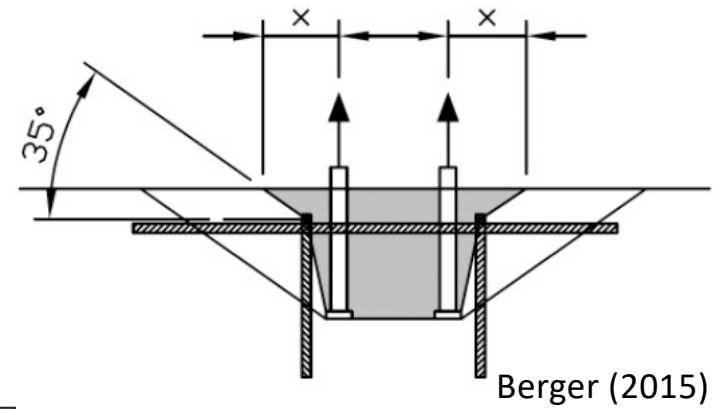
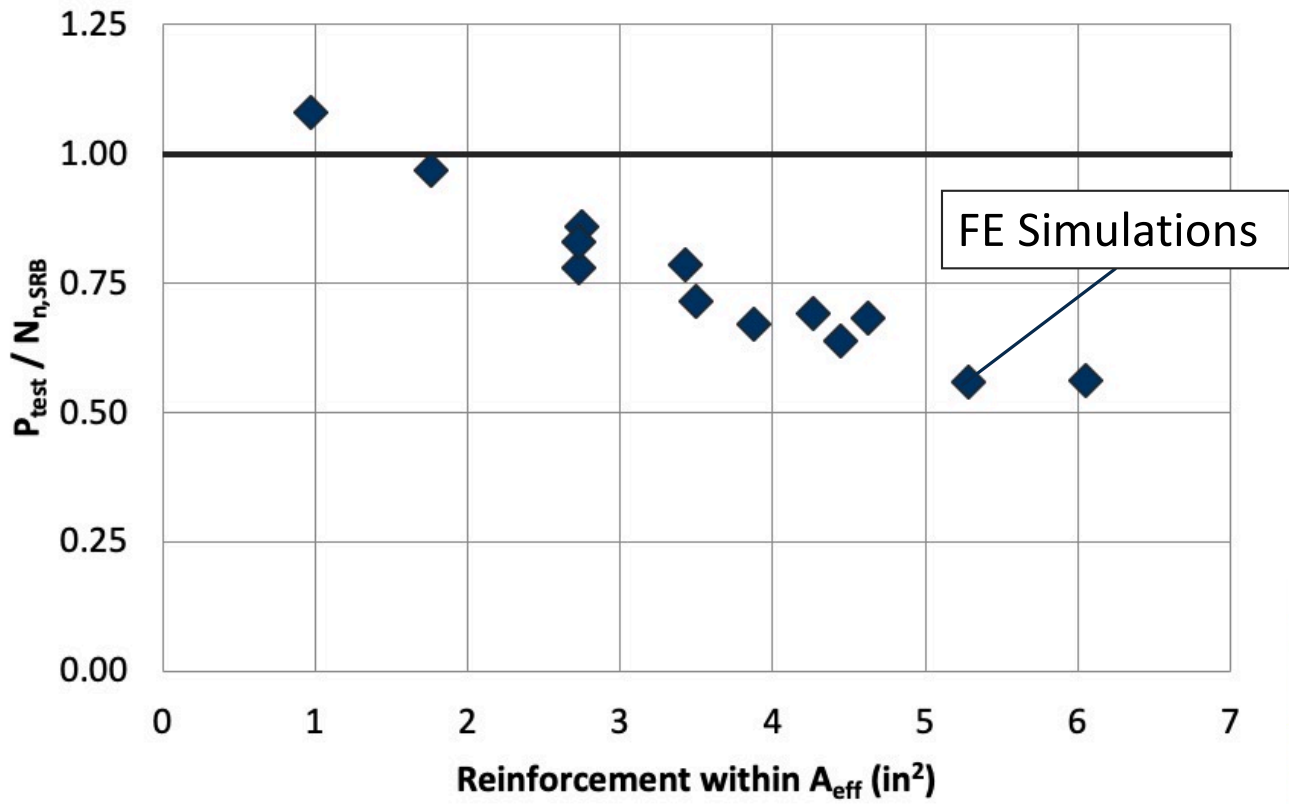
Shear-Reinforced Breakout Design Equation



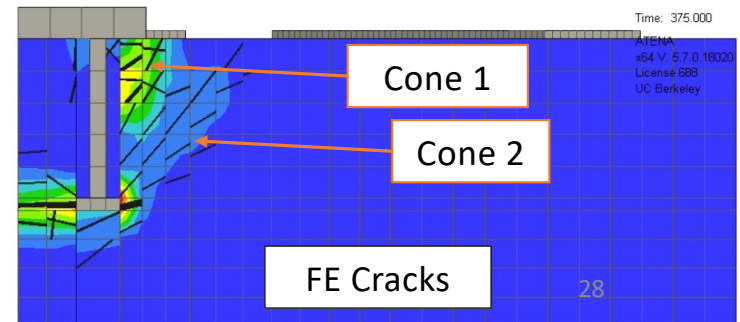
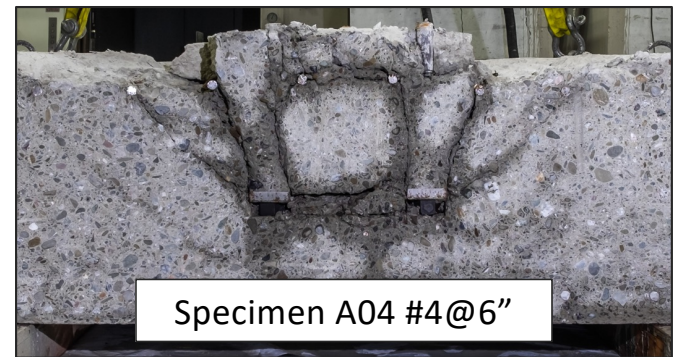
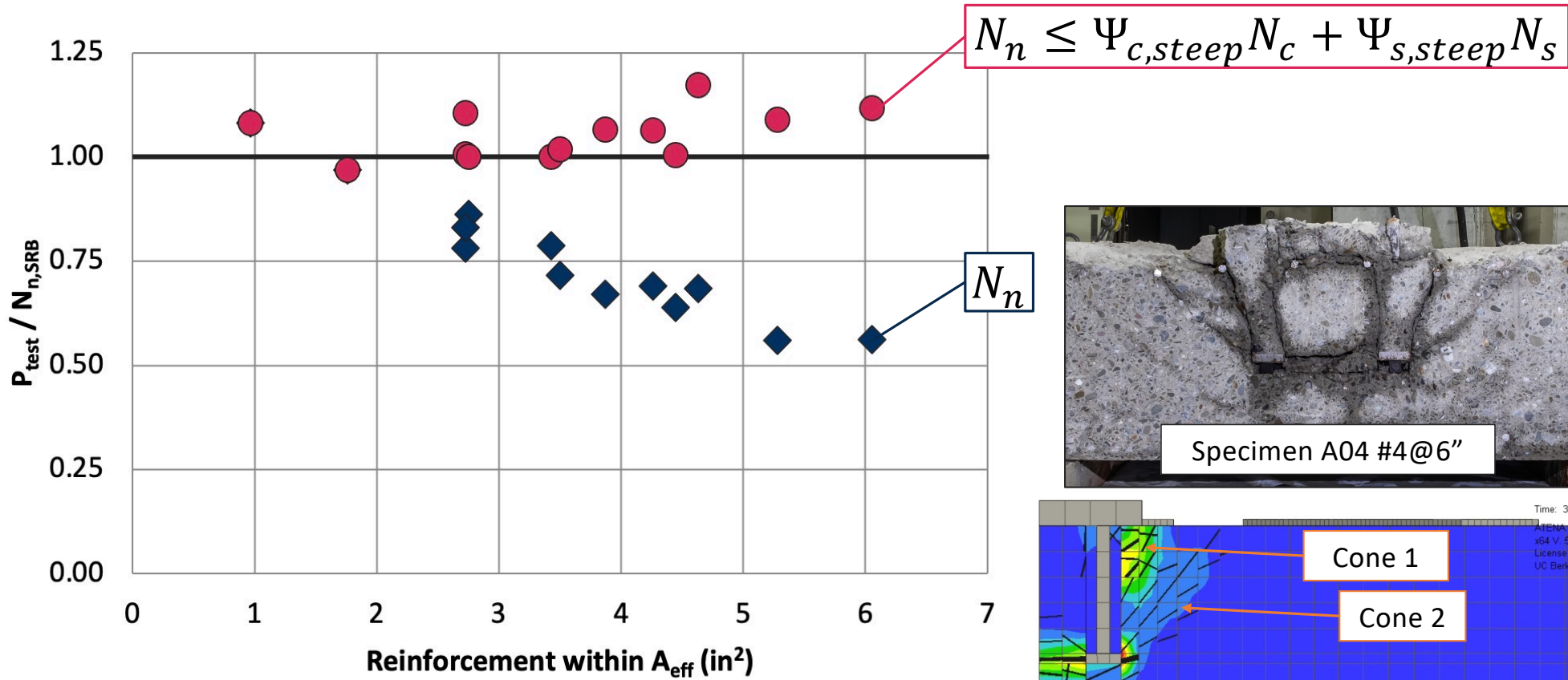
Shear-Reinforced Breakout Design Equation



Upper Limit: Steep Cone Strength



Upper Limit: Steep Cone Strength



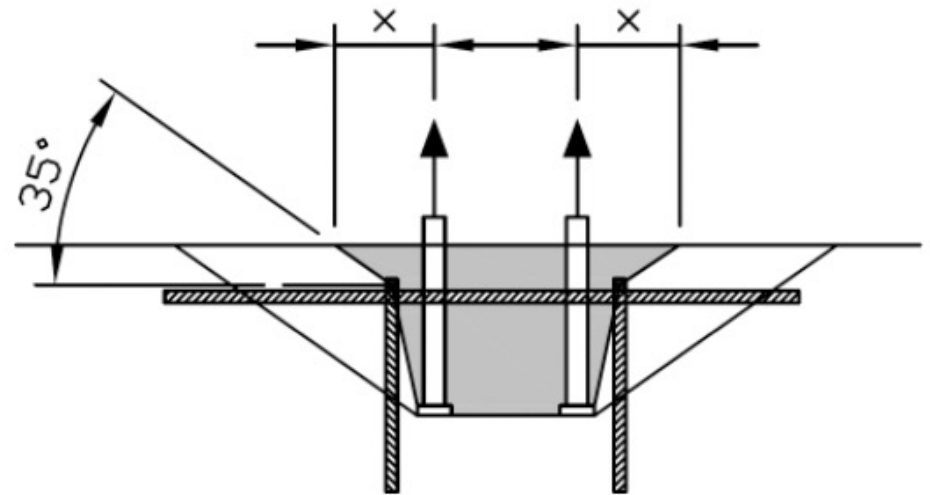
Upper Limit: Steep Cone Strength

- Considered indirectly in ACI implementation

$$N_{n,max} = \Psi_{c,steep} N_c + \Psi_{s,steep} N_s$$

$$\Psi_{c,steep} = 2.75 - 1.75 \frac{A'}{A_{Nc}} \geq 1$$

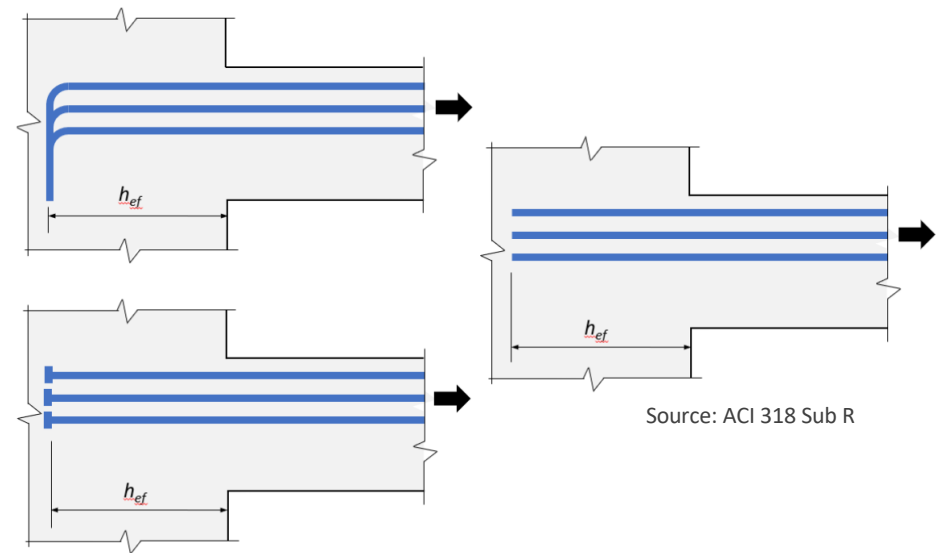
$$\Psi_{s,steep} = 2 \frac{A'}{A_{Nc}} - 1 \geq 0$$



Berger (2015)

ACI 318-25 New Design Equation

- New provisions require breakout failure checks at the termination of groups of straight, hooked, or headed bars.
- Beam-column joints exempt



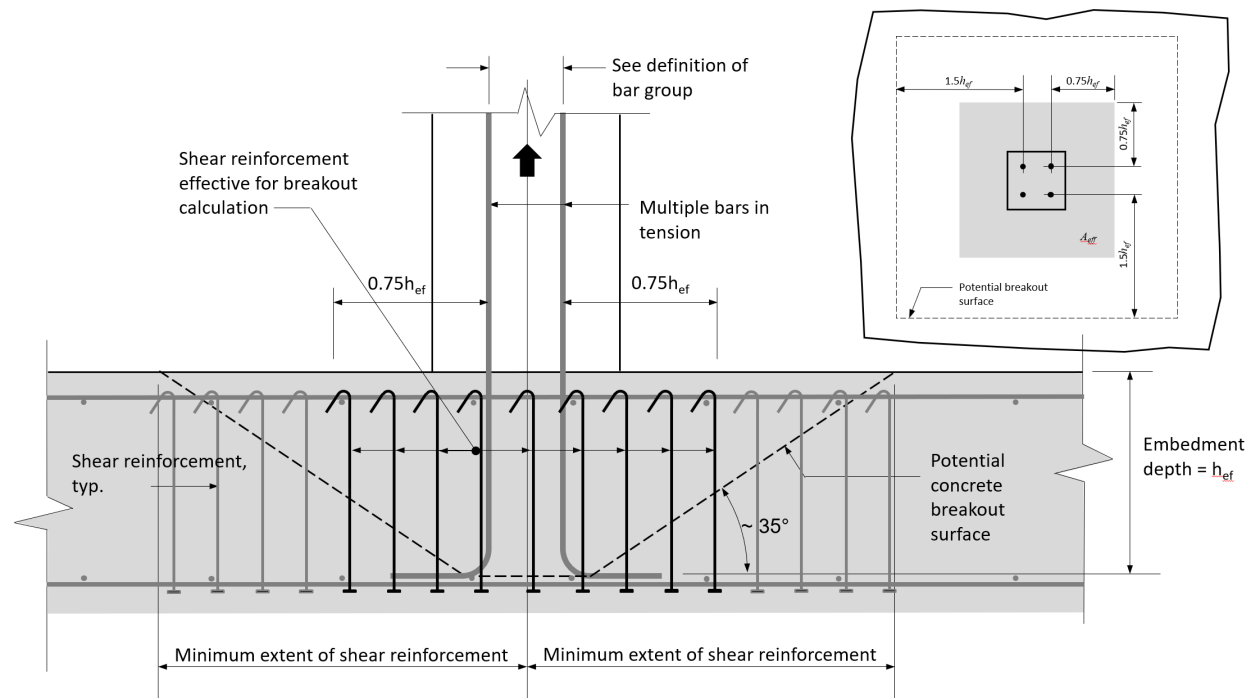
Code Implementation: Detailing Requirements

1. Shear reinforcement shall be parallel to bar group
2. Shear reinforcement shall terminate in hooks or heads beyond the termination of the bar group satisfying the requirements for stirrups in 25.7.1.3
3. Shear reinforcement bar diameter shall not exceed the diameter of the smallest bar in the bar group
4. Shear reinforced region extends at least throughout projected cone region
5. Maximum bar spacing

$$s_{max} = 0.5h_{ef}$$

If $N_{n,SRB} \geq 2.5N_c$

$$s_{max} = 0.25h_{ef}$$



ACI 318 Anchor Reinforcement

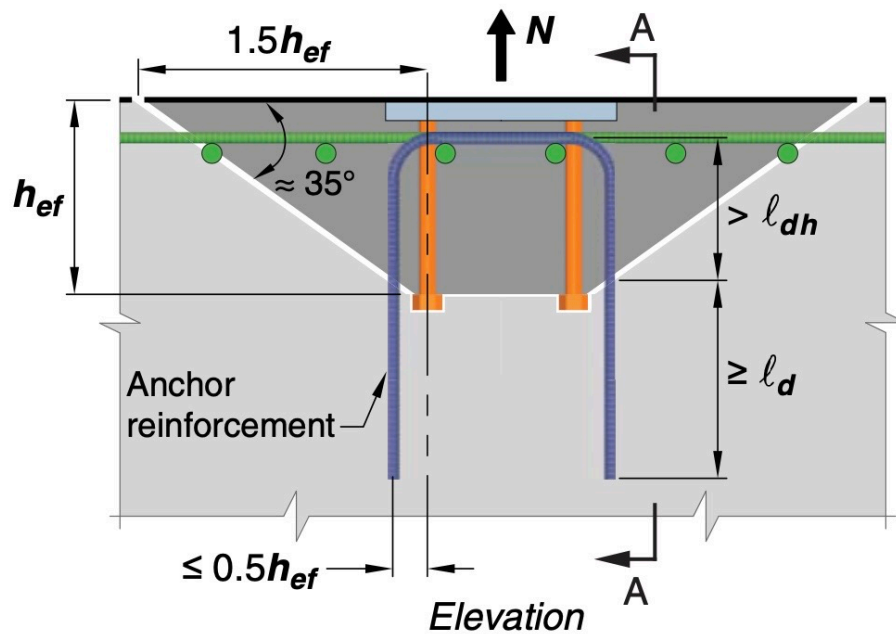


Fig. R17.5.2.1a—Anchor reinforcement for tension.

- Anchor Reinforcement is still an allowable solution
- Concrete strength is ignored

Publications

ACI STRUCTURAL JOURNAL TECHNICAL PAPER

Title No. 119-S104

Moment Transfer at Column-Foundation Connections: Physical Tests

by Benjamin L. Worsfold, Jack P. Moehle, and John F. Silva

ACI STRUCTURAL JOURNAL TECHNICAL PAPER

Title No. 120-S39

Moment Transfer at Column-Foundation Connections: Analytical Studies

by Benjamin L. Worsfold and Jack P. Moehle



Wason Medal Most Meritorious Paper (2023)

Engineering Structures 283 (2023) 115783

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Shear-reinforced concrete breakout design methodology for moment transfer at column-foundation connections

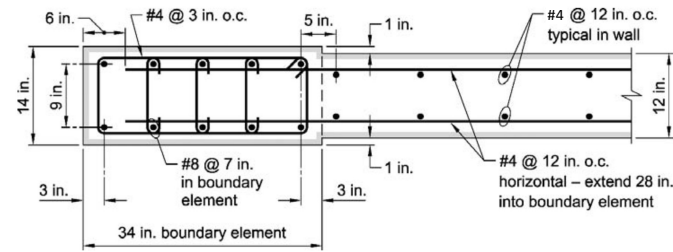
Benjamin L. Worsfold ^{a,*}, Jack P. Moehle ^b

Shear-Reinforced Concrete Breakout Failure in Axially Loaded Anchor Groups by Benjamin Worsfold, Dara Karać, and Jack Moehle



Example: Boundary element to thin foundation

Potential exists for concrete breakout failure even if the bars are placed $1.25l_{dt}$ into the foundation



SP-17(14) Design Handbook
SDC D
Special Structural Wall
 $f'_c = 5000\text{psi}$
 $f_y = 60\text{ksi}$

Nominal yield strength:

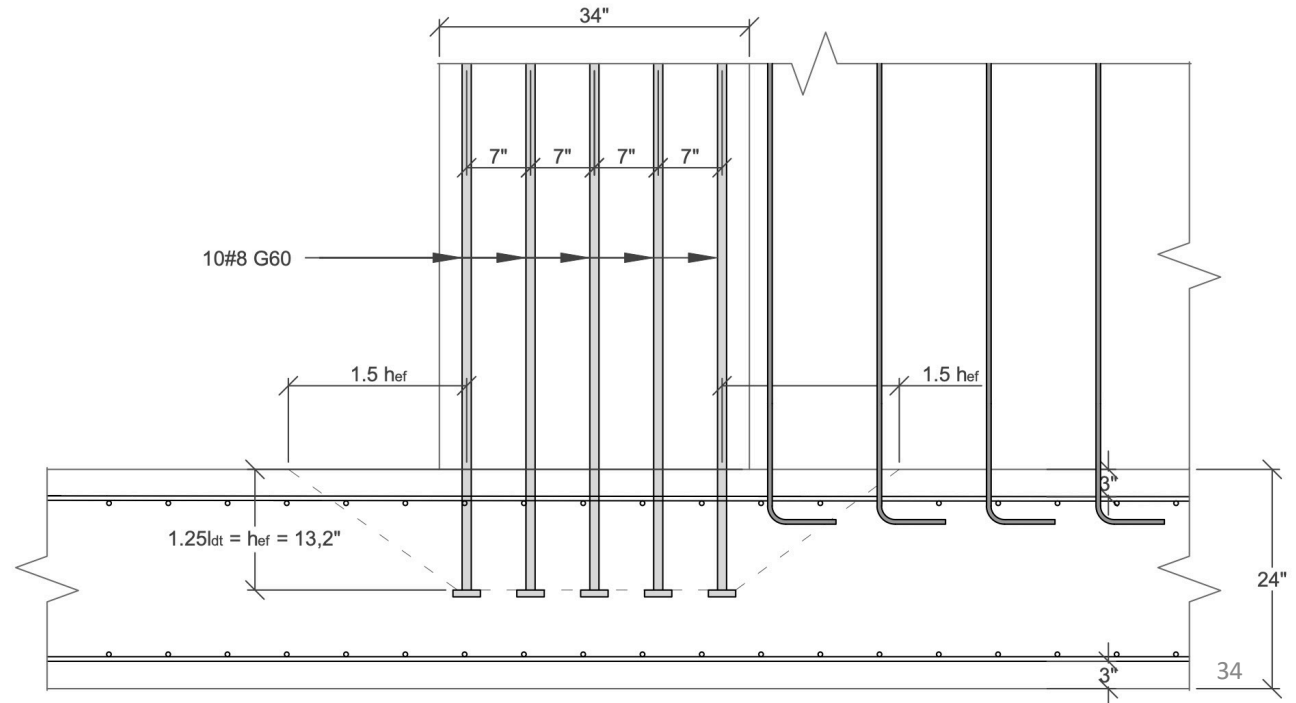
$$T_y = 474 \text{ kips}$$

Mean breakout strength:

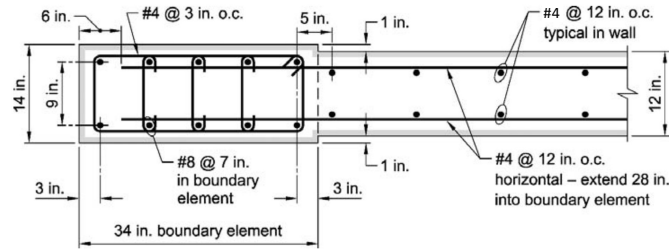
$$N_c = 284 \text{ kips}$$

Difference:

$$T_y - N_c = 190 \text{ kips}$$



Example: Boundary element to thin foundation



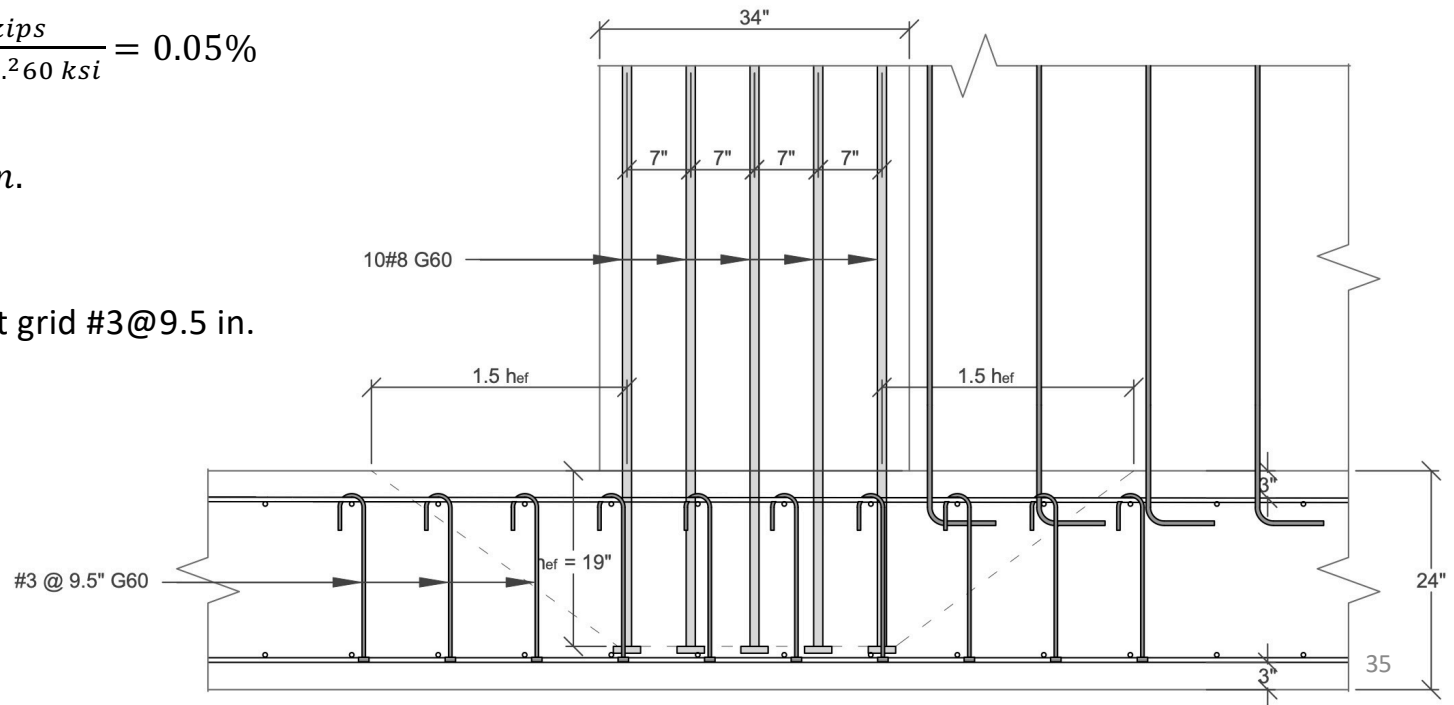
SP-17(14)
 SDC D
 Special Structural Wall
 $f'_c = 5000\text{psi}$
 $f_y = 60\text{ksi}$

$$\rho_{tr,min} = \frac{N_s}{A_{eff}f_{yt}} = \frac{70\text{kips}}{1377\text{ in.}^2 \cdot 60\text{ ksi}} = 0.05\%$$

$$s_{max} = \frac{h_{ef}}{2} = \frac{19\text{in.}}{2} = 9.5\text{in.}$$

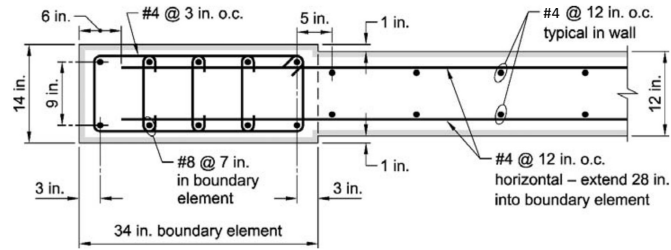
Select shear reinforcement grid #3@9.5 in.

$$\rho_{tr} = 0.12\%$$



Example: Boundary element to thin foundation

Boundary element
 $1.25f_y$



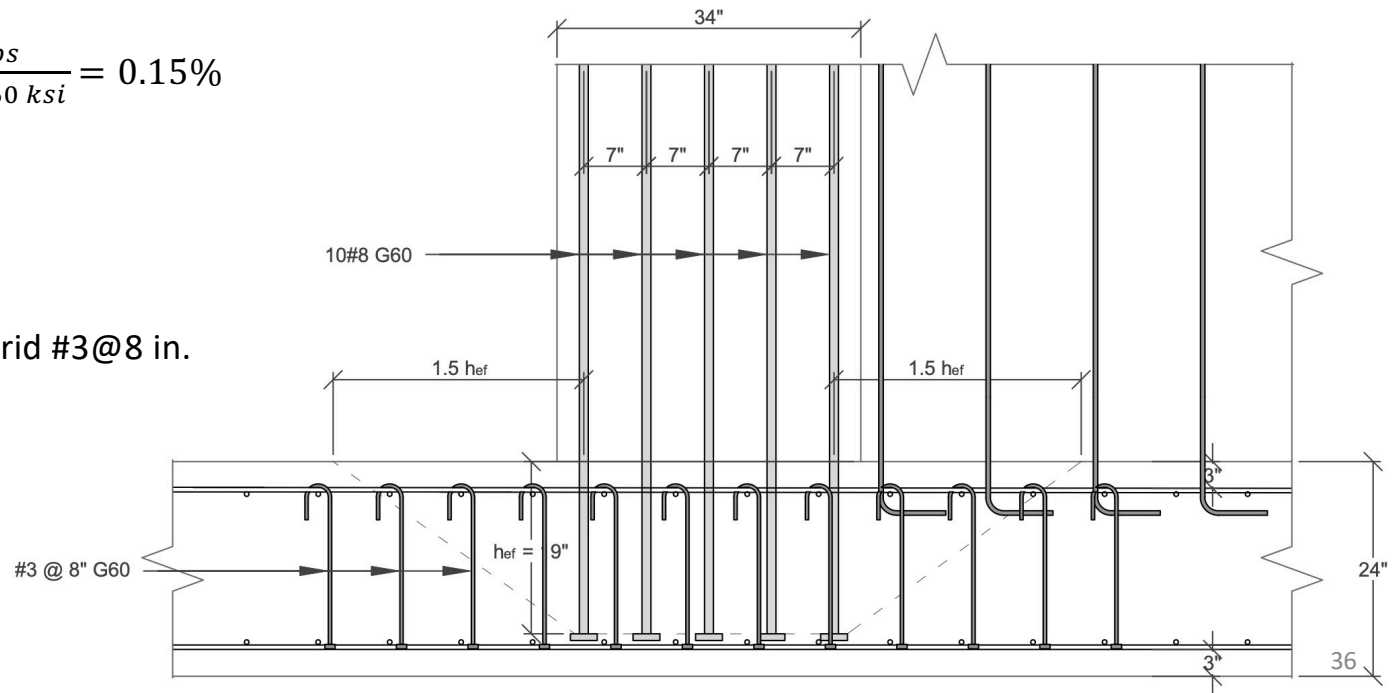
SP-17(14)
SDC D
Special Structural Wall
 $f'_c = 5000\text{psi}$
 $f_y = 60\text{ksi}$

$$\rho_{tr,min} = \frac{N_s}{A_{eff}f_{yt}} = \frac{188\text{kips}}{1377\text{ in.}^2 \cdot 60\text{ ksi}} = 0.15\%$$

$$s_{max} = \frac{h_{ef}}{2} = \frac{19\text{ in.}}{2} = 9.5\text{ in.}$$

Select shear reinforcement grid #3@8 in.

$$\rho_{tr} = 0.17\%$$





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- Worsfold, B., Moehle, J., and Silva, J., accepted for publication 2022, Moment transfer at column-foundation connections: physical tests, *ACI-Structural Journal*, V. 119, No. 5, September 2022²⁸
- Worsfold, B. and Moehle, J., accepted for publication 2022b, Moment Transfer at Column-to-Footing Connections: Analytical Studies, *ACI Structural Journal*