



# Column Base Connections: Research, Design, and a Look to the Future

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Professor, University of California, Davis



2022  
**T.R. HIGGINS  
LECTURESHIP  
AWARD**

# Acknowledgments

## Sponsors

- AISC
- Charles Pankow Foundation
- Pacific Earthquake Engineering Research Center
- National Science Foundation
- California Department of Conservation

# Acknowledgments

## Students

- Ahmad Hassan, UC Davis
- Biao Song, University College London
- Ivan Gomez, Berkshire Hathaway Specialty Insurance
- David Grilli, AARK Engineering
- Ryan Cooke, Schuff Steel
- Vince Pericoli, Sandia Labs
- Santos Jordan, Bushra Tsai Structural Engineers

# Acknowledgments

## Collaborators

- Farzin Zareian, UC Irvine
- Carmine Galasso, University College London
- Dimitrios Lignoş EPFL, Switzerland
- Pablo Torres, University of San Francisco, Ecuador
- Greg Deierlein, Stanford University
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# Acknowledgments

## Other researchers and practitioners

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- Rick Drake, Fluor Corporation
- Geoff Bomba and Mason Walters, Forell Elsesse Engineers
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- Bo Dowswell, ARC International
- Tara Hutchinson, UCSD
- Frantisek Wald, Czech Technical University, Prague
- John Barsom
- Tom Schlafly, AISC

# T.R. HIGGINS JURY 2022

Michel Bruneau – University at Buffalo SUNY

John Rolfes – CSD

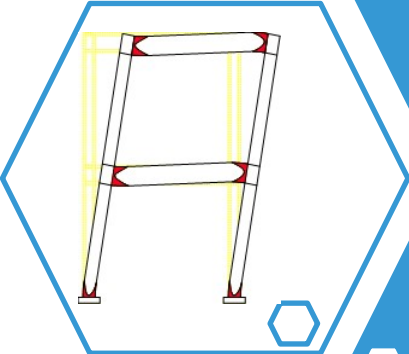
Joel Chandler – Owen Steel Company

Tom Sabol – Englekirk Structural Engineers

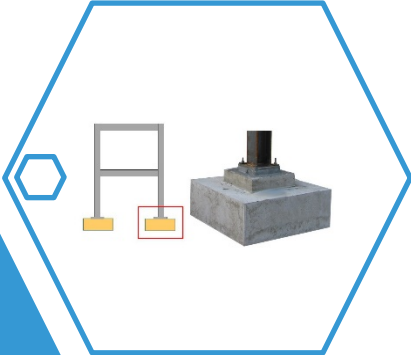
Matthew Eatherton – Virginia Tech

Matt Smith – L&M Industrial Fabrication

# Column base connections

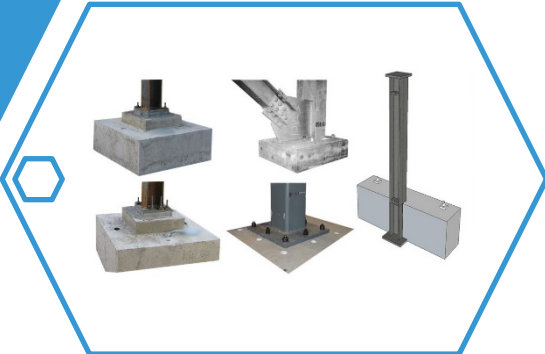


Used in all buildings

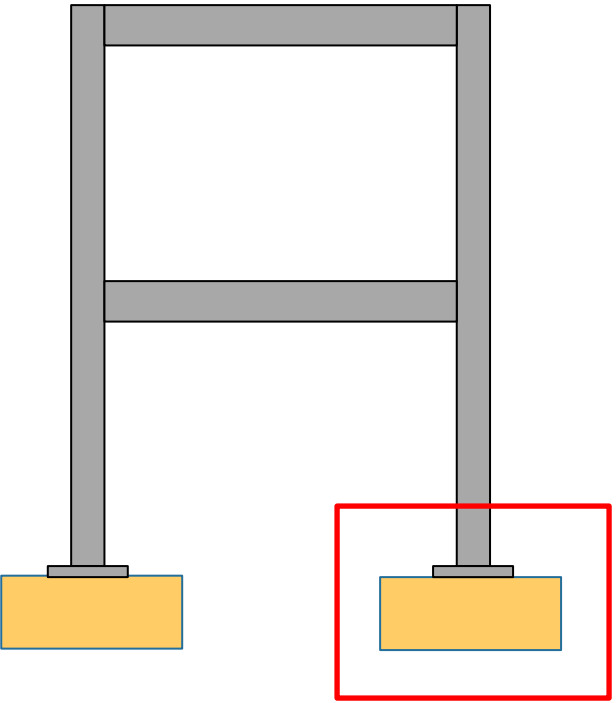


Wide range of details

Used in many contexts



# Used in all buildings





# Used in all buildings

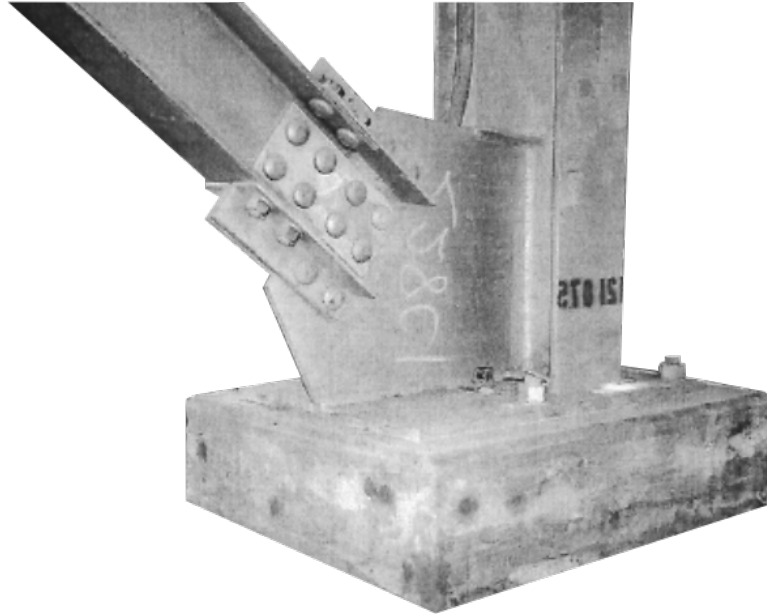
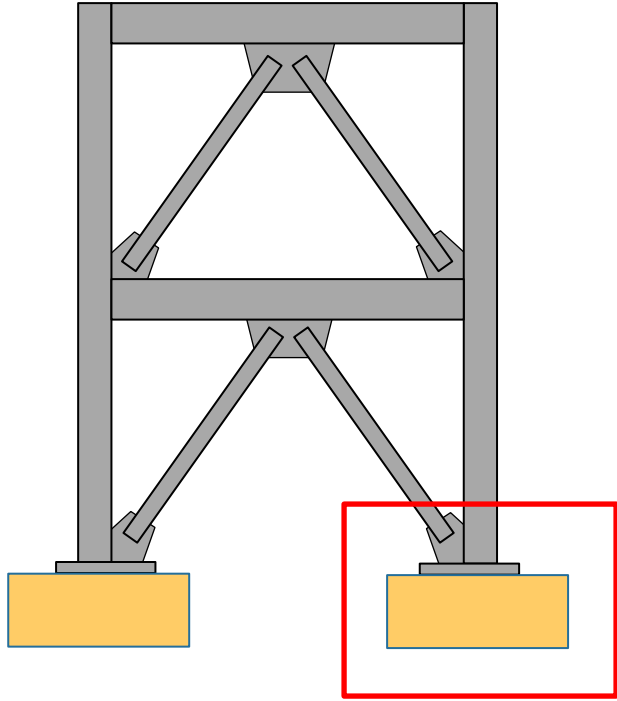
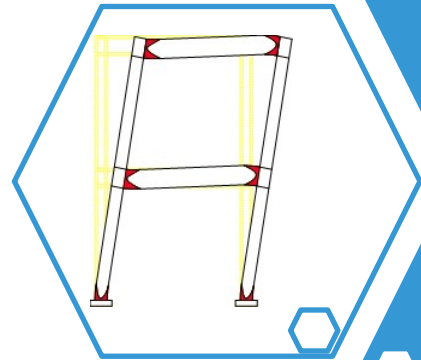
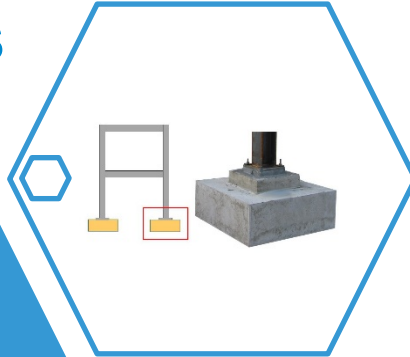


Photo credit: Rick Drake (2003)

# Column base connections

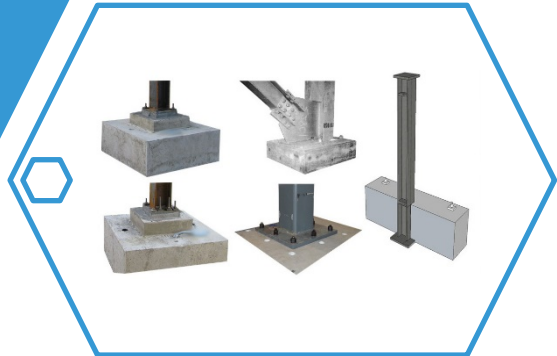


Used in  
all  
buildings

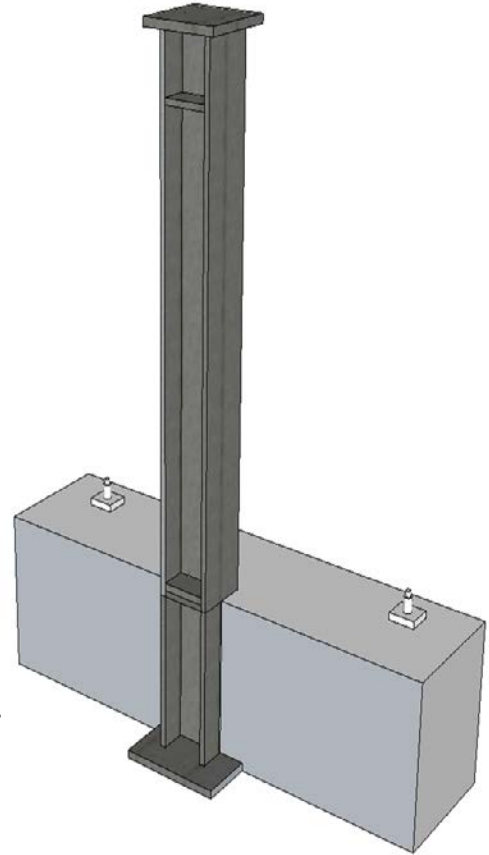
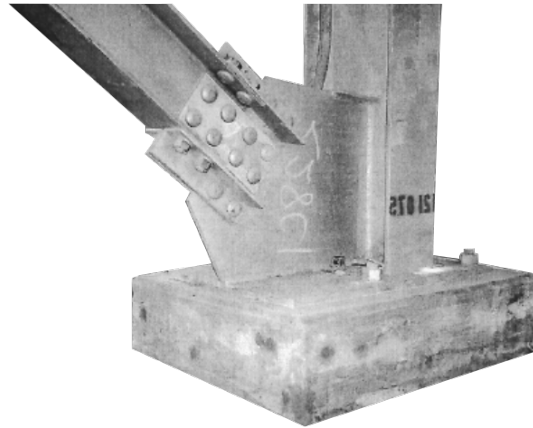


Wide  
range of  
details

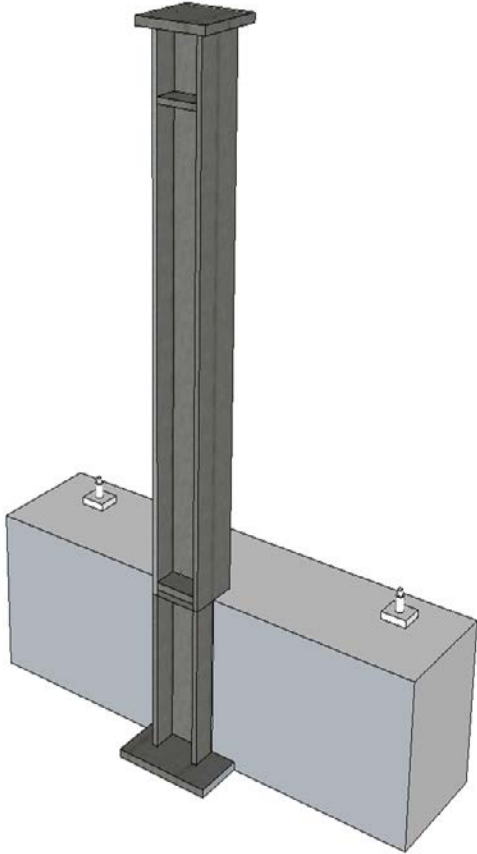
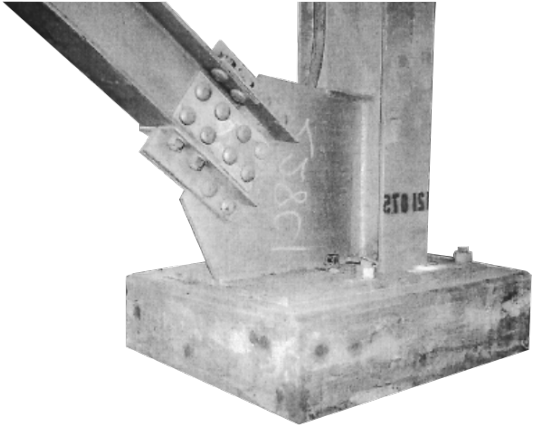
Used in  
many  
contexts



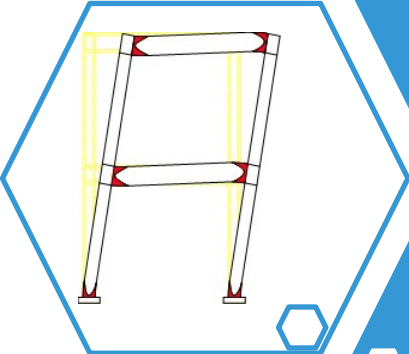
# Diversity in details



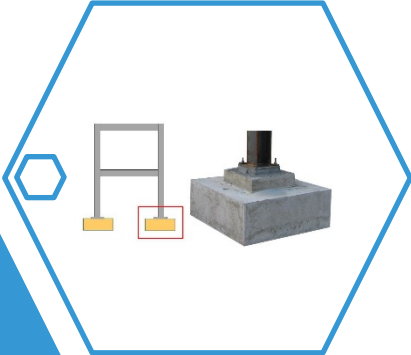
# Always at steel/concrete interface



# Column base connections

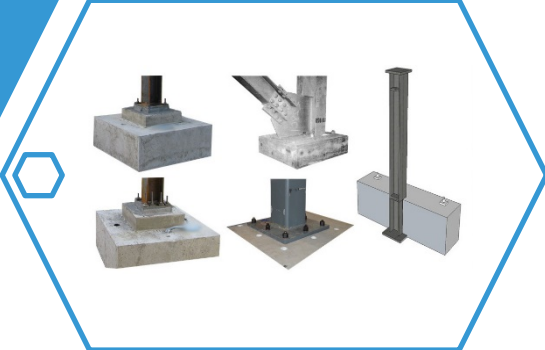


Used in all buildings



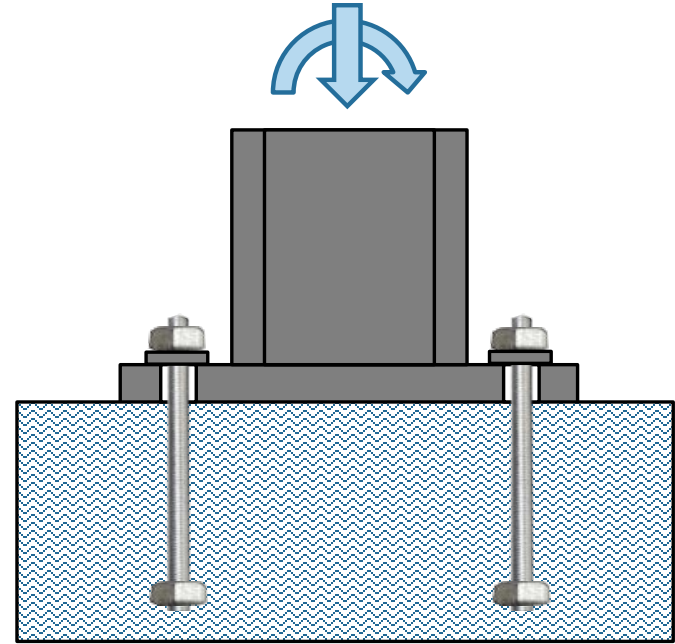
Wide range of details

Used in many contexts



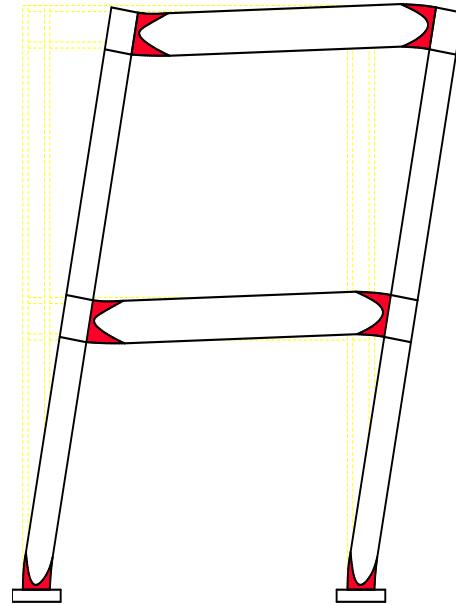
# Interesting in many contexts

- Static loads
- Seismic loads
- Interactions with frame



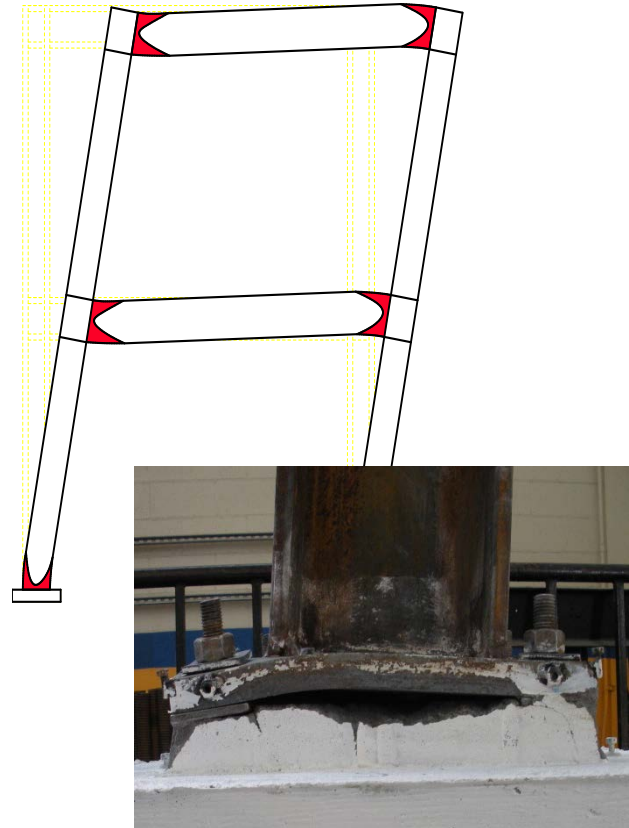
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- Static loads
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# Interesting in many contexts

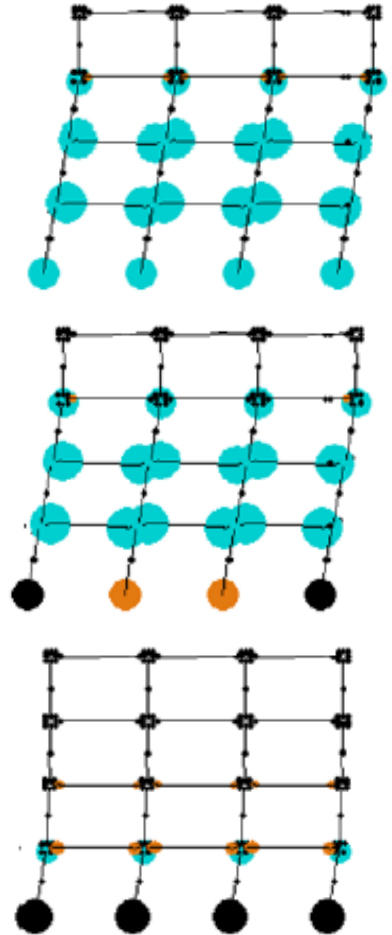
- Static loads
- Seismic loads
- Interactions with frame





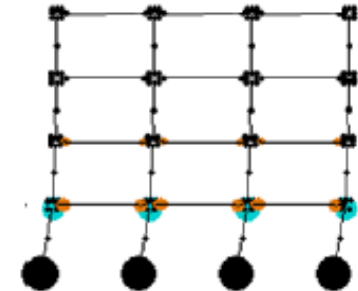
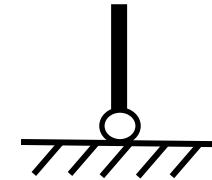
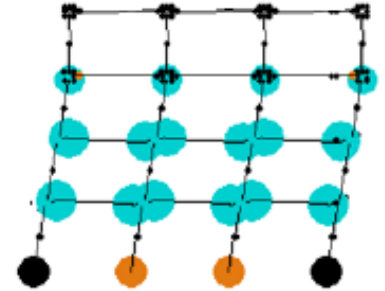
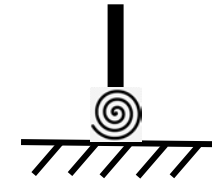
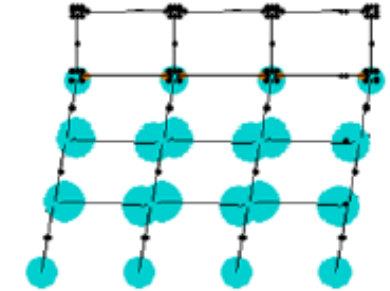
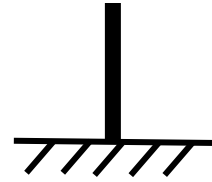
# Interesting in many contexts

- Static loads
- Seismic loads
- Interactions with frame



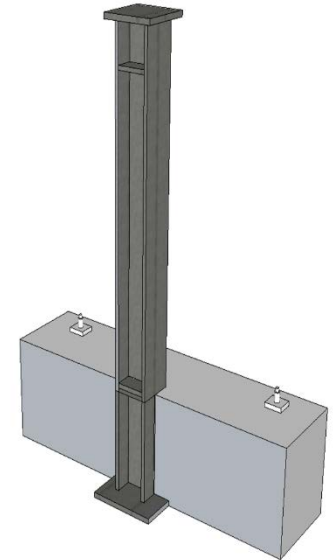
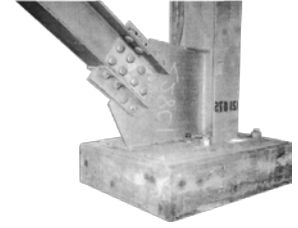
# Interesting in many contexts

- Static loads
- Seismic loads
- Interactions with frame

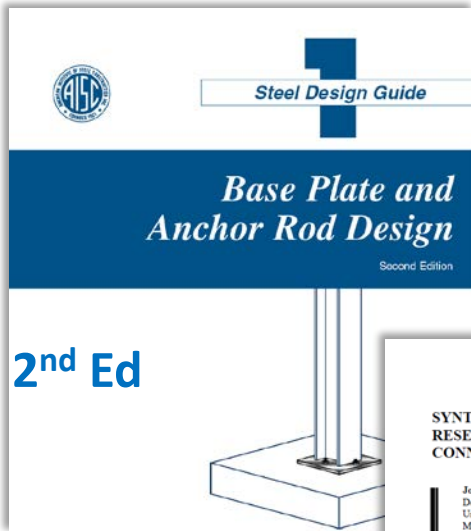


# Challenging to navigate

- Static loads
- Seismic loads
- Interactions with frame



# Timeline and scope



2<sup>nd</sup> Ed

## SYNTHESIS OF DESIGN, TESTING AND ANALYSIS RESEARCH ON STEEL COLUMN BASE PLATE CONNECTIONS IN HIGH-SEISMIC ZONES

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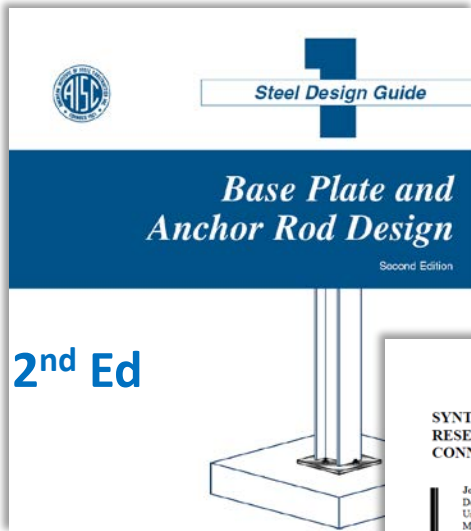
Structural Engineering Report No. ST-04-02

Department of Civil Engineering  
500 Pillsbury Drive SE  
University of Minnesota  
Minneapolis, Minnesota 55455-0116  
<http://www.ce.umn.edu>

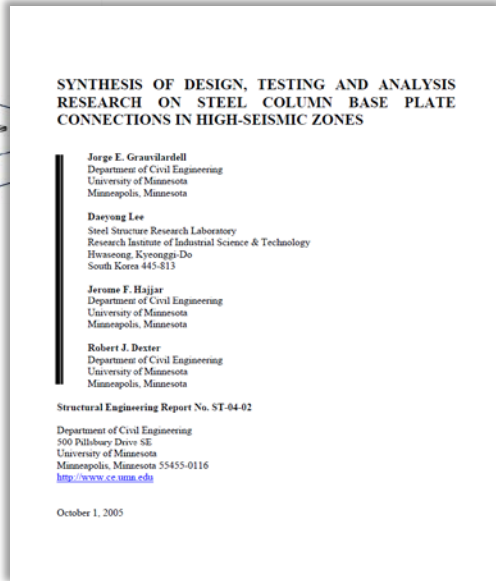
October 1, 2005

2005-2006

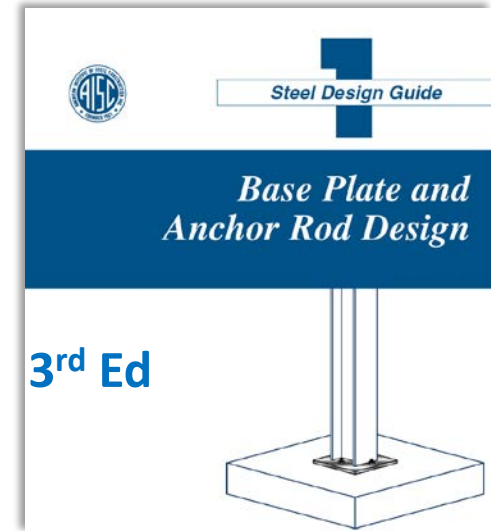
# Timeline and scope



2<sup>nd</sup> Ed



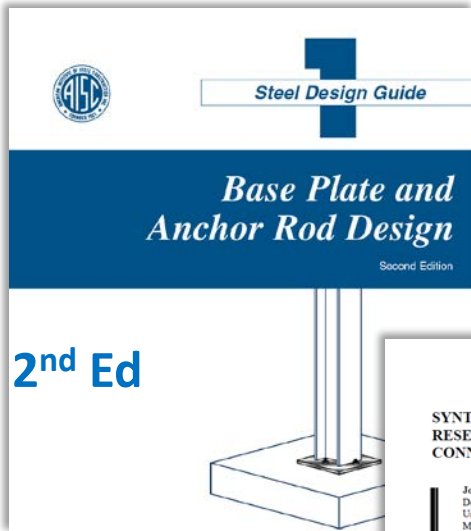
2005-2006



3<sup>rd</sup> Ed

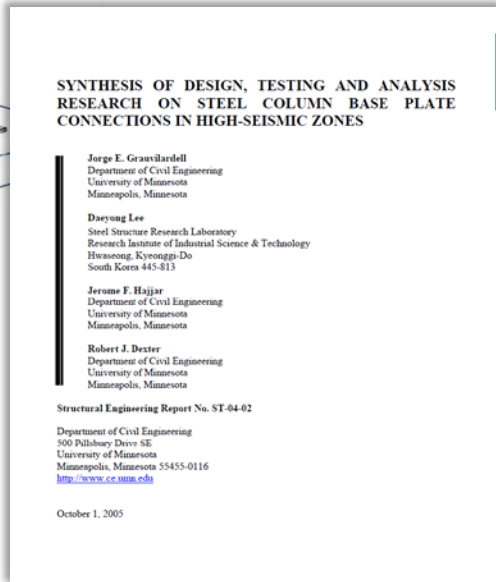
2024-ish

# Timeline and scope

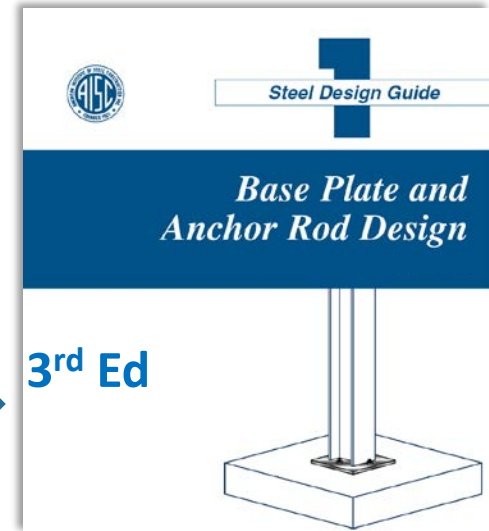


2<sup>nd</sup> Ed

2005-2006



New  
developments



3<sup>rd</sup> Ed

2024-ish

# Organization

## Part 1

Exposed  
Base Plates

Prevailing  
understanding  
and design  
methods

New  
Developments

~35 mins

## Part 2

Embedded  
Bases

Prevailing  
understanding  
and design  
methods

New  
Developments

~15 mins

## Part 3

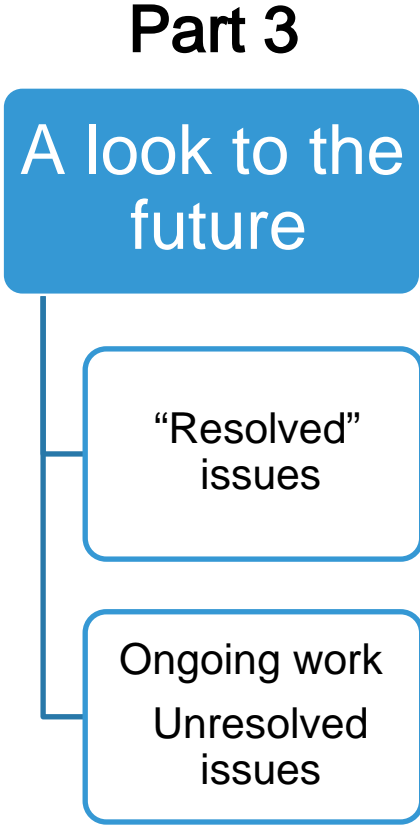
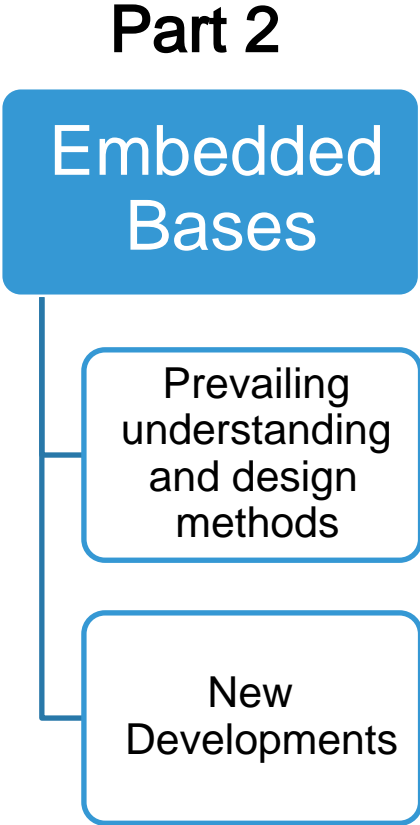
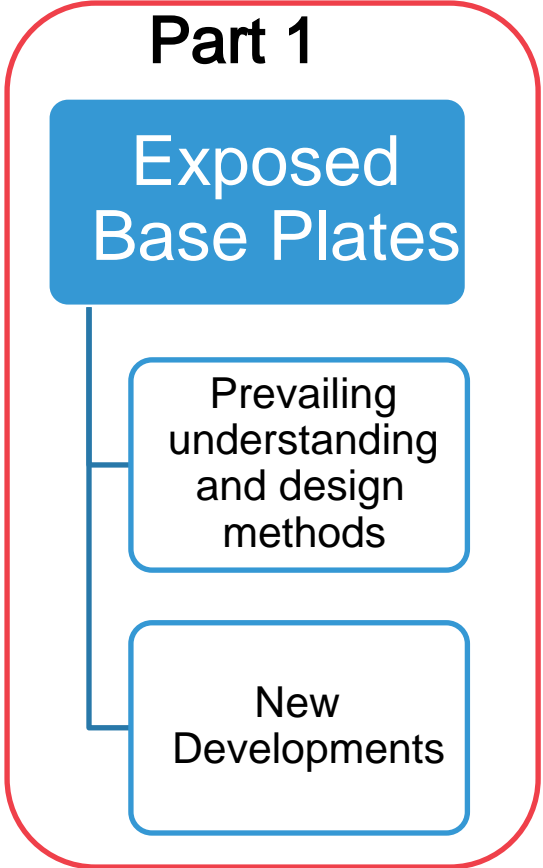
A look to the  
future

“Resolved”  
issues

Ongoing work  
Unresolved  
issues

~15 mins

# Organization



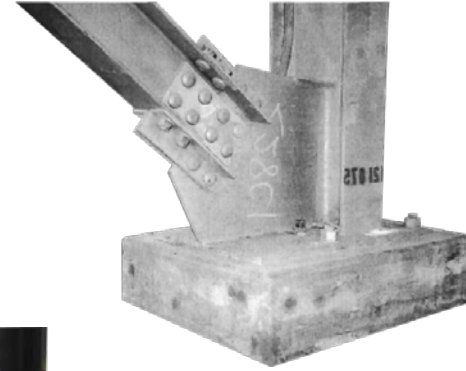


# Part 1 – Exposed Base Plate Connections

## Exposed Base Plates

Prevailing understanding and design methods

New Developments

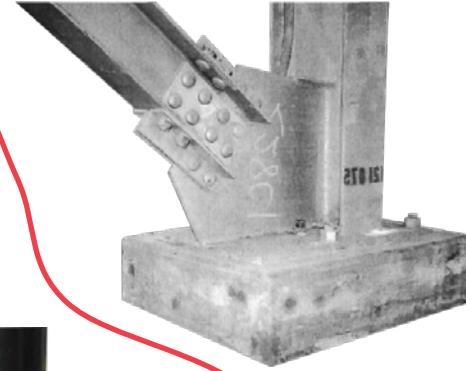


# Part 1 – Exposed Base Plate Connections

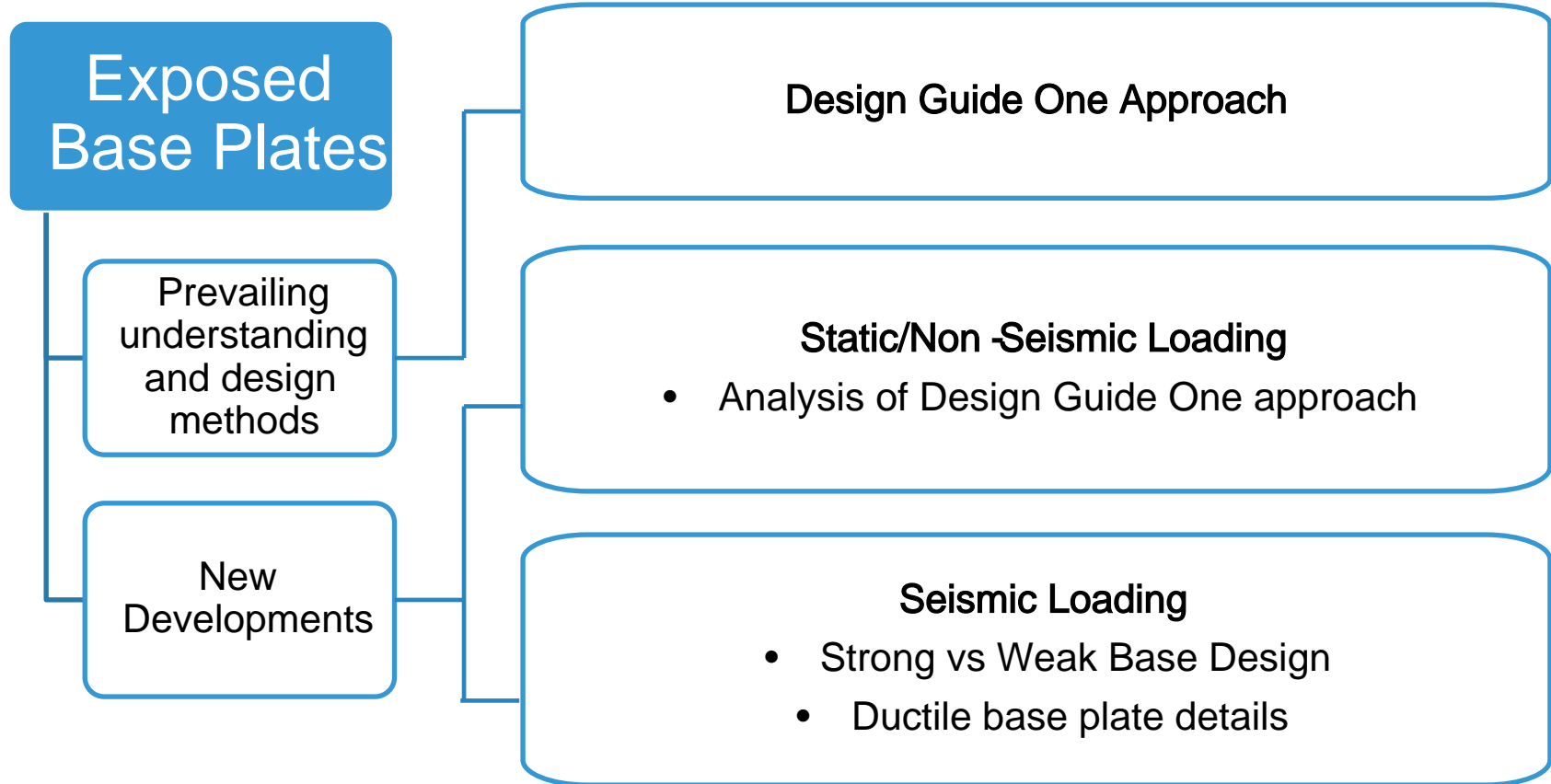
## Exposed Base Plates

Prevailing understanding and design methods

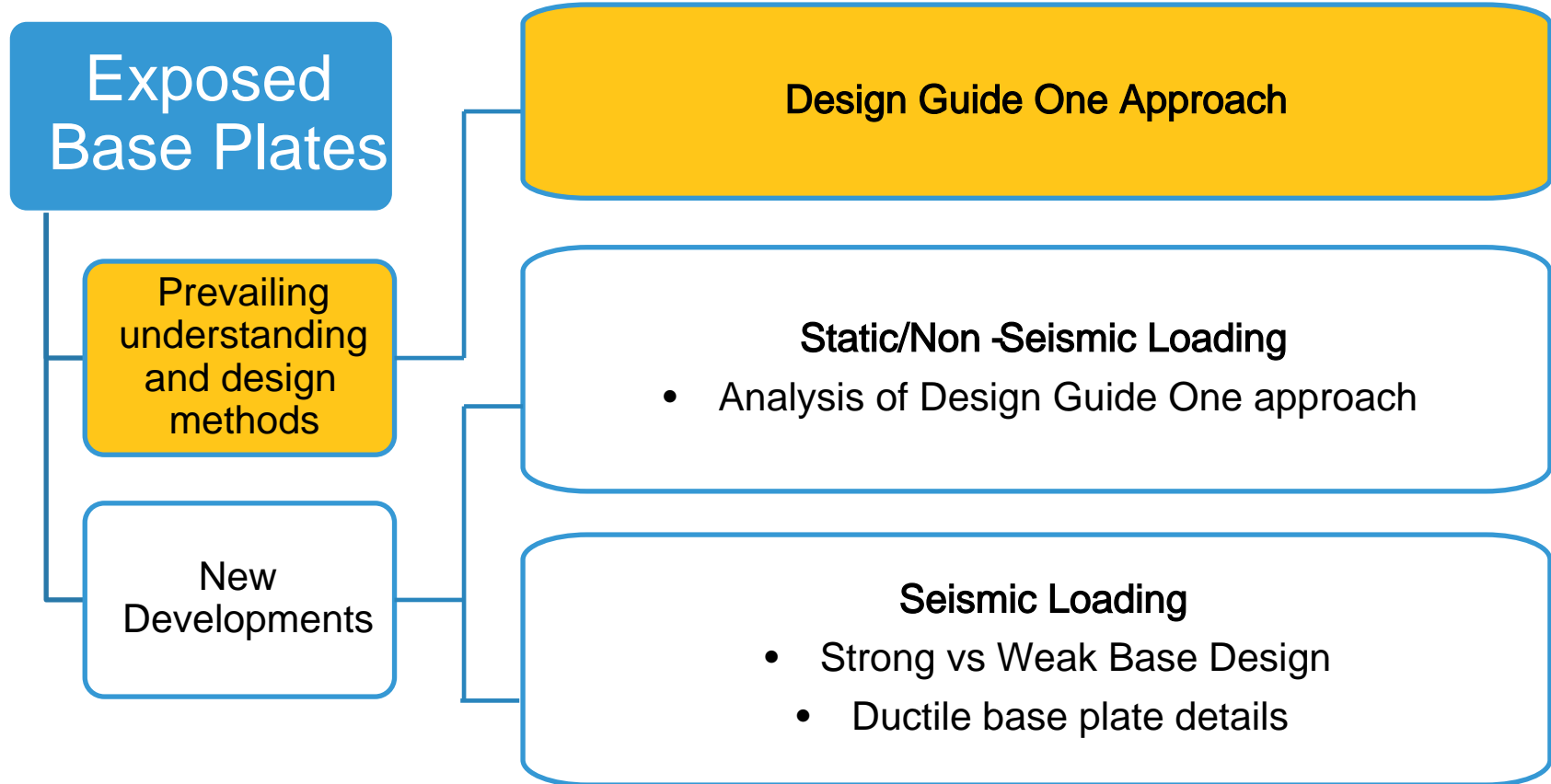
New Developments



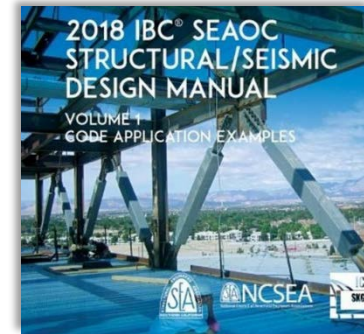
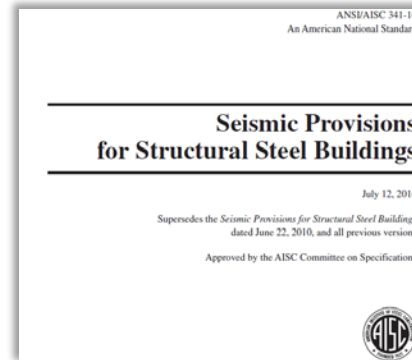
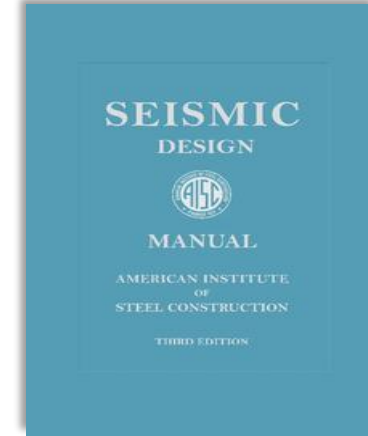
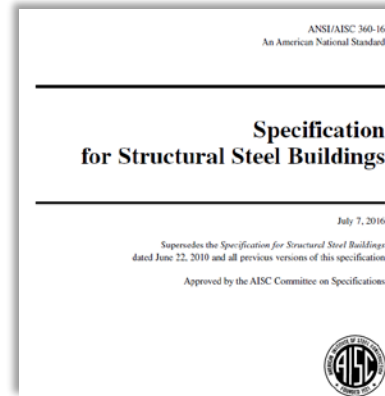
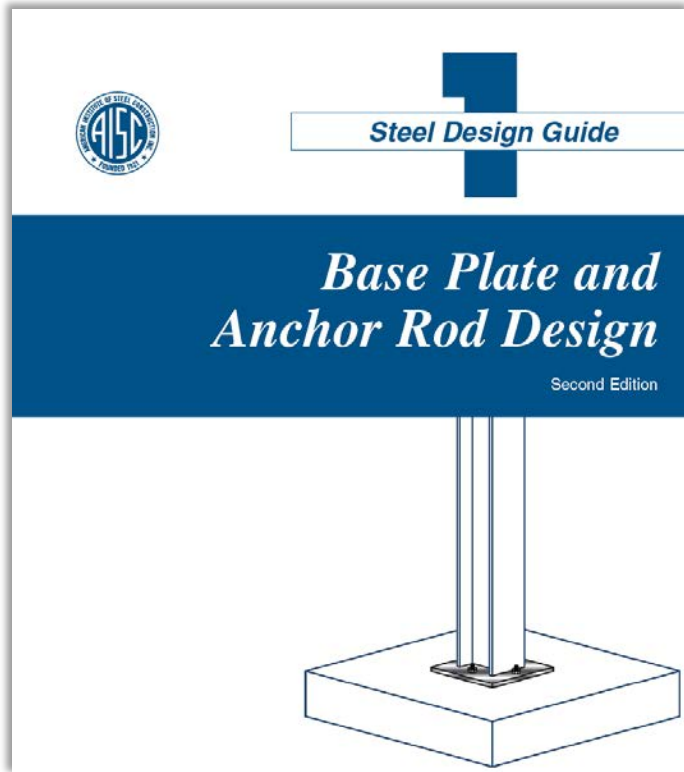
# Part 1 – Exposed Base Plate Connections



# Part 1 – Exposed Base Plate Connections



# State of the art— Exposed base plate connections

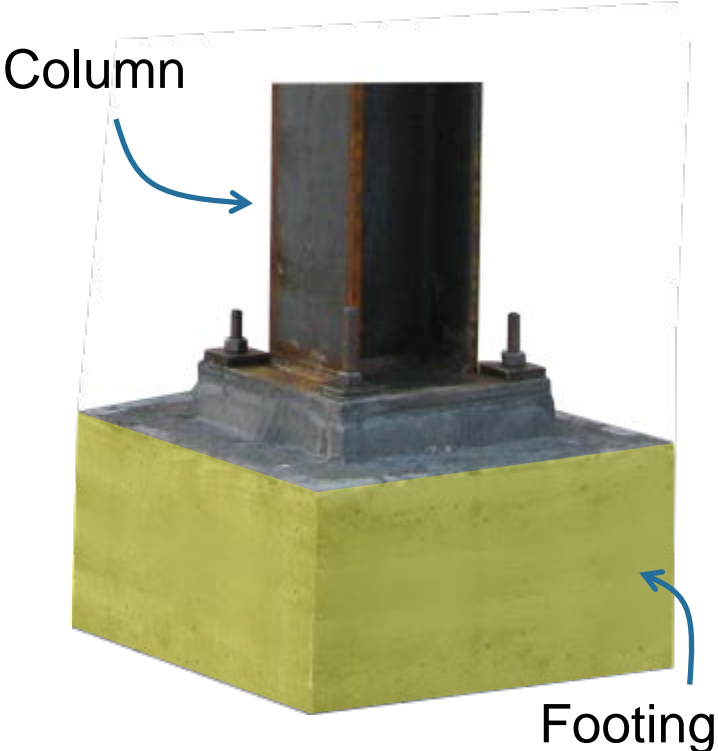


# Design Guide One

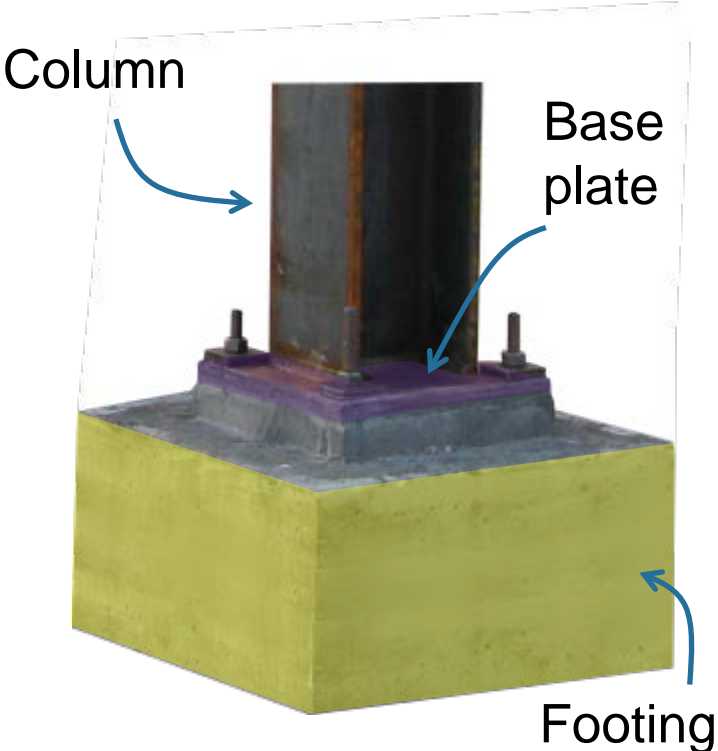
Focusing on one configuration



# Design Guide One

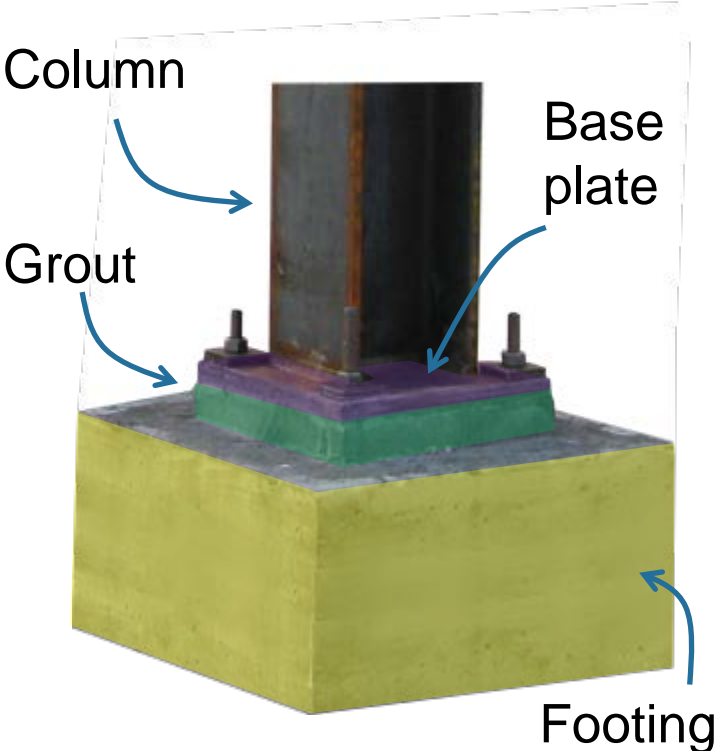


# Design Guide One

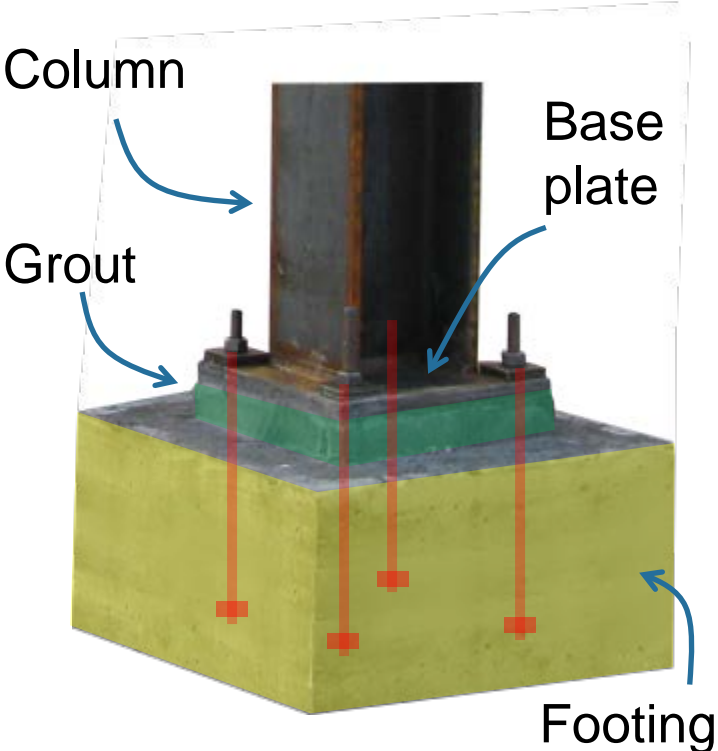




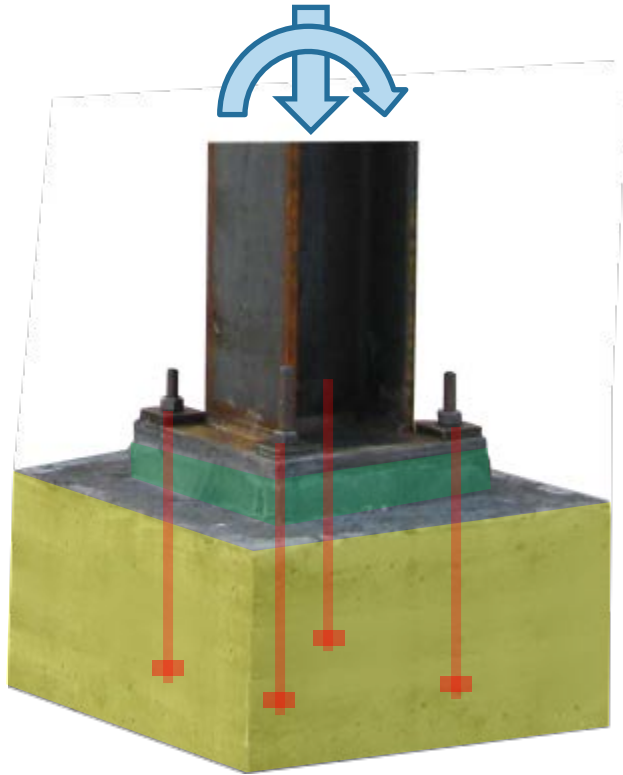
# Design Guide One



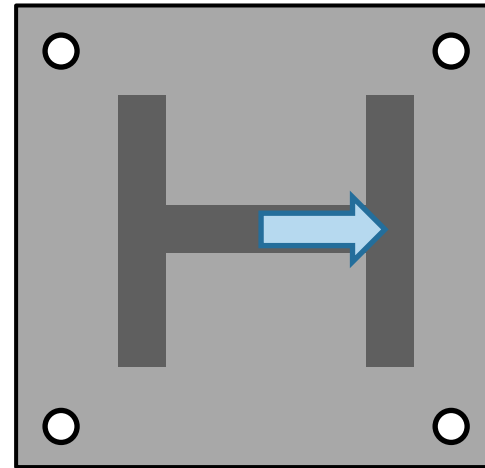
# Design Guide One



# Design Guide One

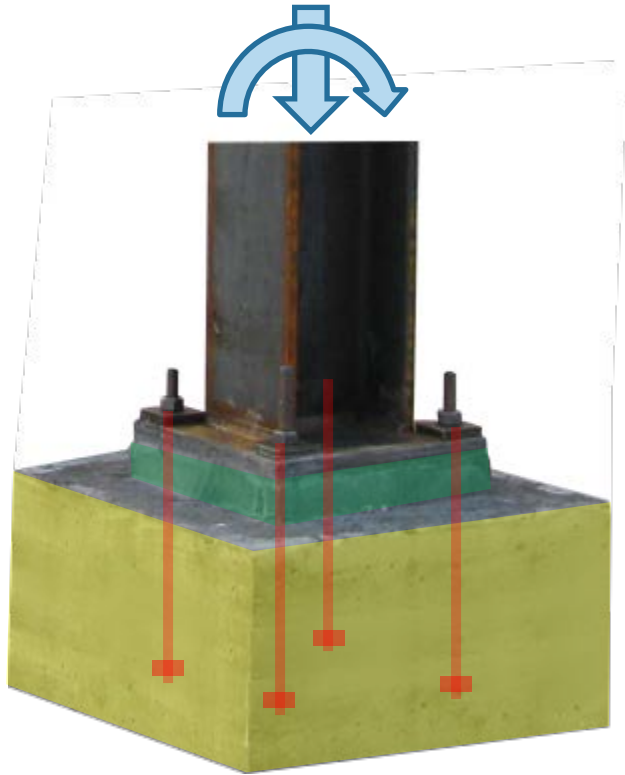


Uniaxial bending with axial compression

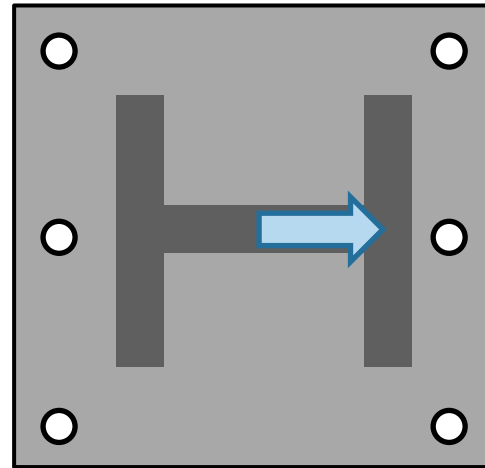


Two rows of anchors resisting bending

# Design Guide One



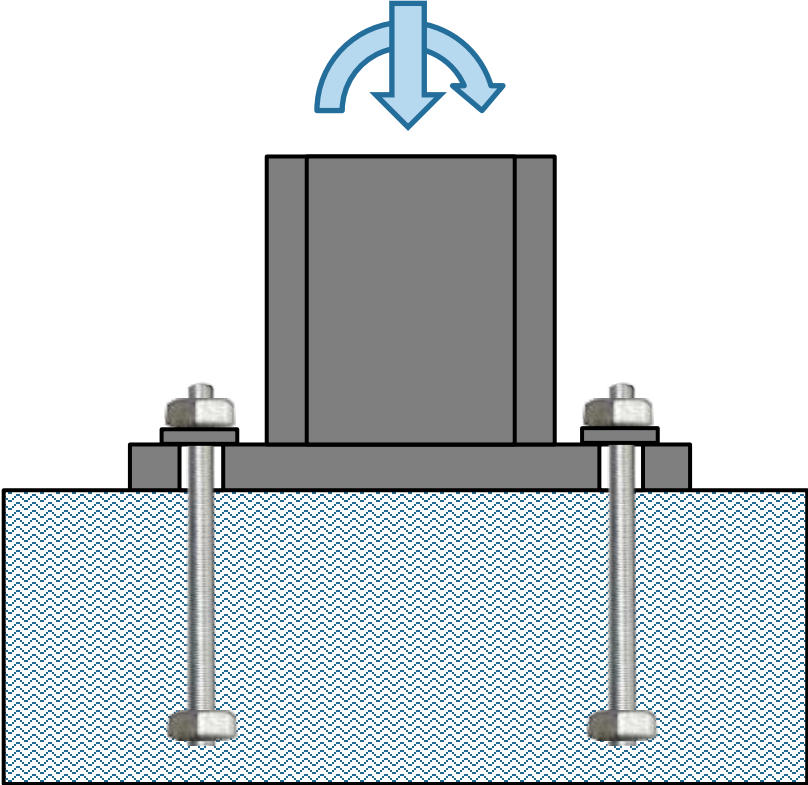
Uniaxial bending with axial compression



Two rows of anchors resisting bending

# The mechanics

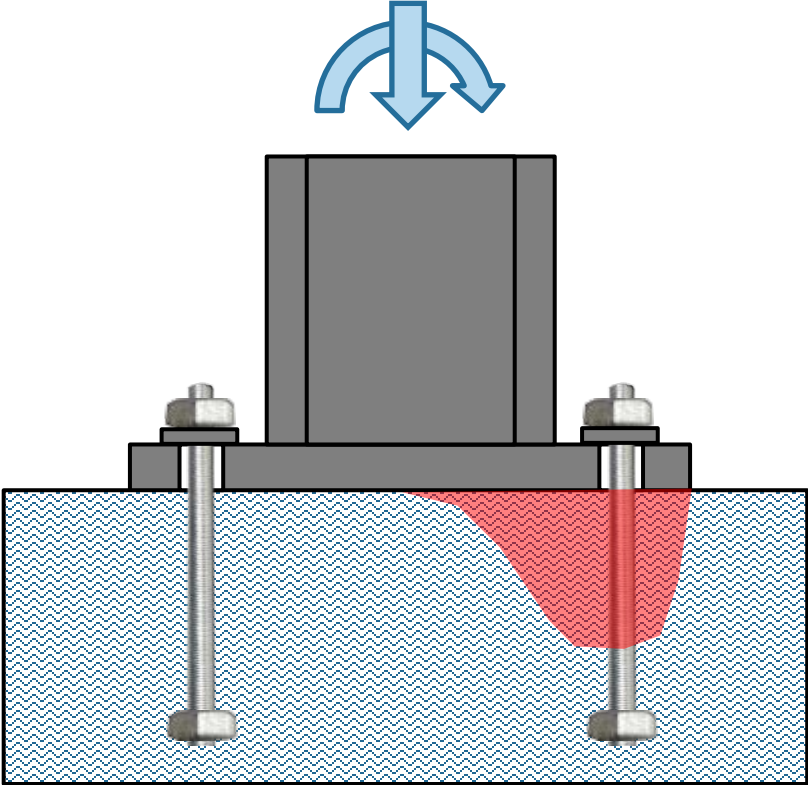
Simple in principle



# The mechanics

Simple in principle

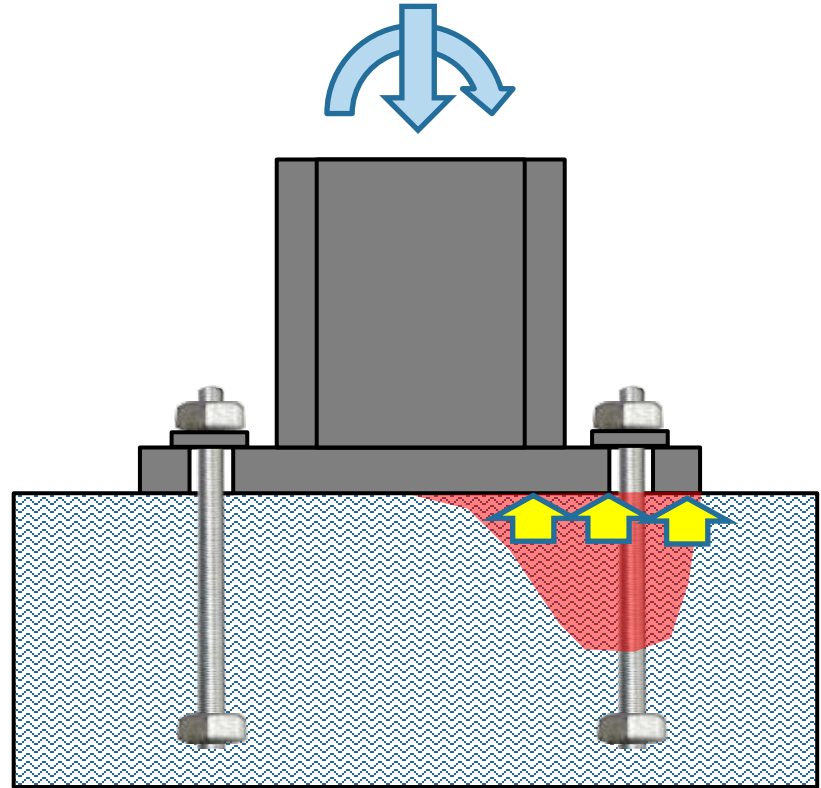
- Bearing in footing



# The mechanics

Simple in principle

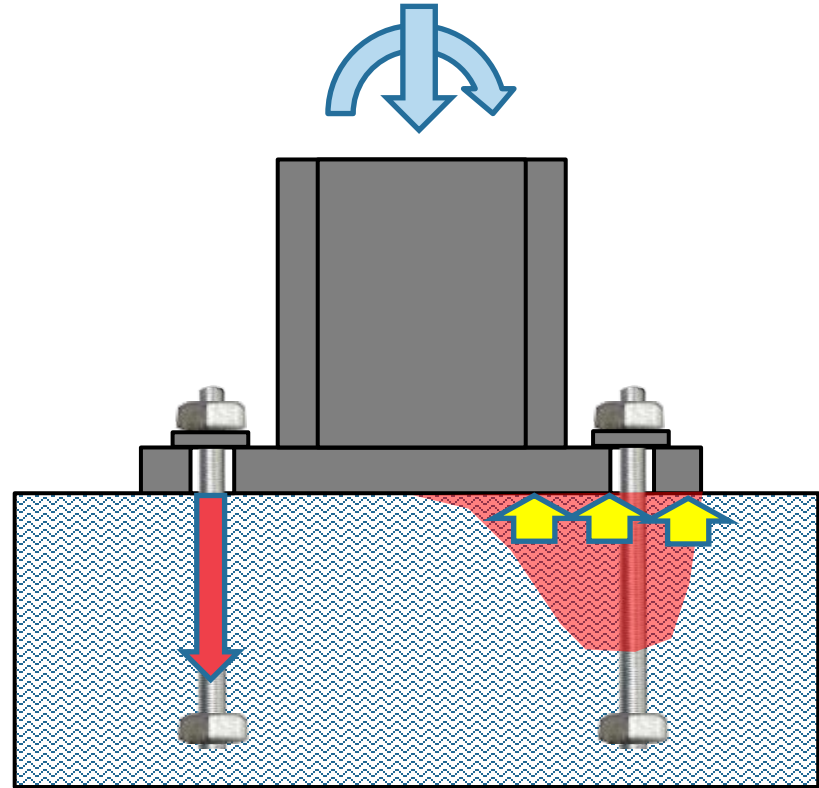
- Bearing in footing



# The mechanics

Simple in principle

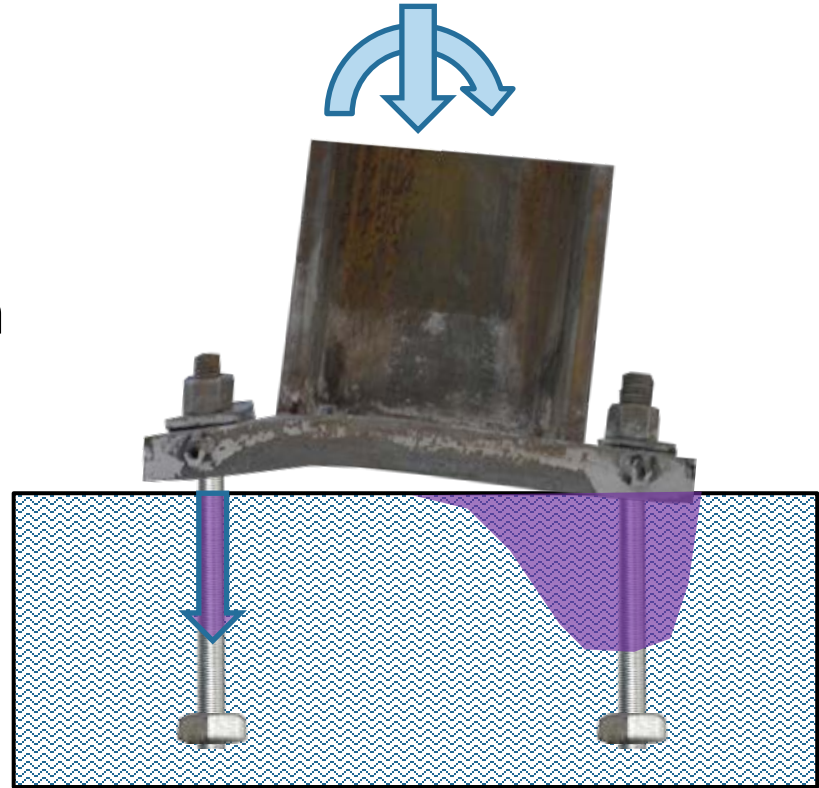
- Bearing in footing
- Tension in rods





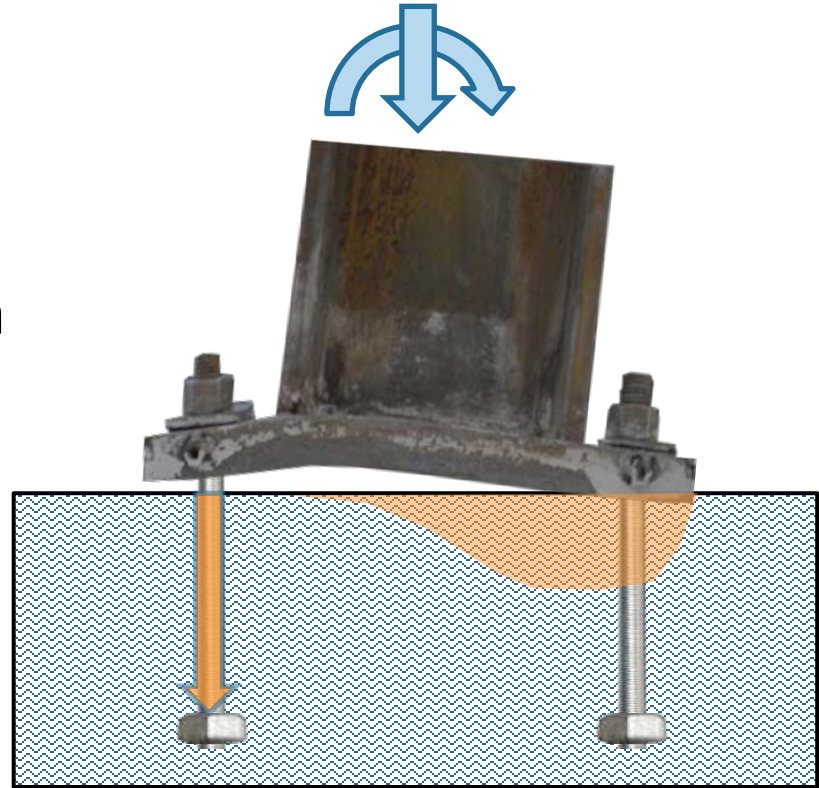
# The mechanics

- Multiple distributions satisfy equilibrium
- True distributions depend on interplay of plate, rod, and flexibility and nonlinearity
- Determining these is non trivial



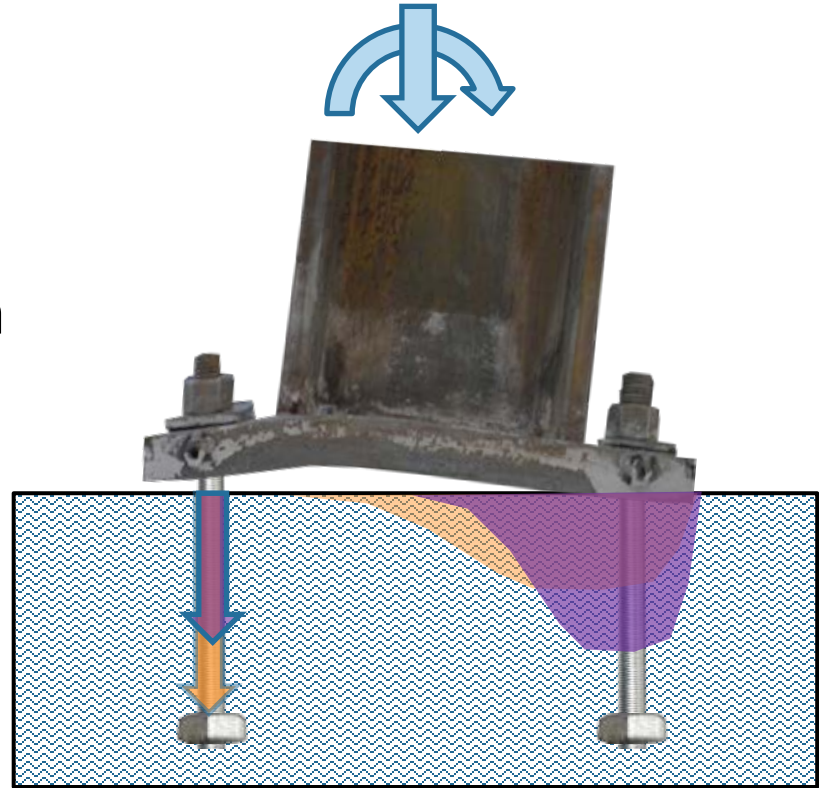
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# The mechanics

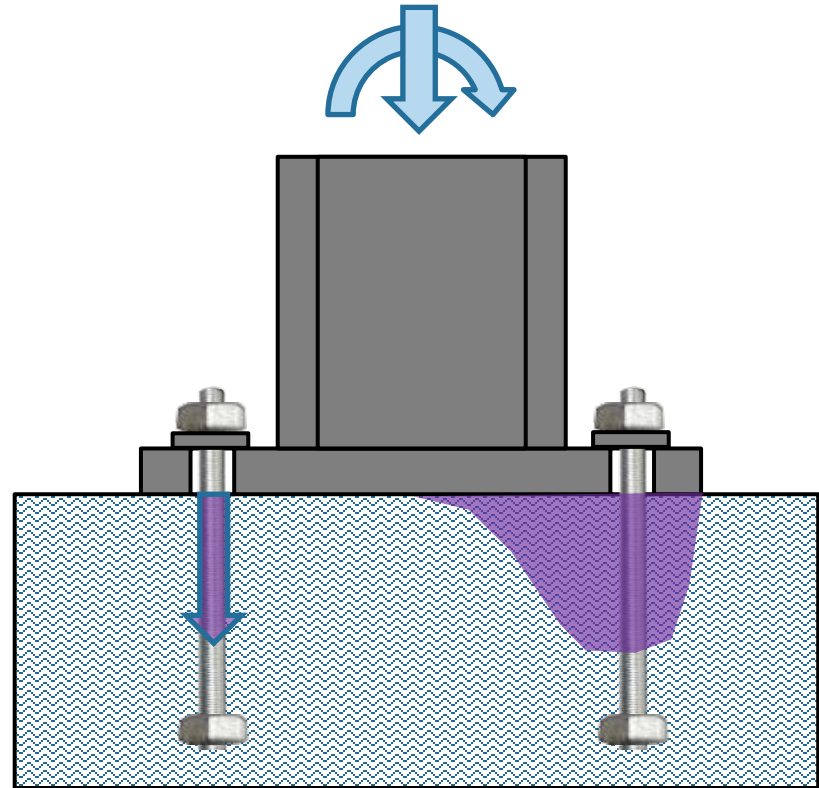
- Multiple distributions satisfy equilibrium
- True distributions depend on interplay of plate, rod, and flexibility and nonlinearity
- Determining these is non trivial



# Design Guide One approach

Culmination and integration of work by researchers

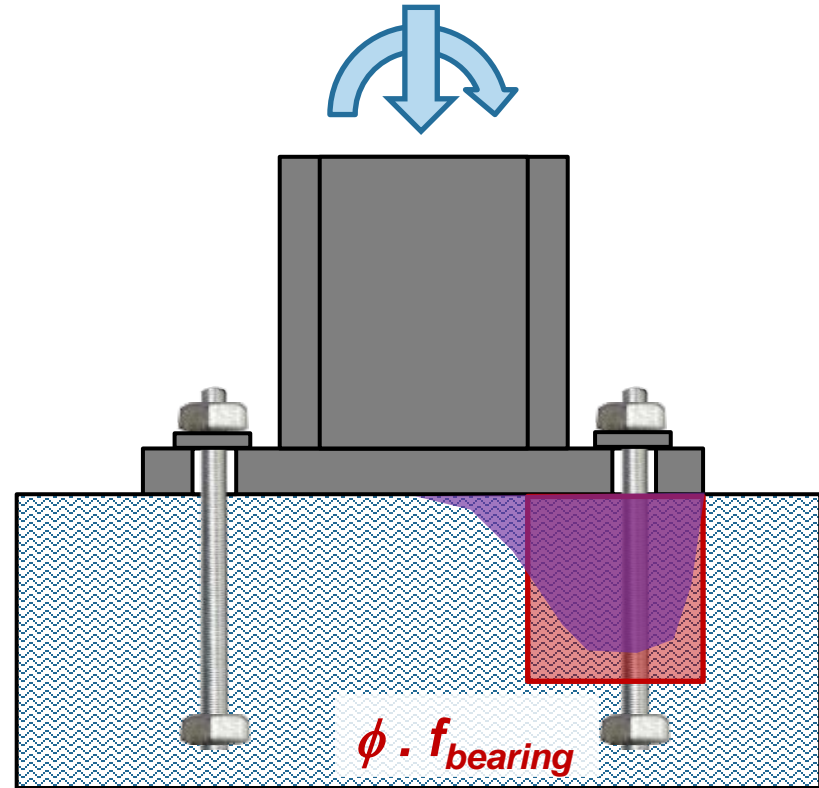
- DeWolf and Sarisley (1978,80,82)
- Thambiratnam and Paramasivam (1986)
- Drake and Elkin (1999)



# Design Guide One approach

## STEP 1

- Idealize distribution based on bearing strength of footing



\*High eccentricity condition

# Design Guide One approach

## STEP 1

- Idealize distribution based on bearing strength of footing

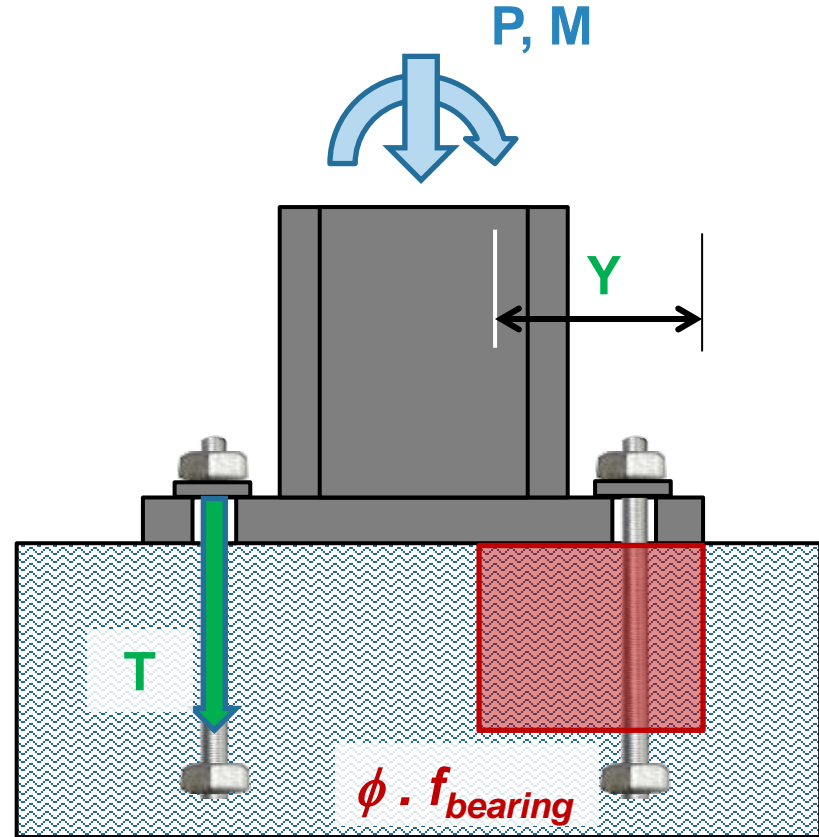
$$\phi \cdot f_{bearing} \quad (\phi = 0.65)$$

- Two equilibrium equations

P and M

- Two unknowns

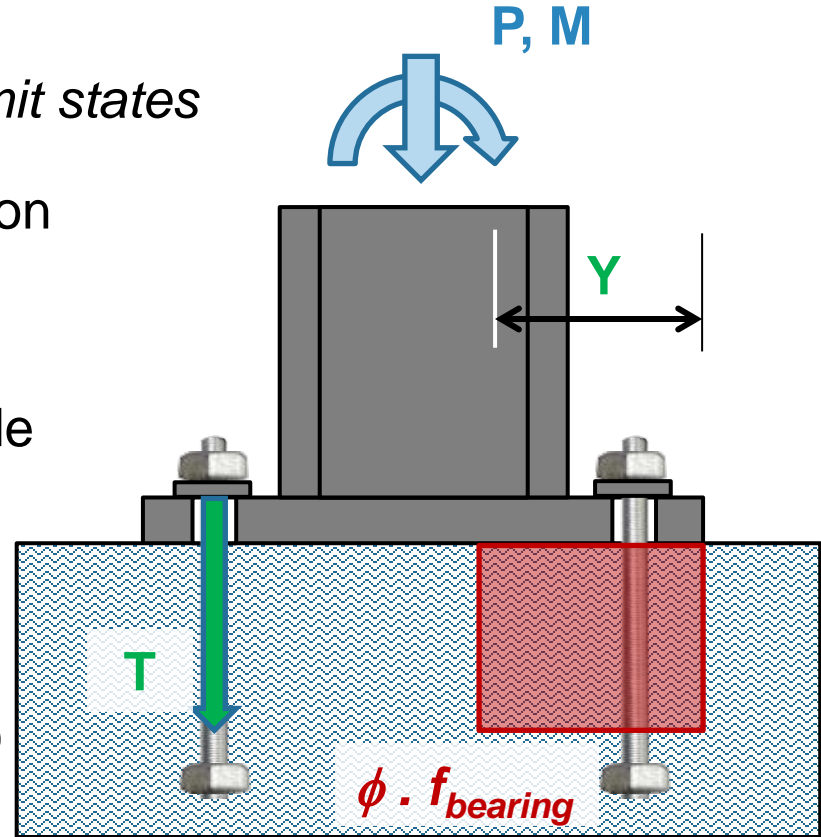
Y and T



# Design Guide One approach

*STEP 2 – Given  $Y$  and  $T$ , evaluate limit states*

- Base plate yielding on compression side
- Base plate yielding on tension side
- Anchor rod yielding
- Bearing failure of footing (implicit)

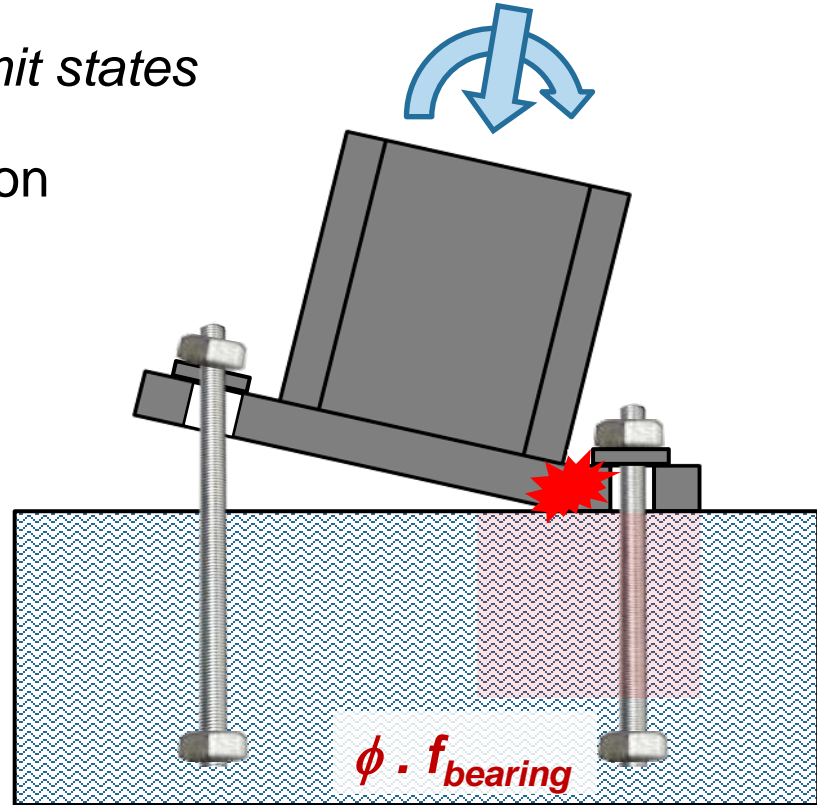


# Design Guide One approach

*STEP 2 – Given  $Y$  and  $T$ , evaluate limit states*

- Base plate yielding on compression side

$$M_{comp} < \phi \cdot M_{plate}$$



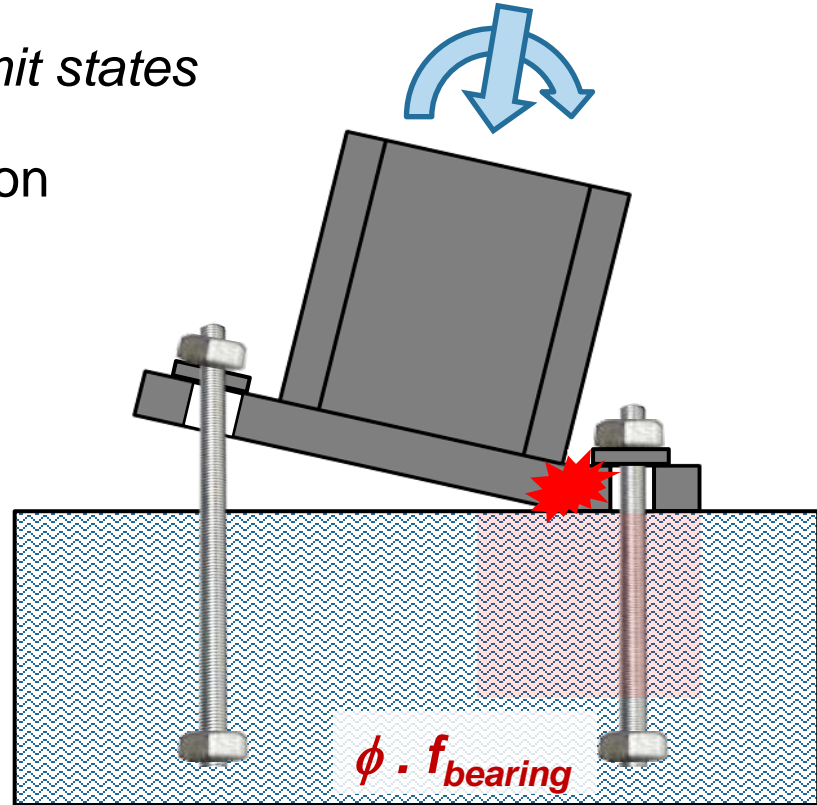
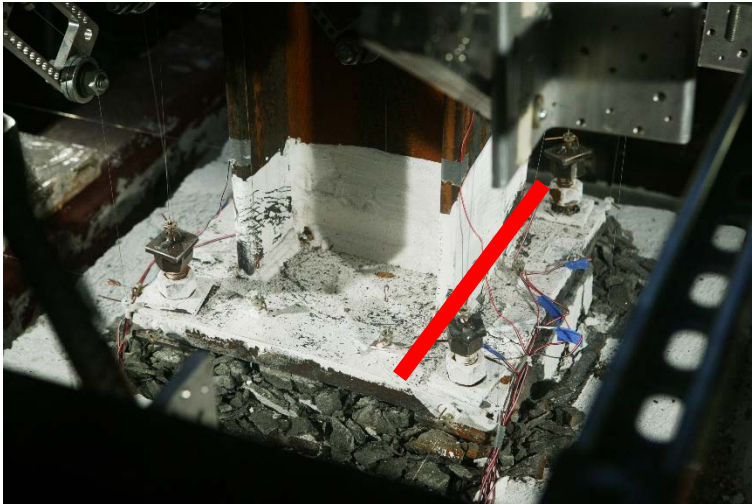


# Design Guide One approach

*STEP 2 – Given  $Y$  and  $T$ , evaluate limit states*

- Base plate yielding on compression side

$$M_{comp} < \phi \cdot M_{plate} \quad (\phi = 0.9)$$

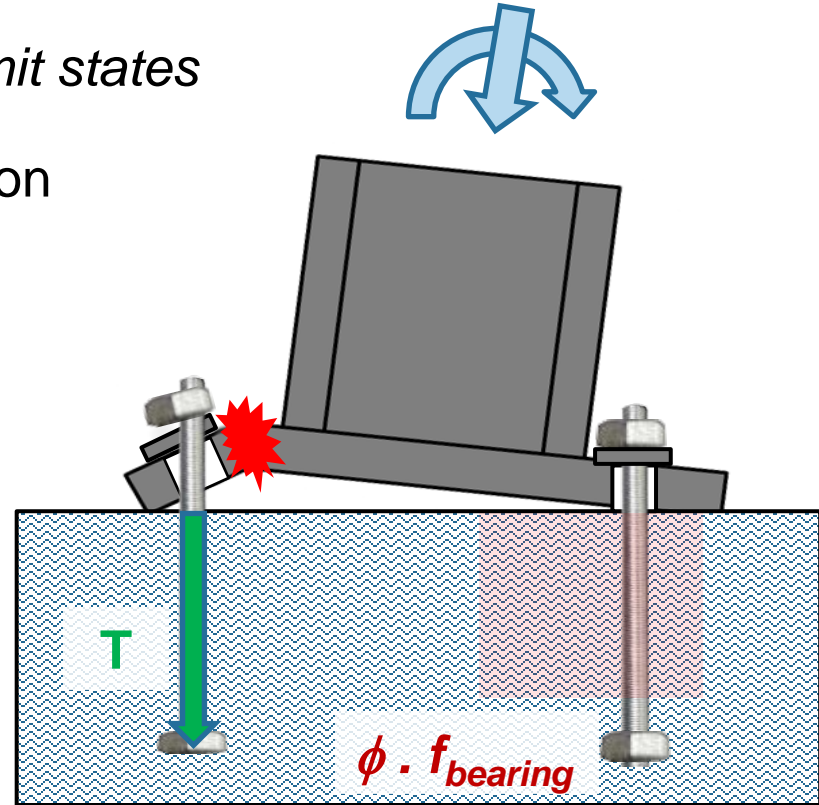
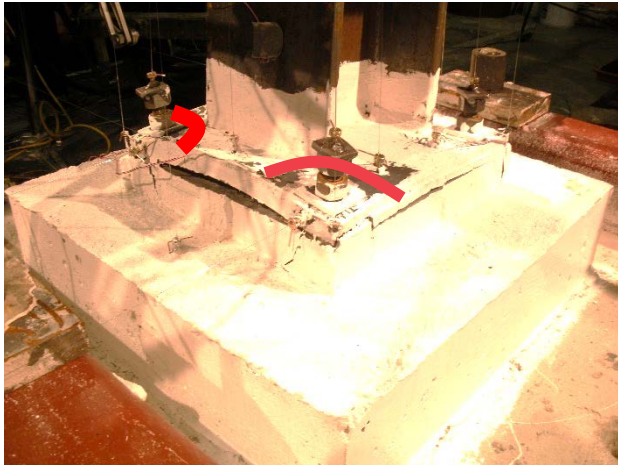


# Design Guide One approach

*STEP 2 – Given  $Y$  and  $T$ , evaluate limit states*

- Base plate yielding on compression side

$$M_{tens} < \phi \cdot M_{plate} \quad (\phi = 0.9)$$

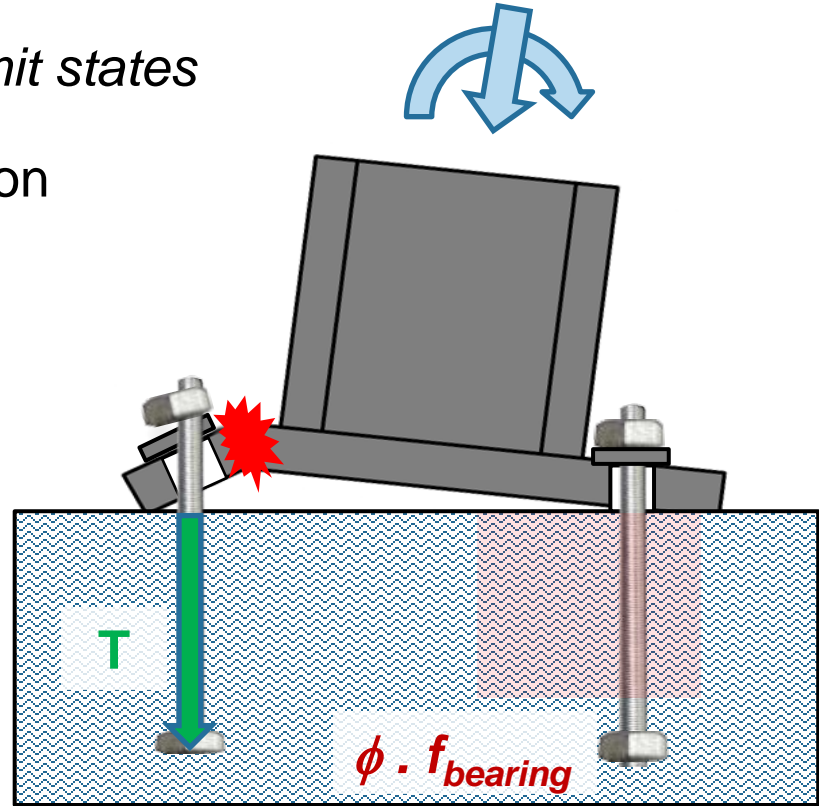
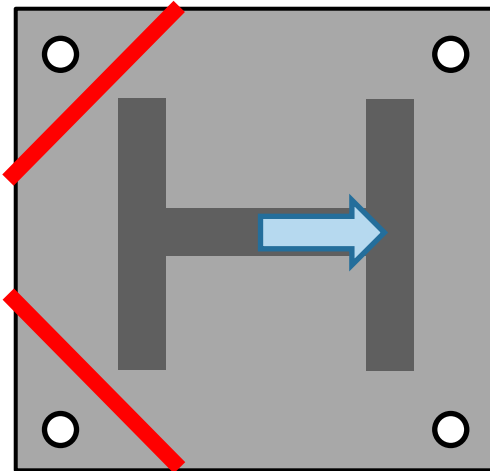


# Design Guide One approach

STEP 2 – Given  $Y$  and  $T$ , evaluate limit states

- Base plate yielding on compression side

$$M_{tens} < \phi \cdot M_{plate} \quad (\phi = 0.9)$$

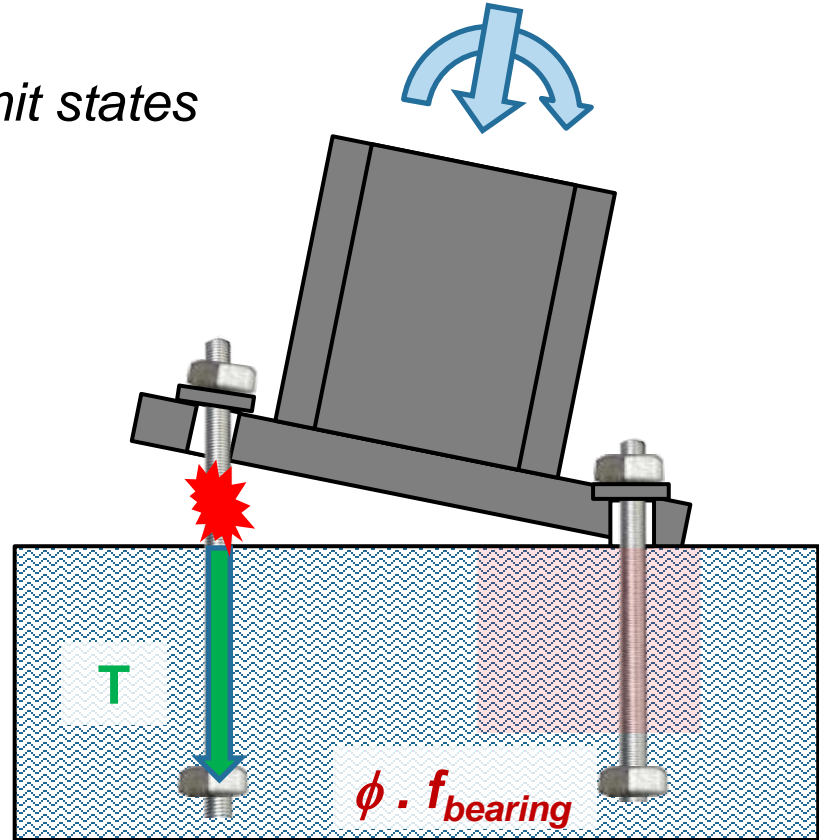
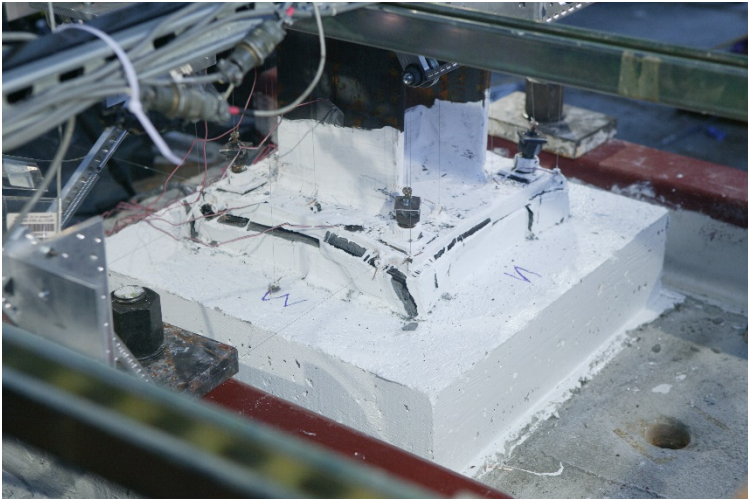


# Design Guide One approach

*STEP 2 – Given  $Y$  and  $T$ , evaluate limit states*

- Yielding or failure of the anchors

$$T < \phi \cdot T_{rod} (\phi = 0.9)$$

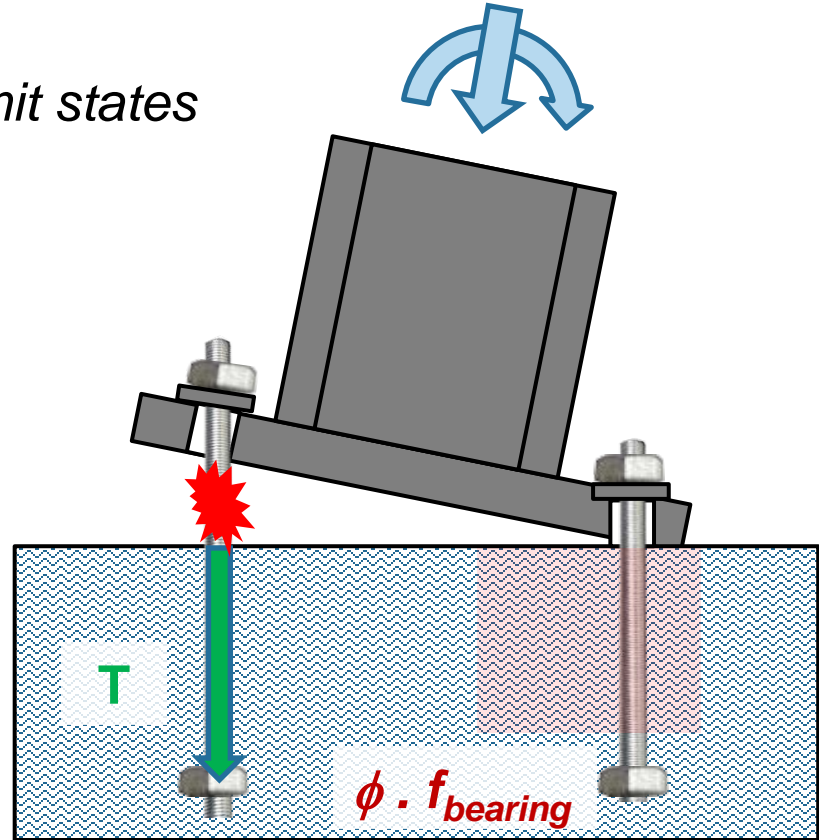
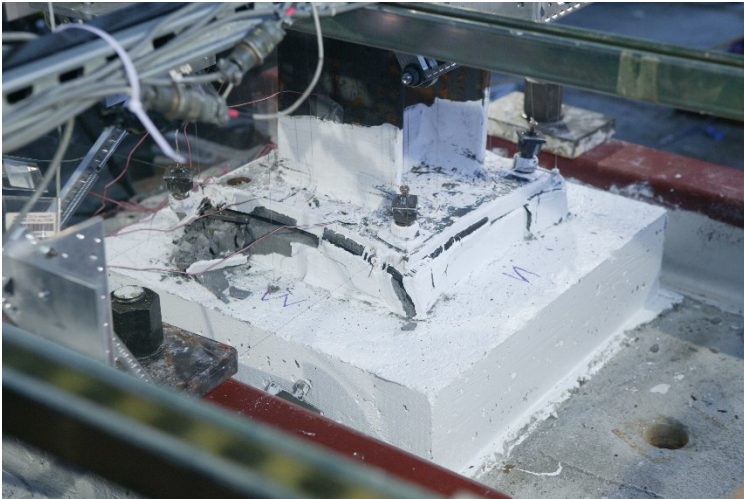


# Design Guide One approach

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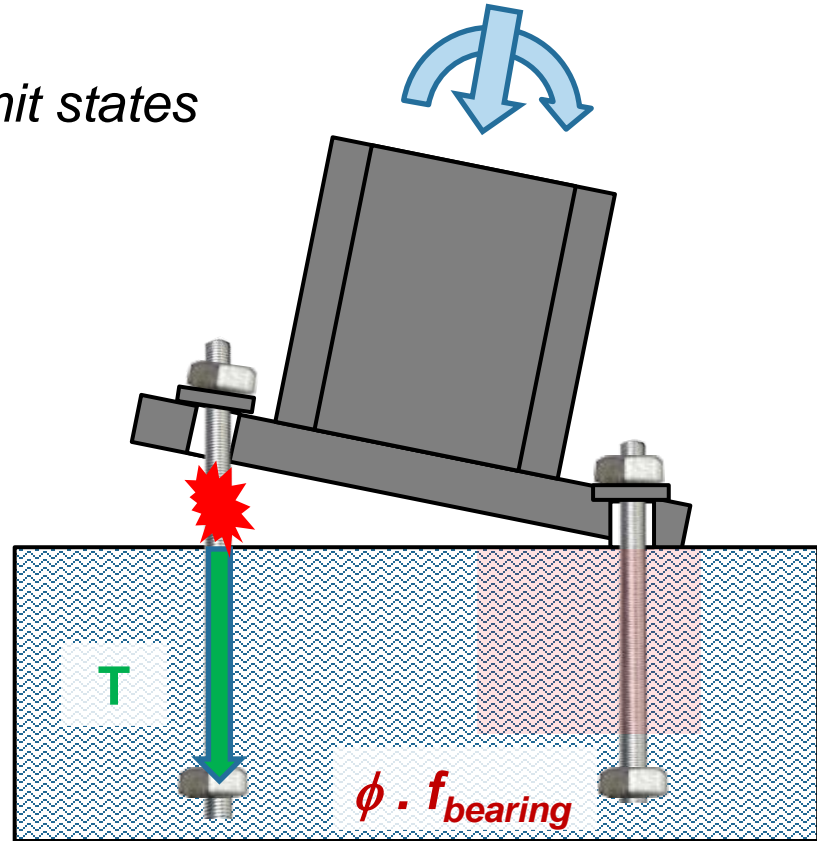
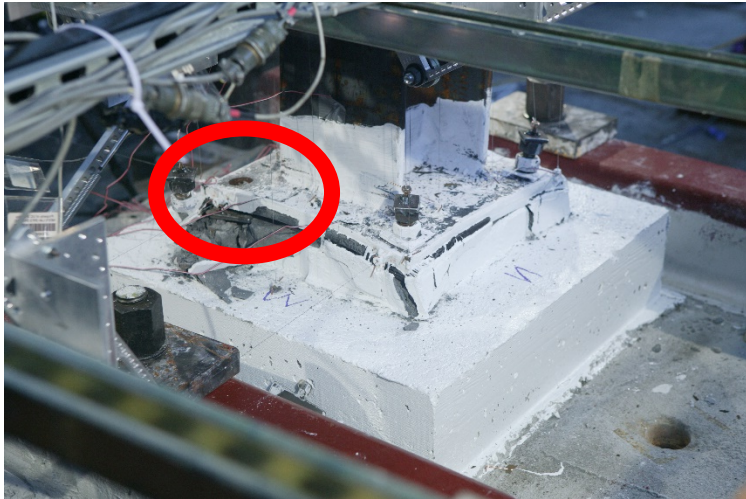


# Design Guide One approach

*STEP 2 – Given  $Y$  and  $T$ , evaluate limit states*

- Yielding or failure of the anchors

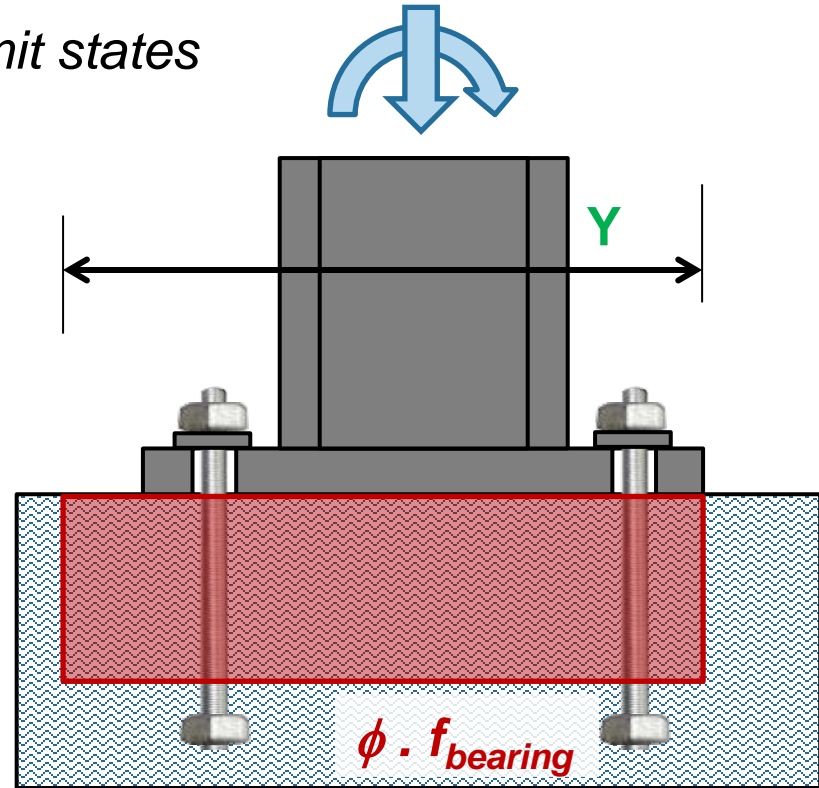
$$T < \phi \cdot T_{rod} (\phi = 0.9)$$



# Design Guide One approach

*STEP 2 – Given  $Y$  and  $T$ , evaluate limit states*

- Bearing failure of footing (implicit check)
- Bearing stress over plate footprint cannot accommodate compression
- Resize the plate plan dimensions



# Design checks

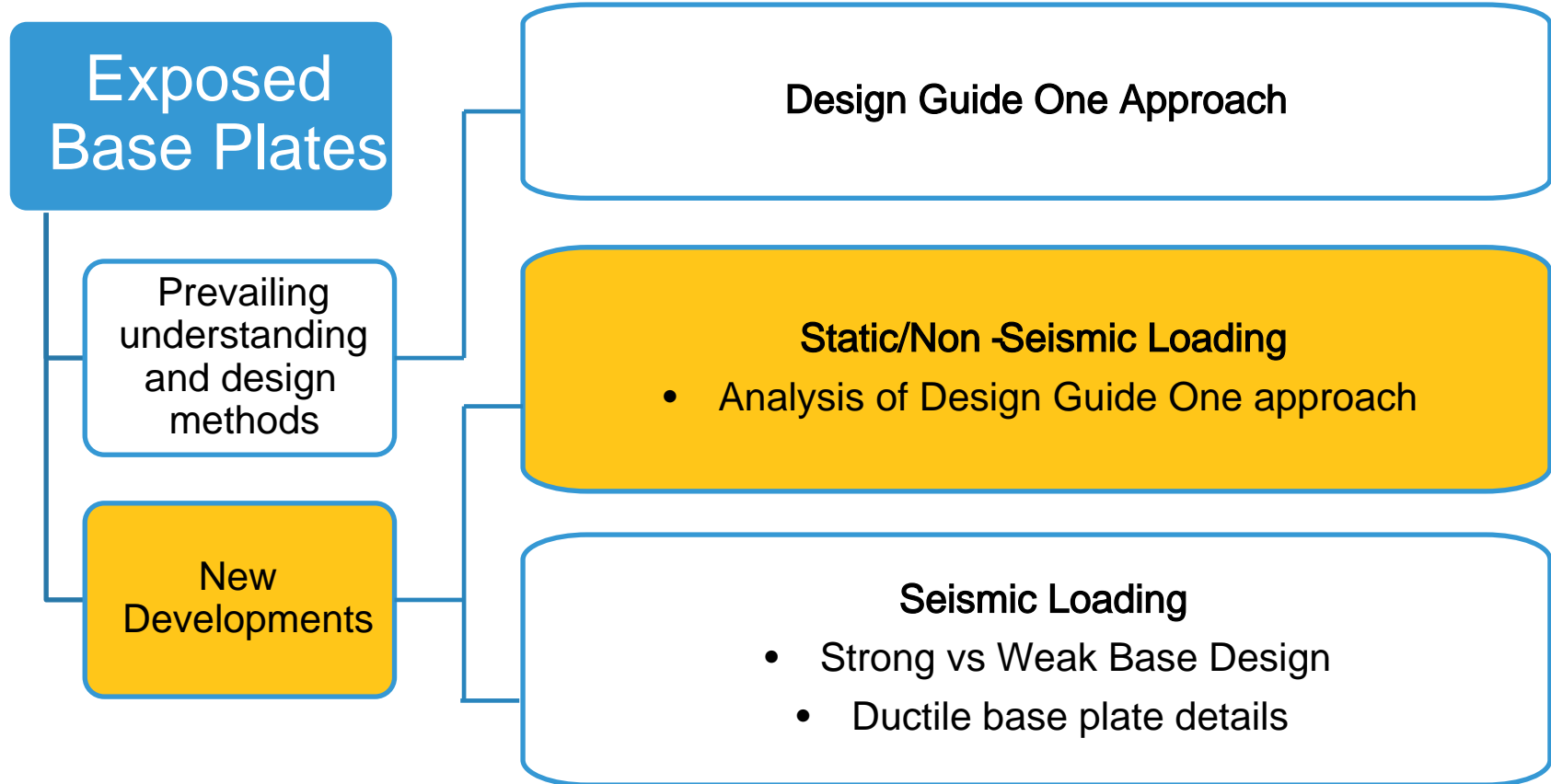
*STEP 2 – Given  $Y$  and  $T$ , evaluate limit states*

- Base plate yielding on compression side
- Base plate yielding on tension side
- Anchor rod yielding
- Bearing failure of footing (implicit)



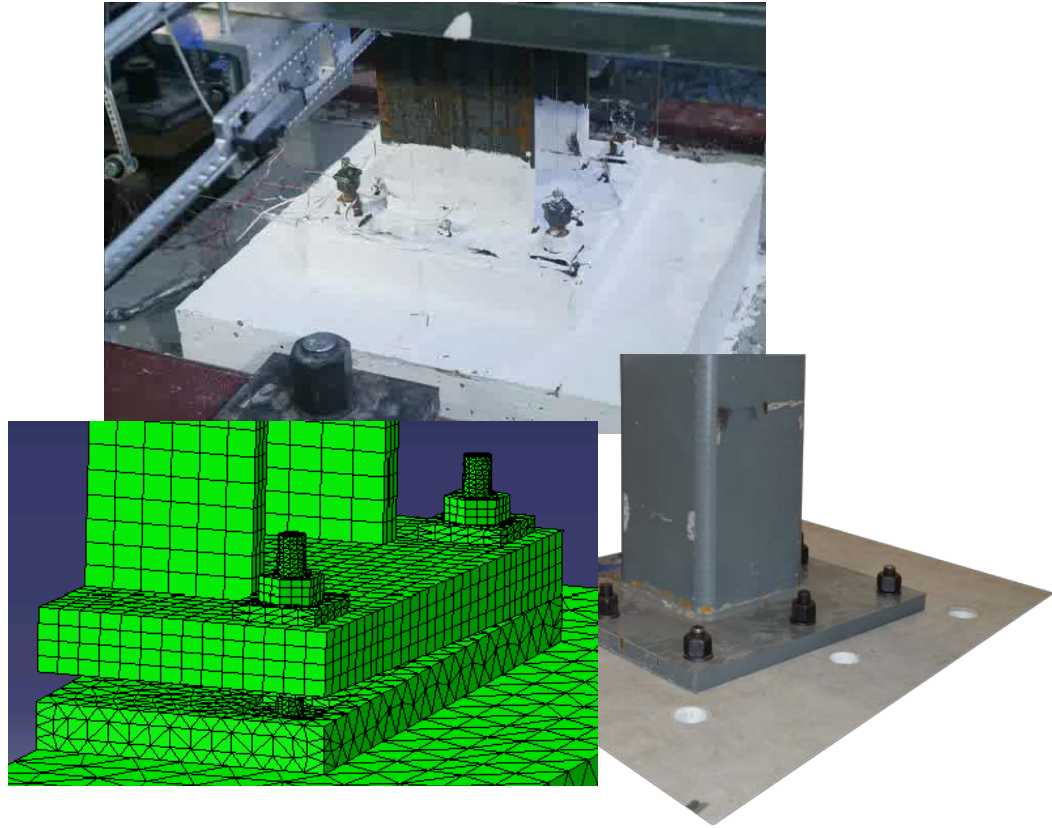


# Part 1 – Exposed Base Plate Connections

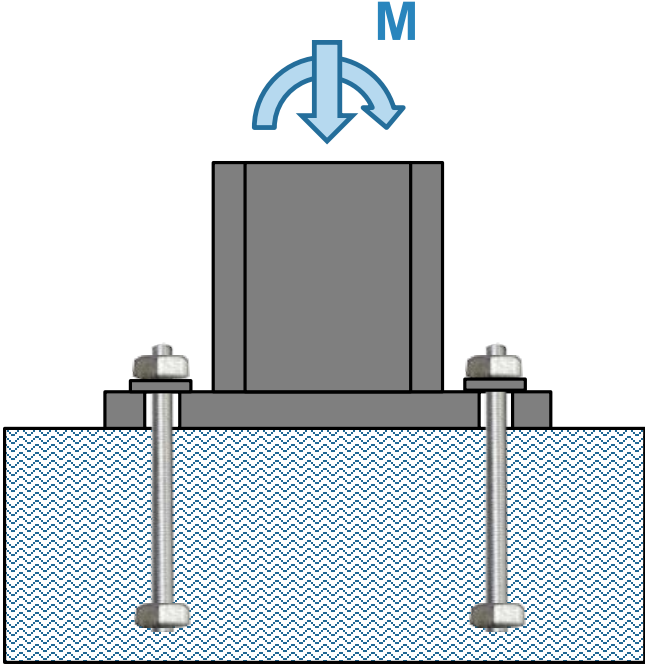
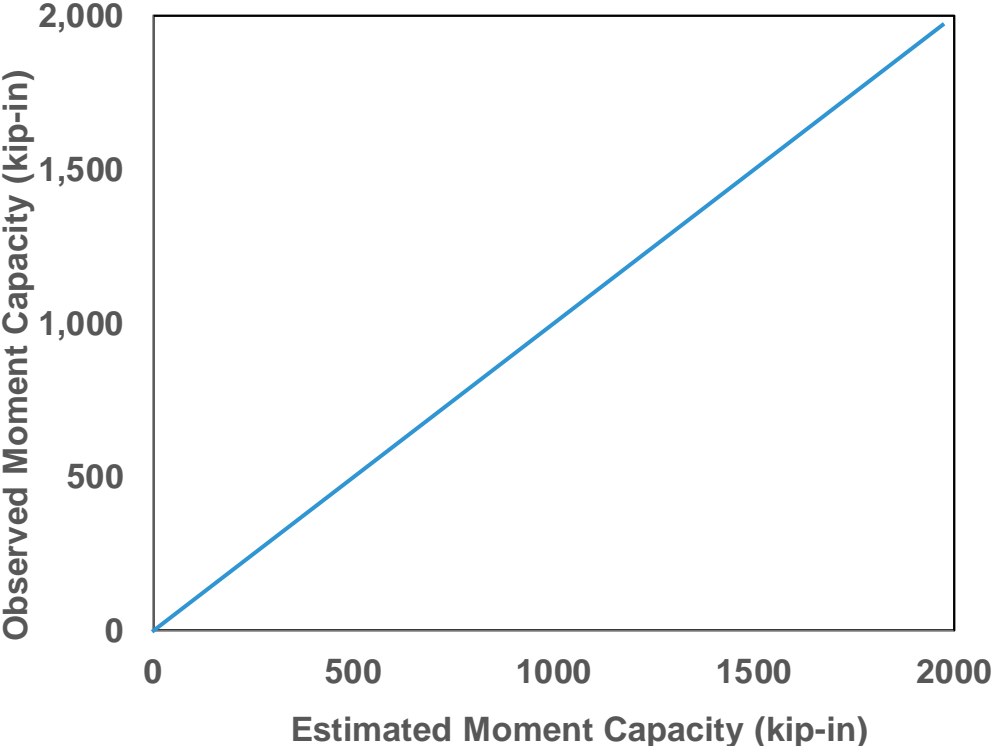


# Research in the last 15 years

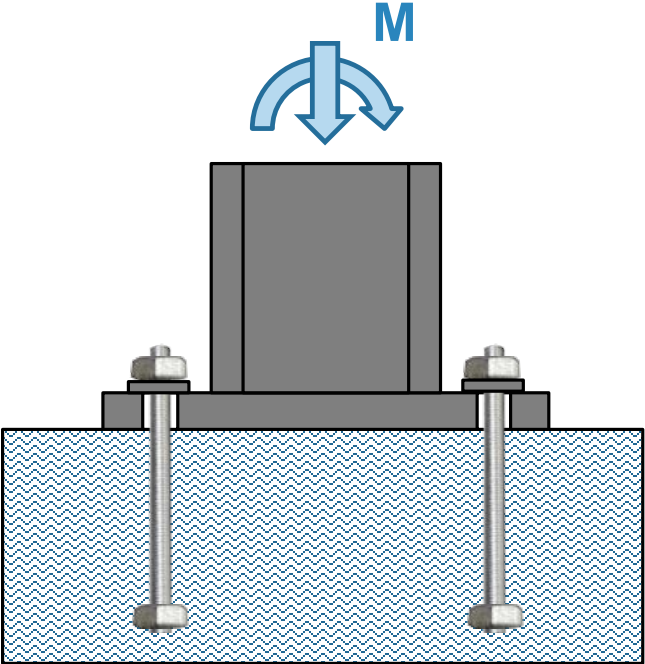
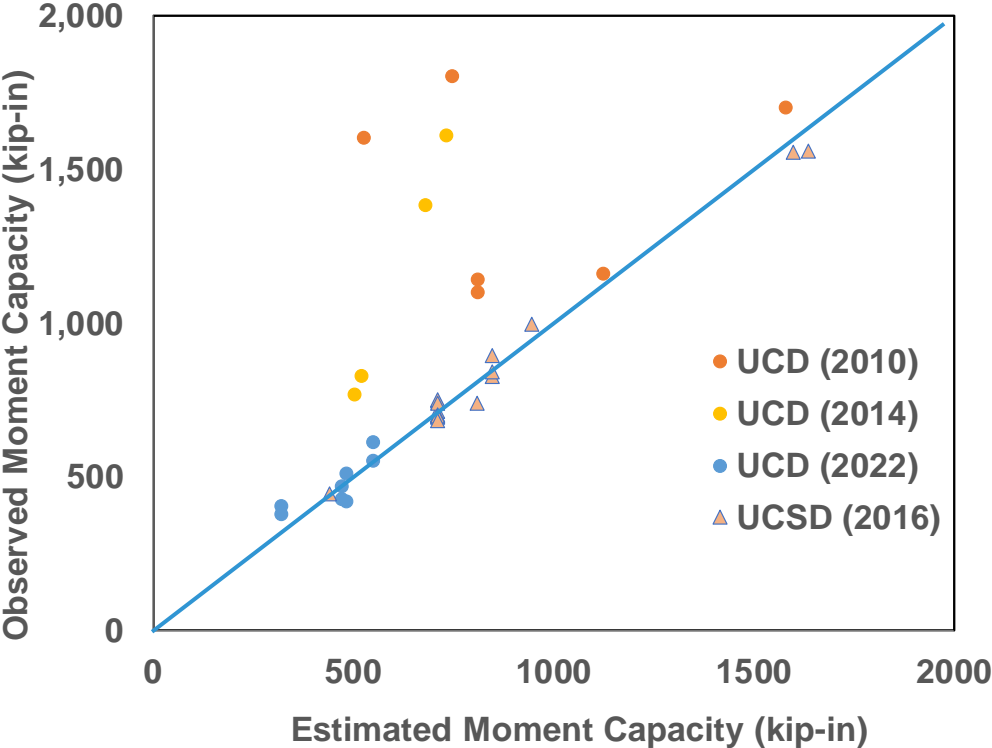
- Many Experiments (34 large scale tests at UCD)
- Finite element and line based simulations
- Monte-Carlo based Reliability analysis



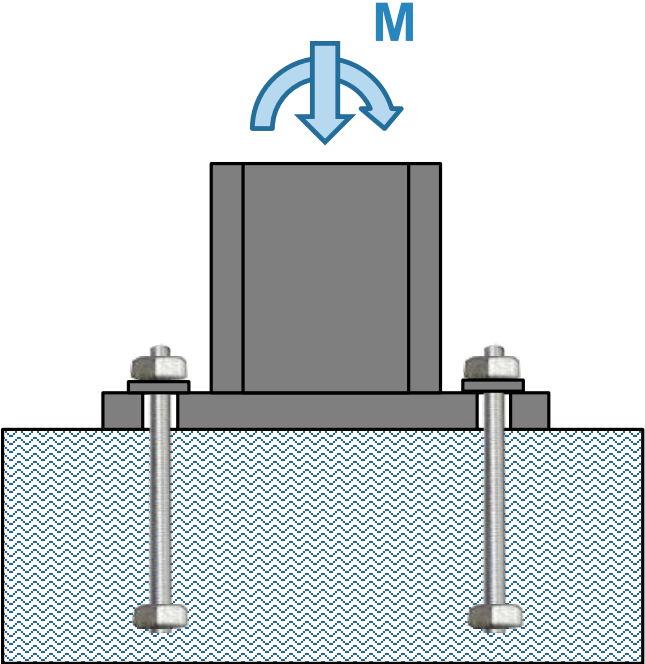
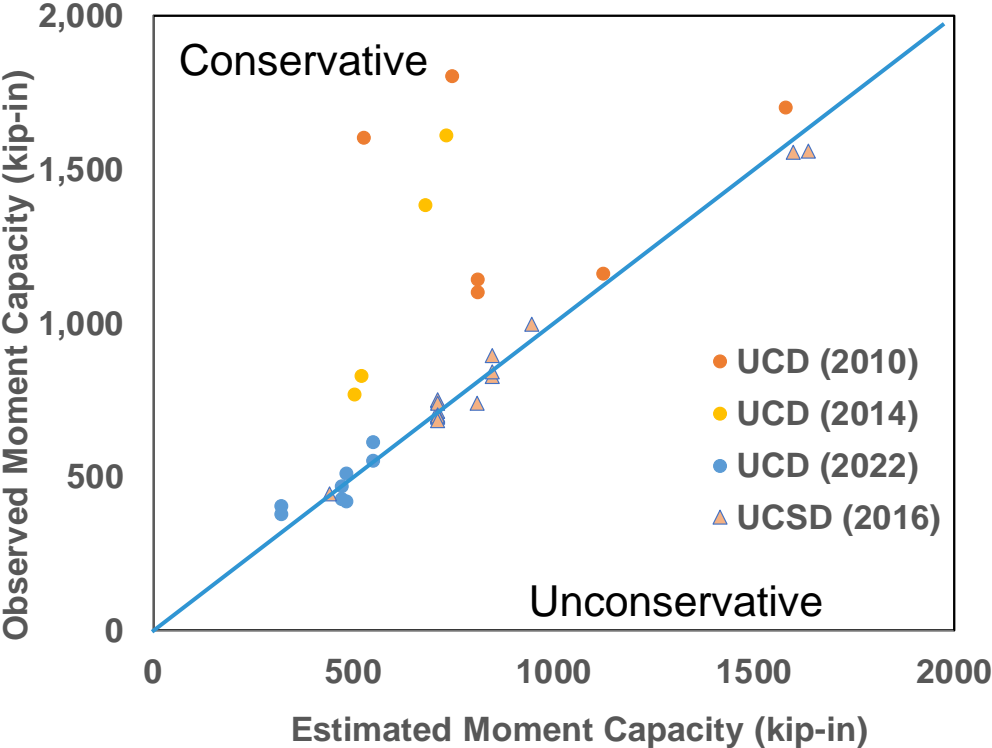
# Strength estimation based on Design Guide One



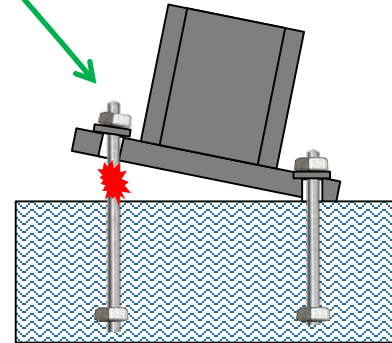
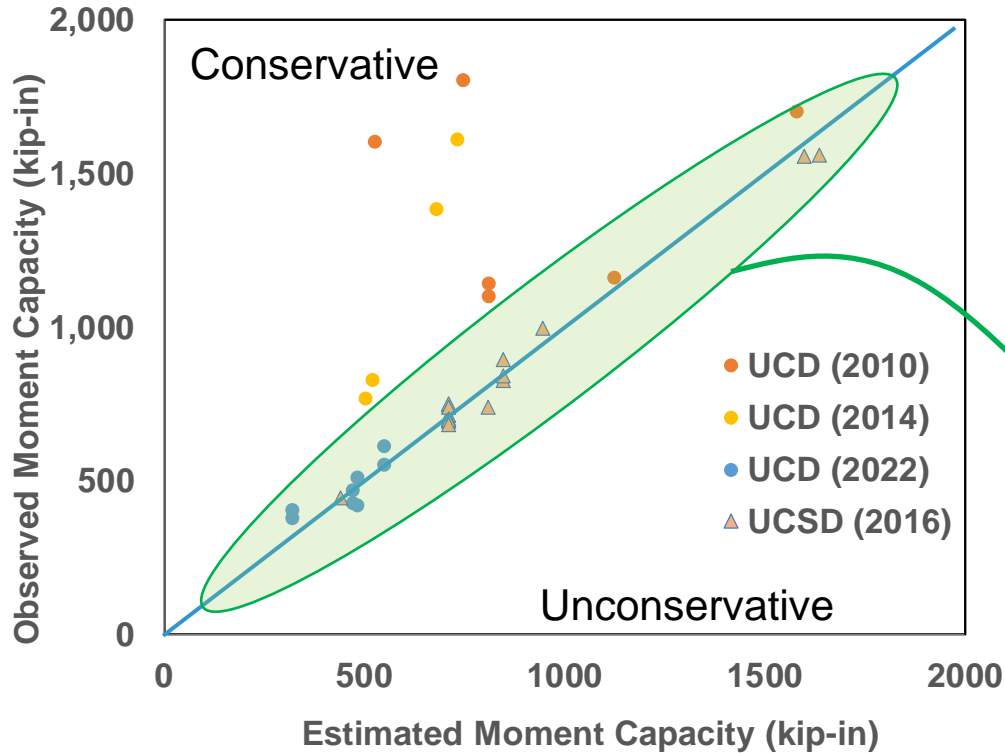
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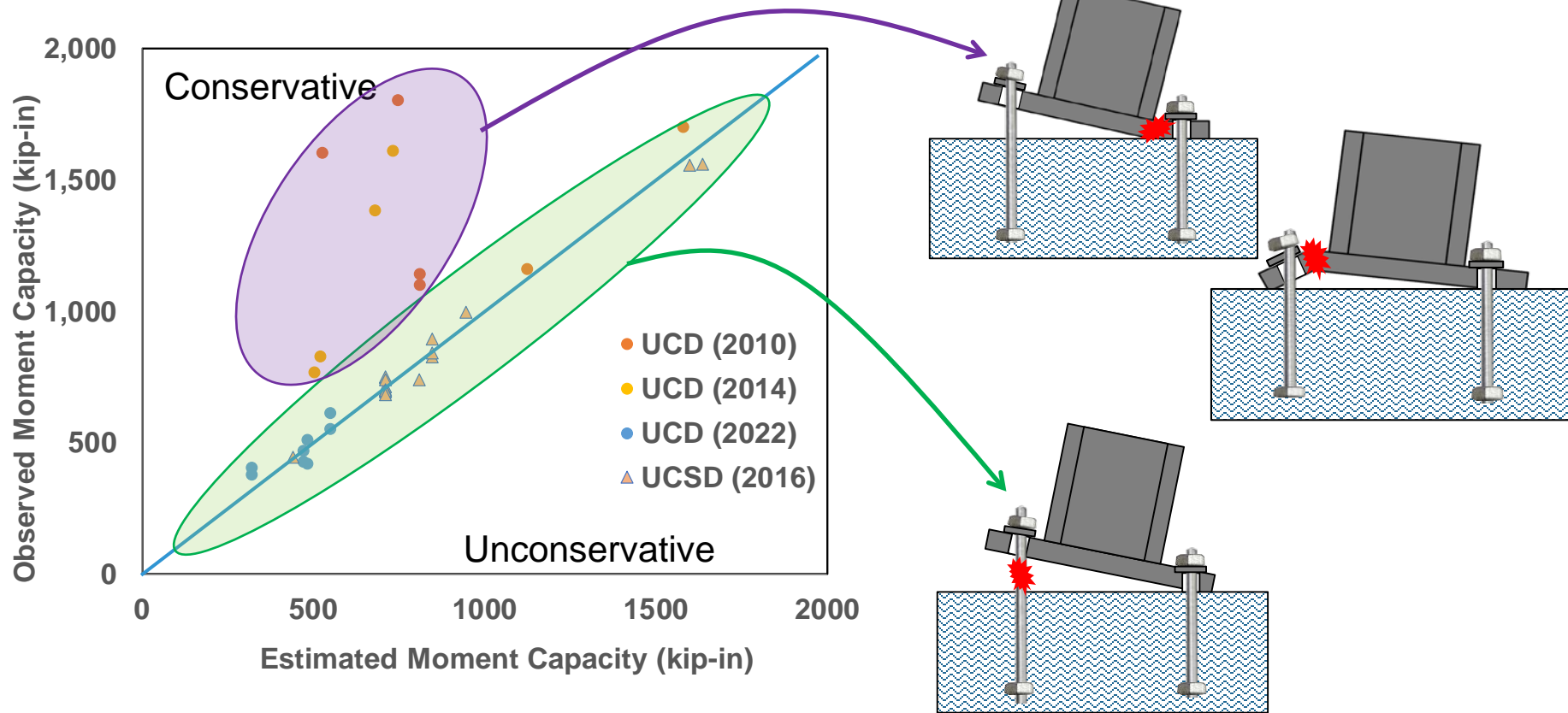
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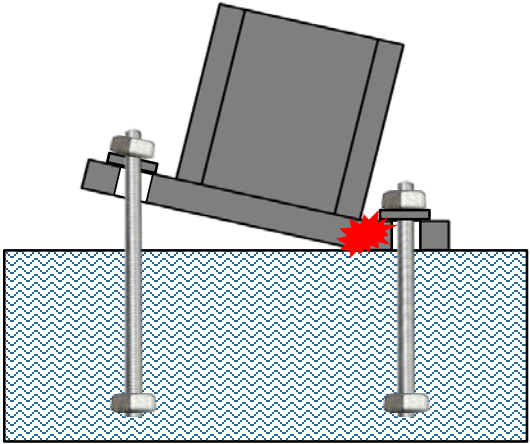
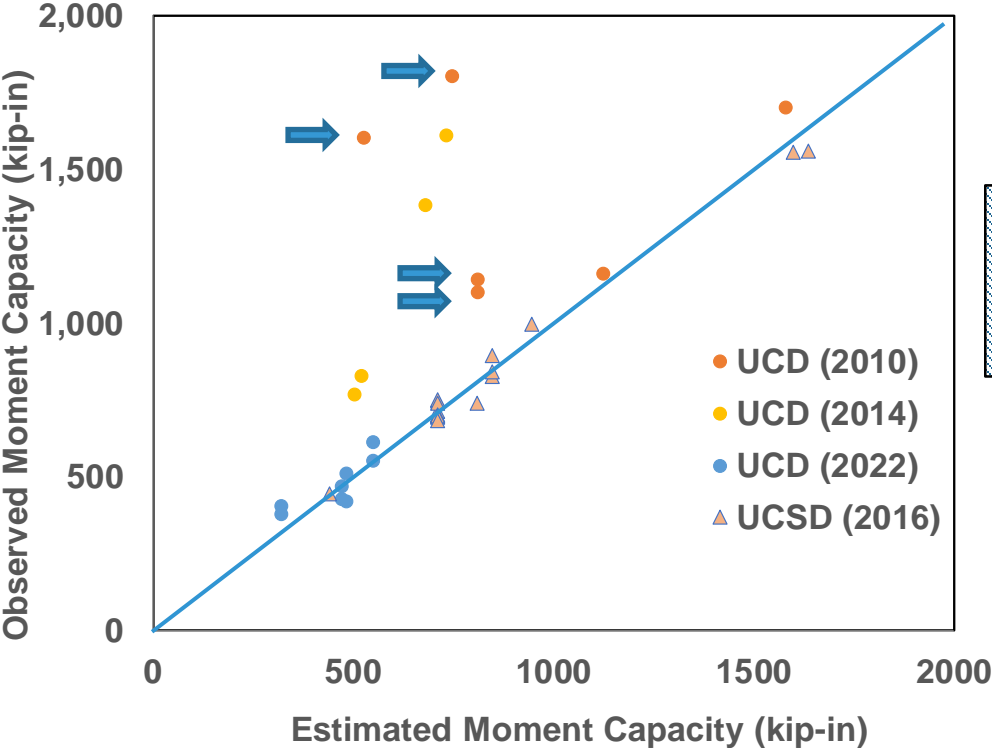
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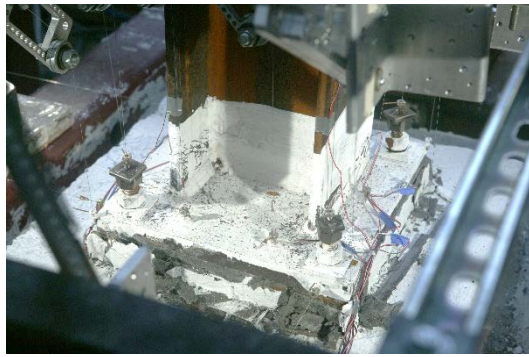
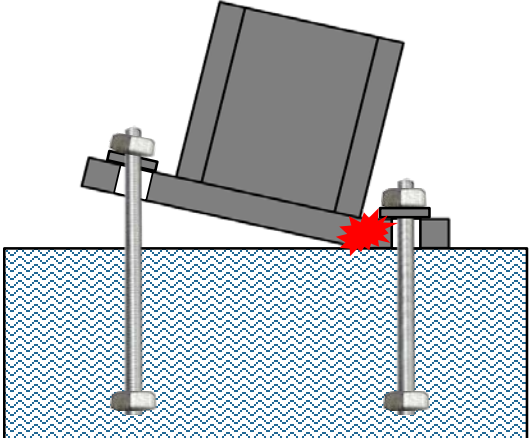
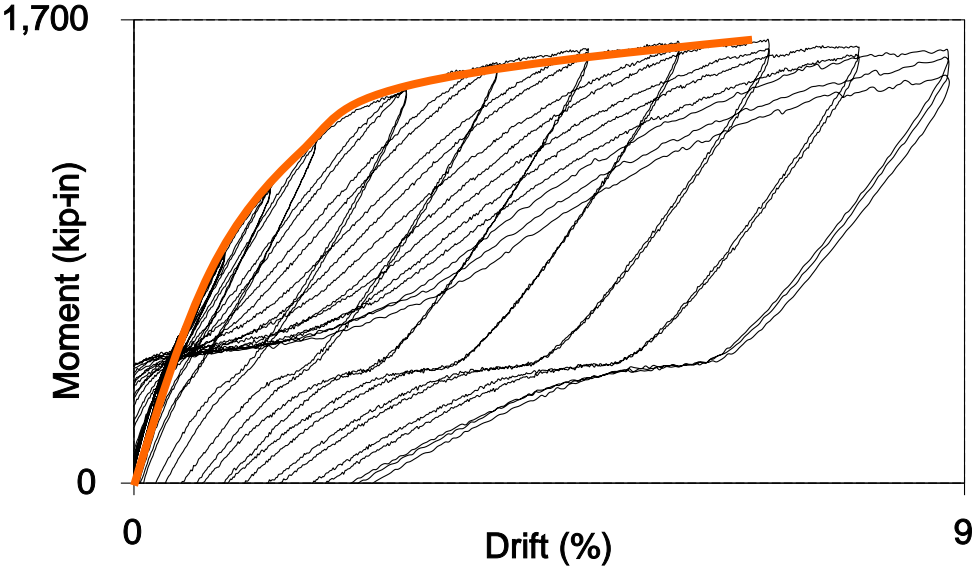


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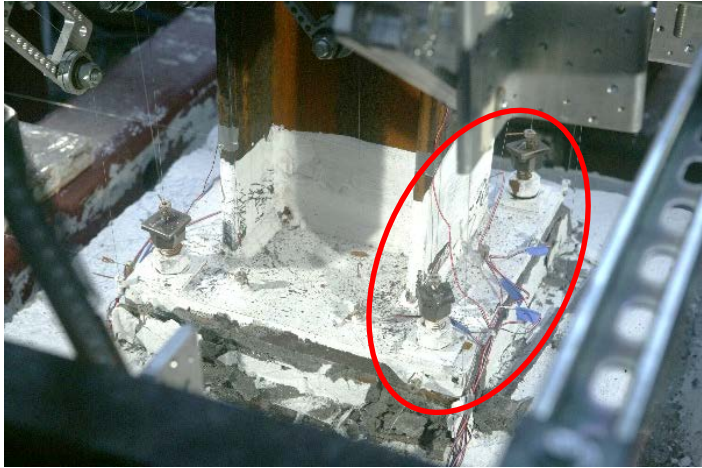
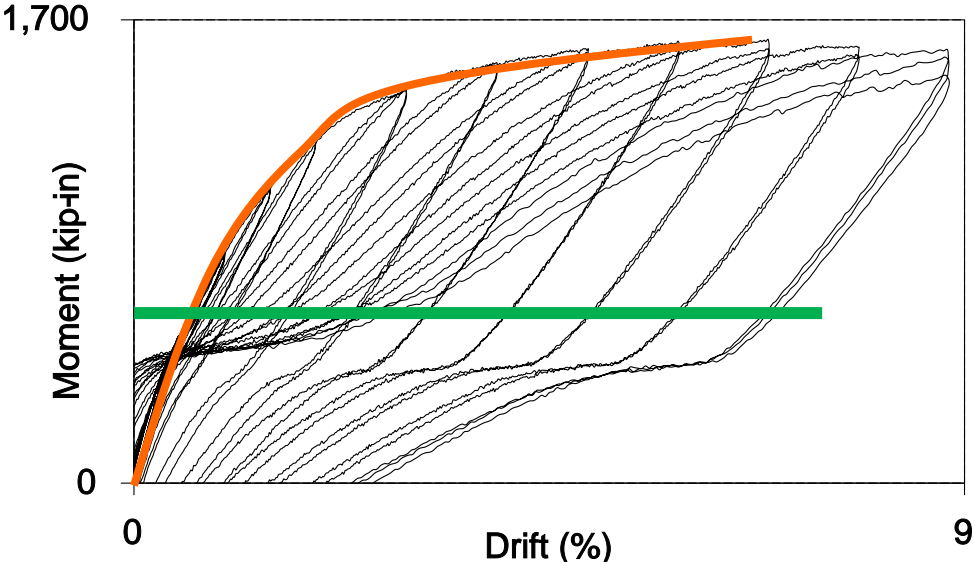




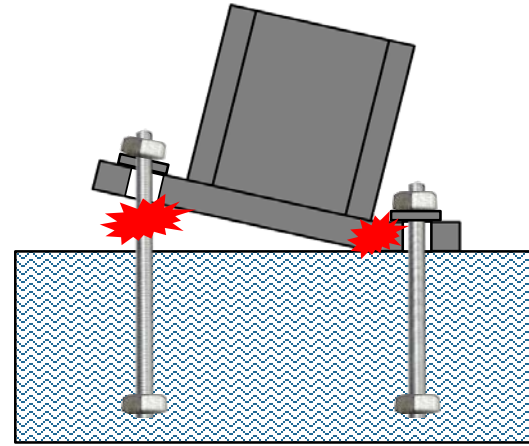
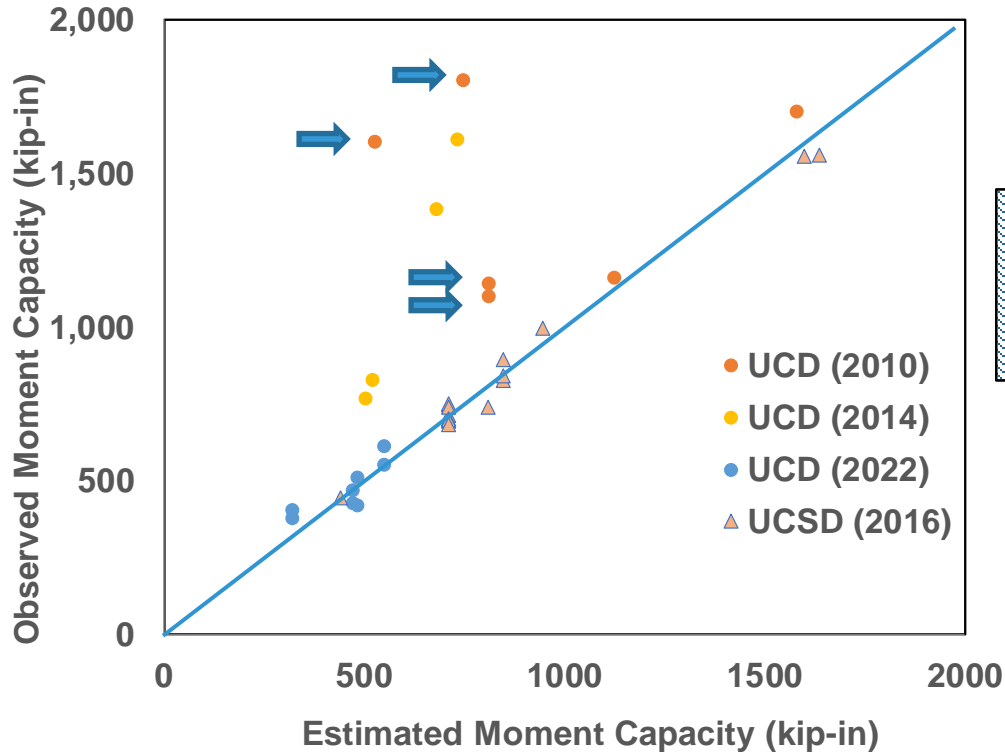
# Plate bending on compression side not consequential



# Plate bending on compression side not consequential

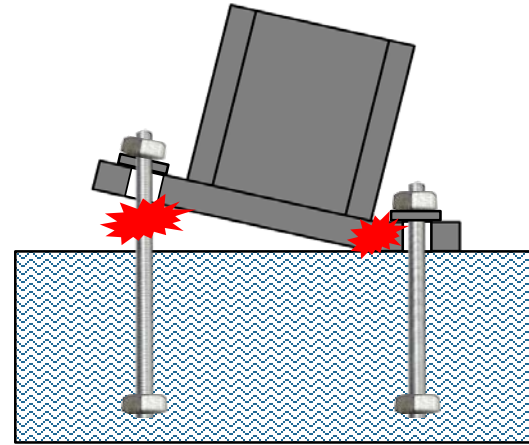
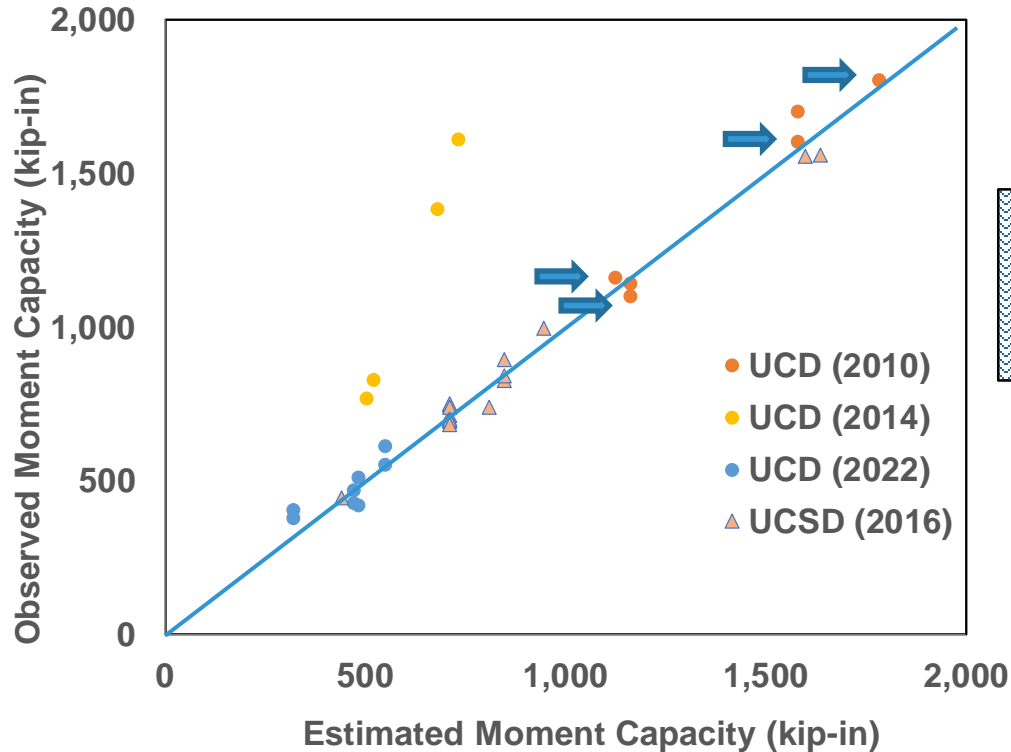


# Plate bending on compression side not consequential



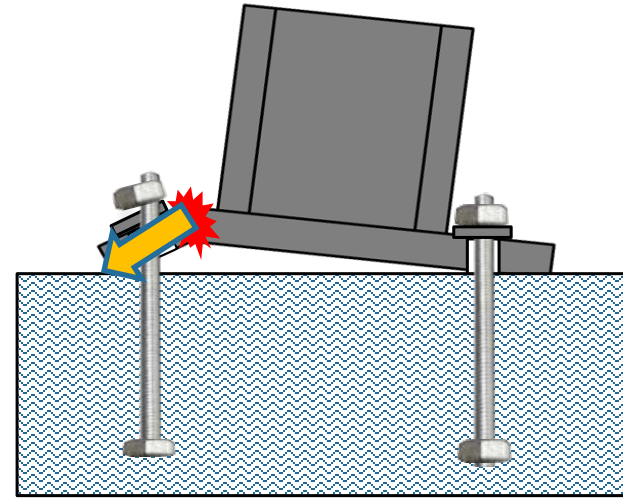
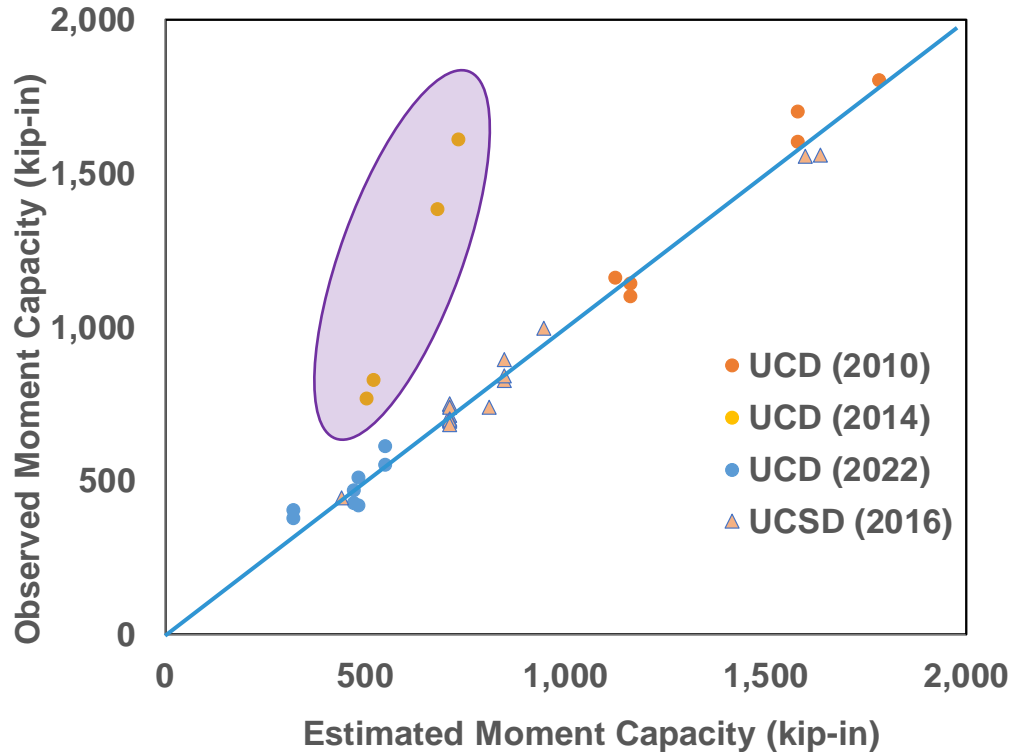
- Compression side yielding did not result in reaching capacity
- Tension side limit state needed

# Plate bending on compression side not consequential



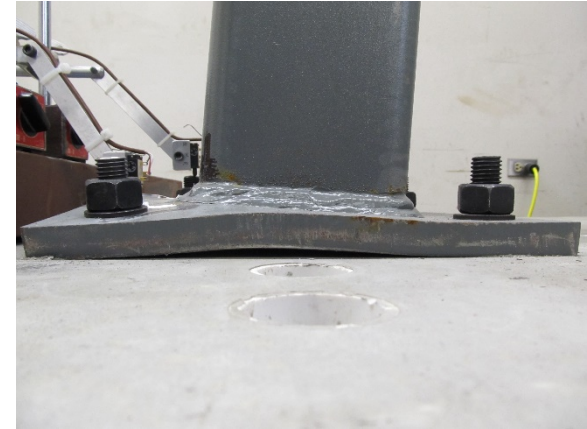
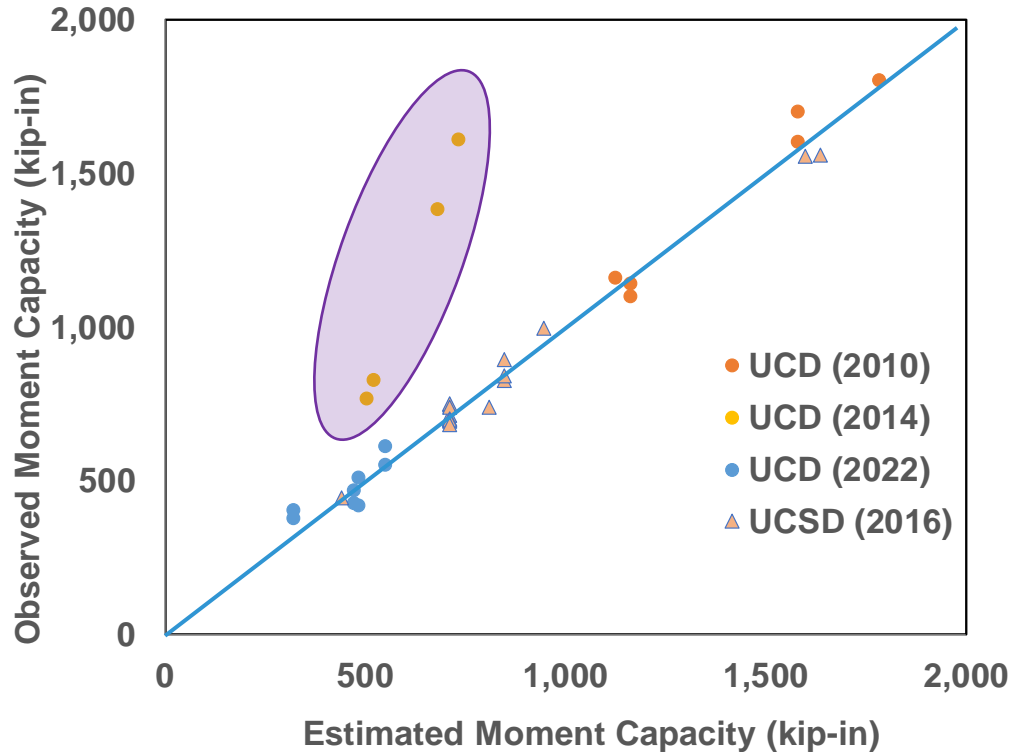
- Determination of a mechanism load addresses this

# Plate bending on tension side



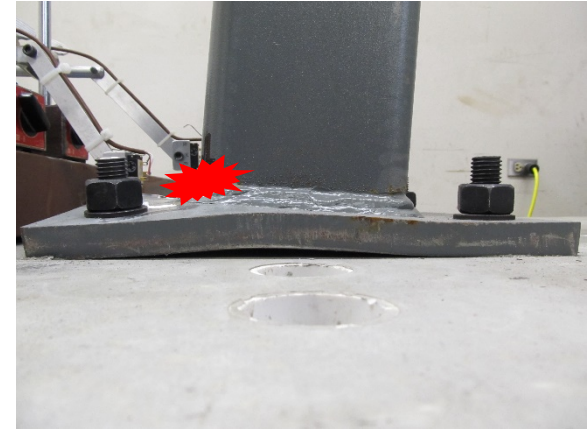
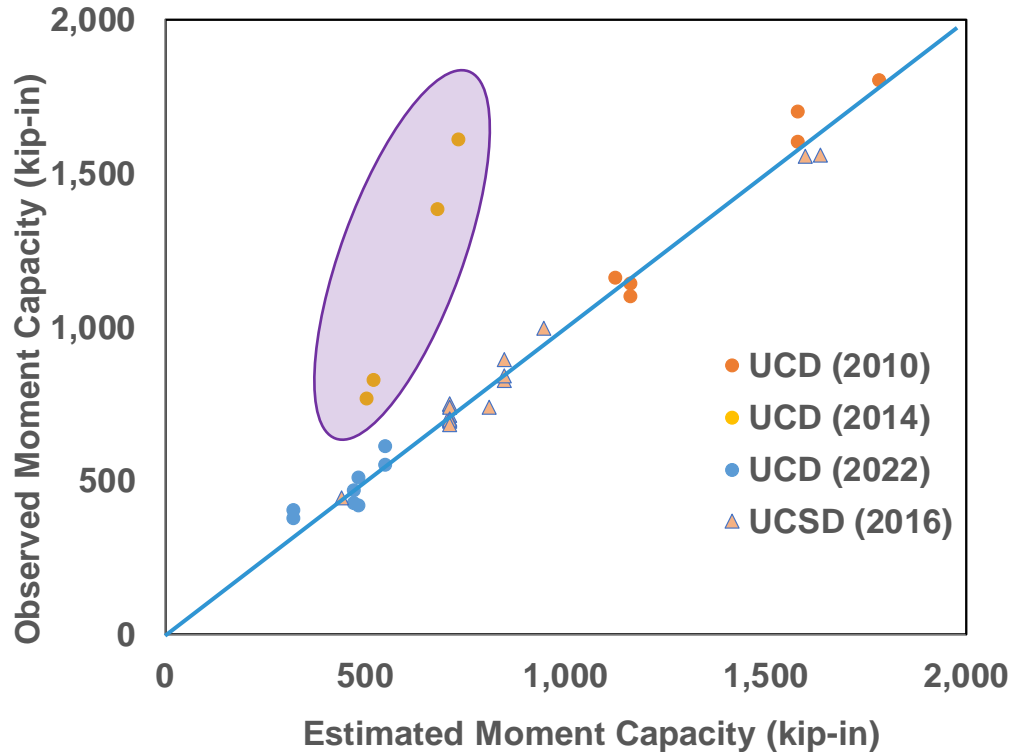
- No eventual yielding of rods
- Strength increase due to membrane action

# Plate bending on tension side



- No eventual yielding of rods
- Strength increase due to membrane action
- Fracture

# Plate bending on tension side



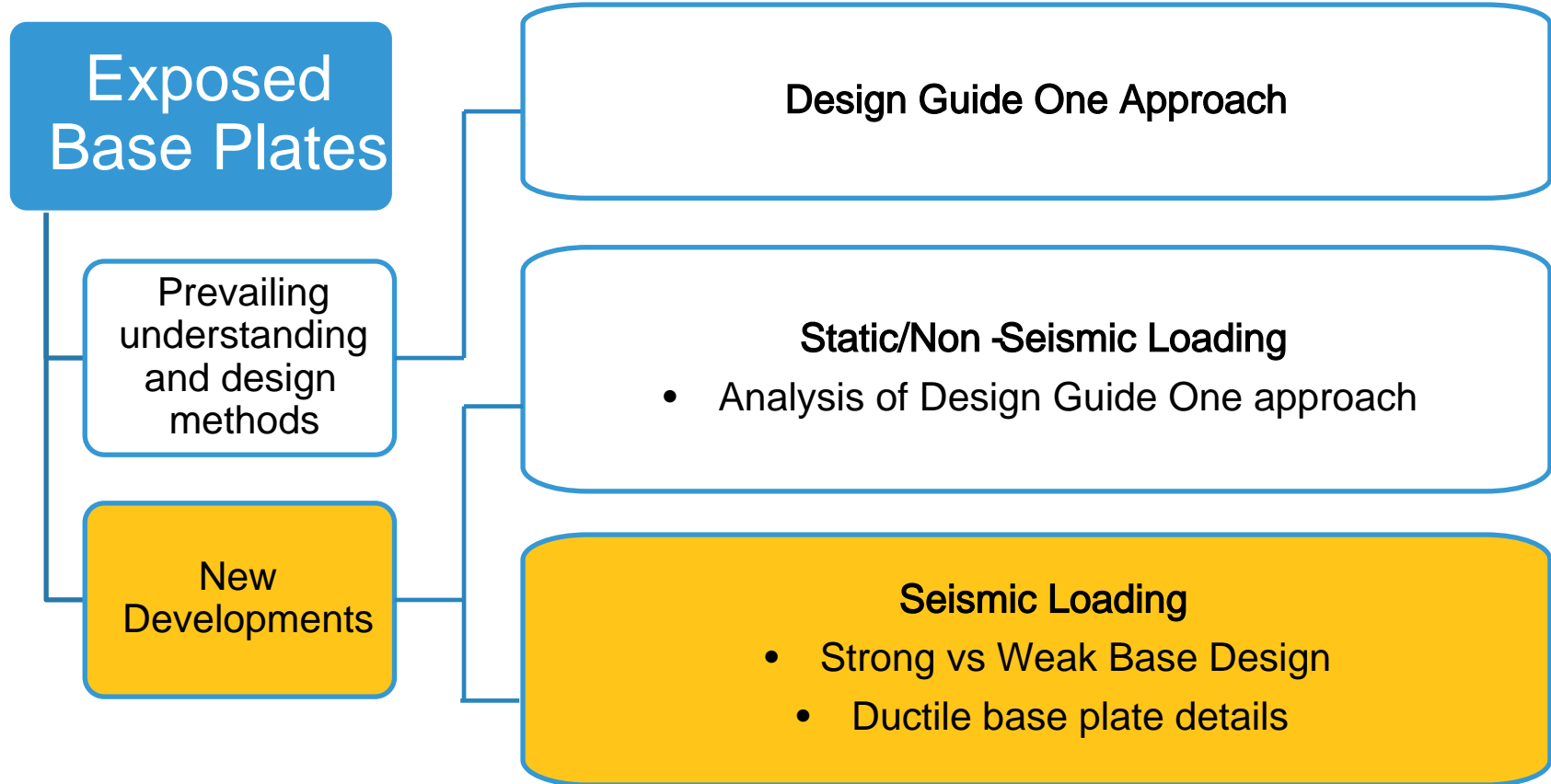
- No eventual yielding of rods
- Strength increase due to membrane action
- Fracture

# Summary– Design Guide One

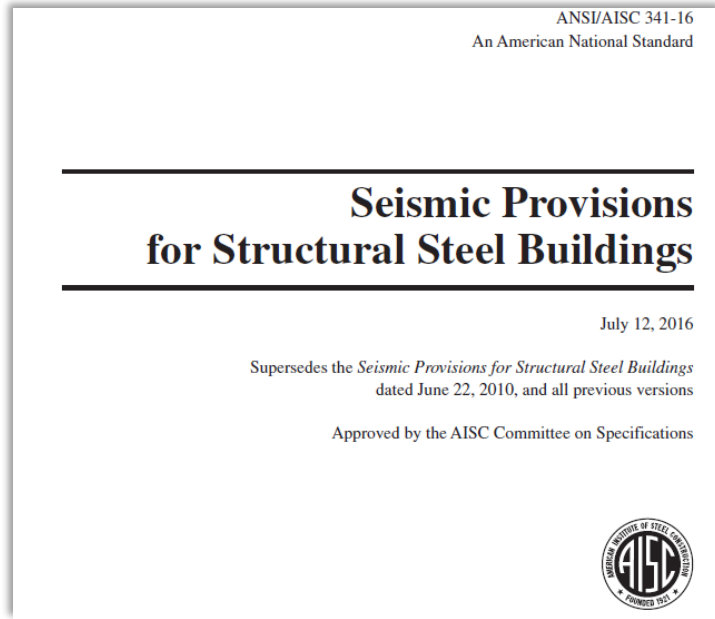
- Fairly accurate for strength characterization
- Conservative when platebending controls
- Scope does not include
  - Seismic connections
  - Embedded connections
  - Modeling



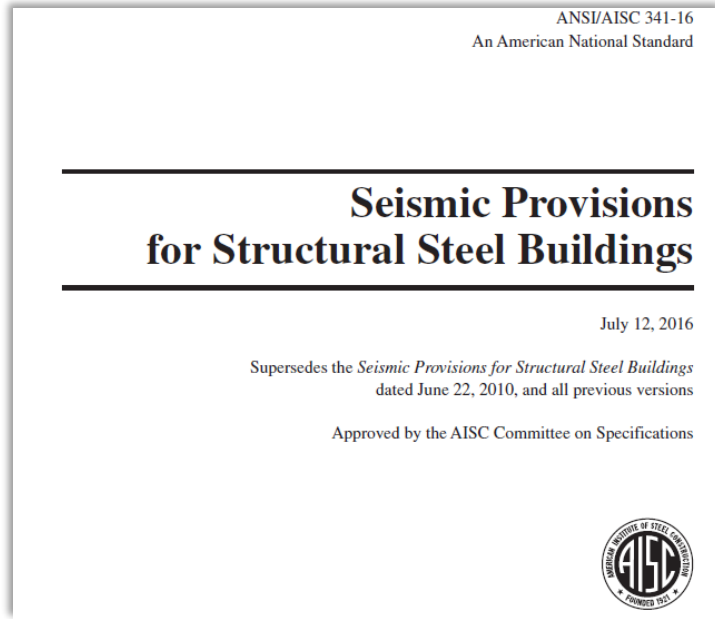
# Part 1 – Exposed Base Plate Connections



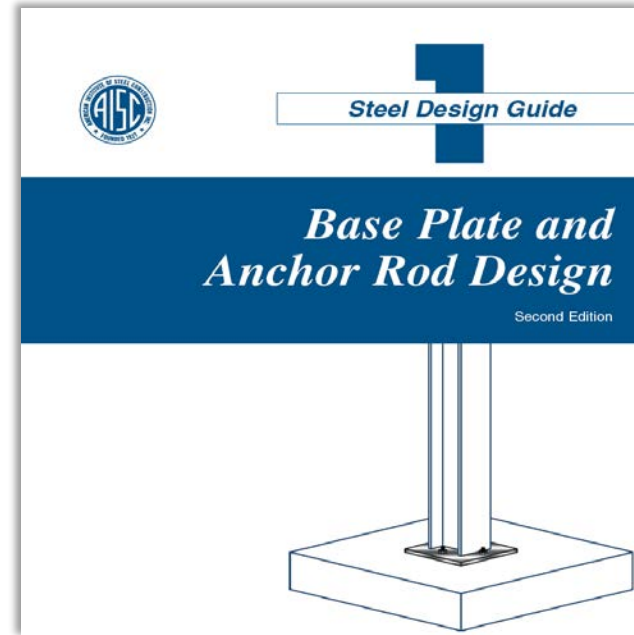
# Seismic considerations— exposed base plates



# Seismic considerations— exposed base plates



Broad principles  
and philosophy



Design and detailing

# Seismic considerations— exposed base plates

ANSI/AISC 341-16  
An American National Standard

## Seismic for Structural Steel

Supersedes the *Seismic Provisions*  
dated June 15, 2010  
Approved by the American Institute of Steel Construction, Inc.

Broad principles  
and philosophy

### 6c. Required Flexural Strength

Where column bases are designed as moment connections to the foundation, the required flexural strength of column bases that are designated as part of the SFRS, including their attachment to the foundation, shall be the summation of the required connection strengths of the steel elements that are connected to the column base as follows:

- (a) For diagonal braces, the required flexural strength shall be at least equal to the required flexural strength of diagonal brace connections.
- (b) For columns, the required flexural strength shall be at least equal to the lesser of the following:
  - (1)  $1.1R_yF_yZ/\alpha_s$  of the column; or
  - (2) The moment calculated using the overstrength seismic load, provided that a ductile limit state in either the column base or the foundation controls the design.

# Two ways to design seismic base connections

## Strong base design

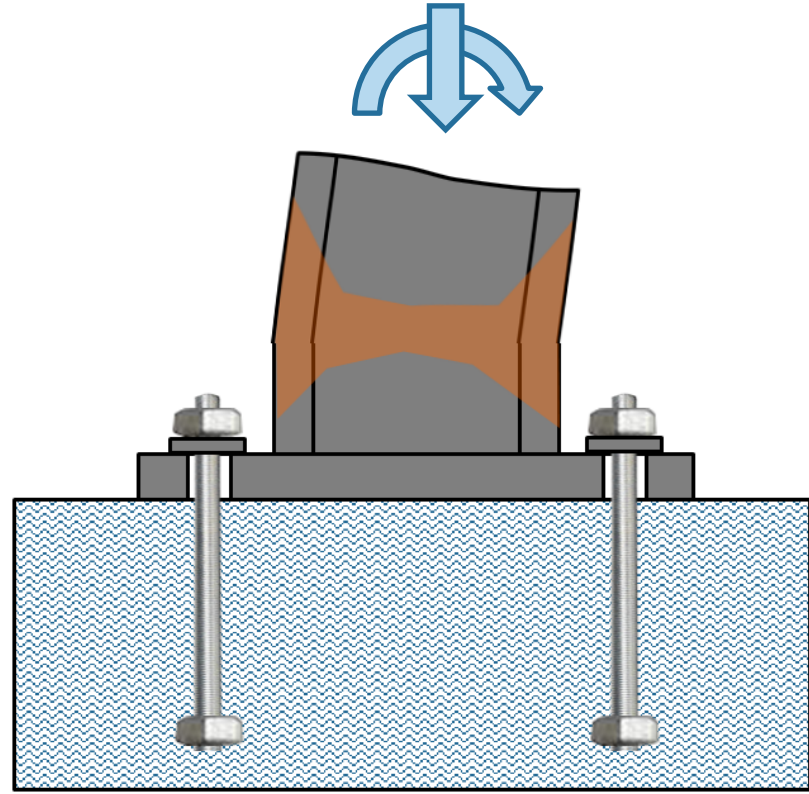
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# Strong base design

- Direct application of Design Guide One
- Large rods, thick plate



# Two ways to design seismic base connections

Weak base  
design using  $\Omega_0$   
loads

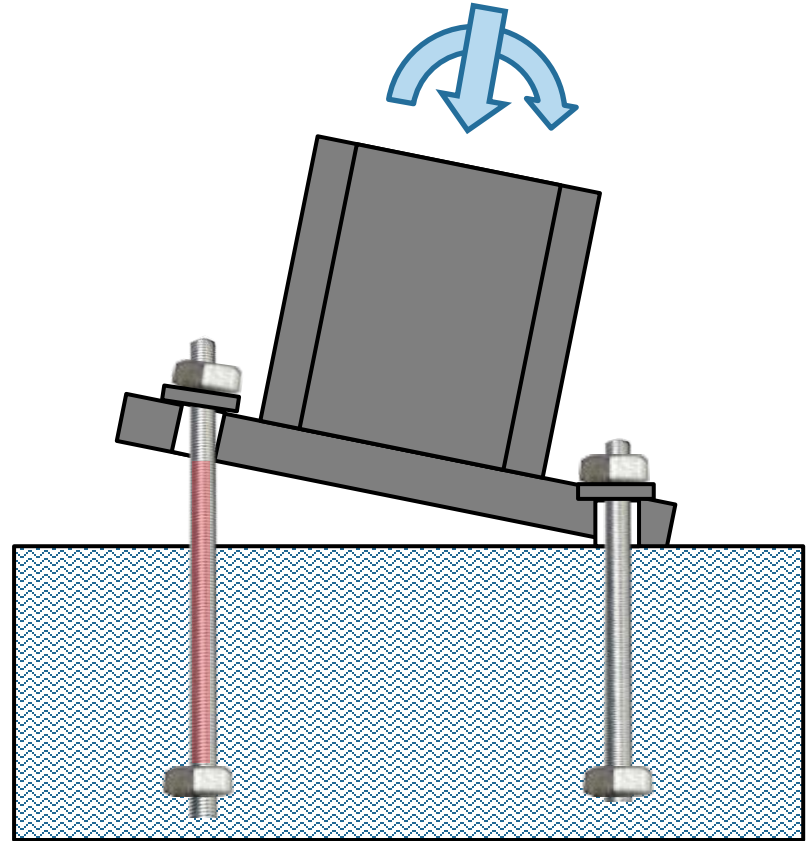
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# Weak base design

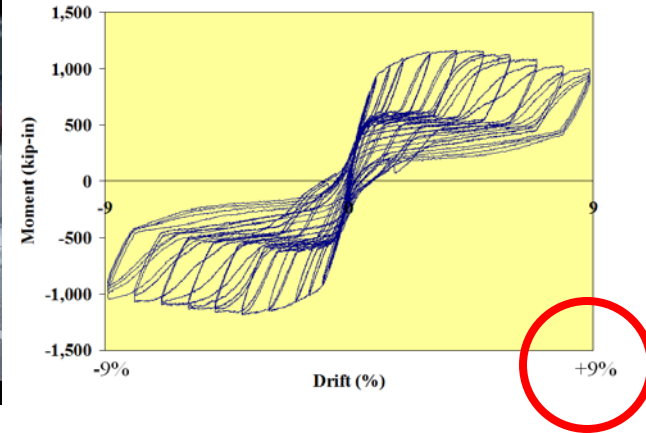
- Weak base design
- Cheaper connection
- Requires ductility
  - Limited specific guidance on how to achieve this





# Inherent ductility of exposed base connections

Great inherent ductility (rotation  $>5\%$ )



Gomez et al. (2010), Kanvinde et al. (2015), Trautner et al. (2017),  
Astaneh et al. (1992), Fahmy et al. (1999), Burda & Itani (1999), Lee et al. (2008) and Wald et al. (2020)

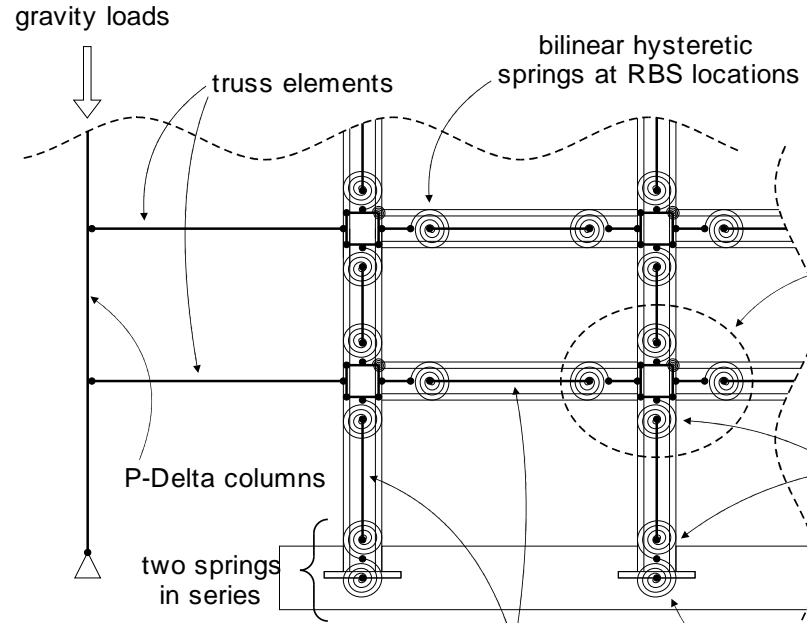
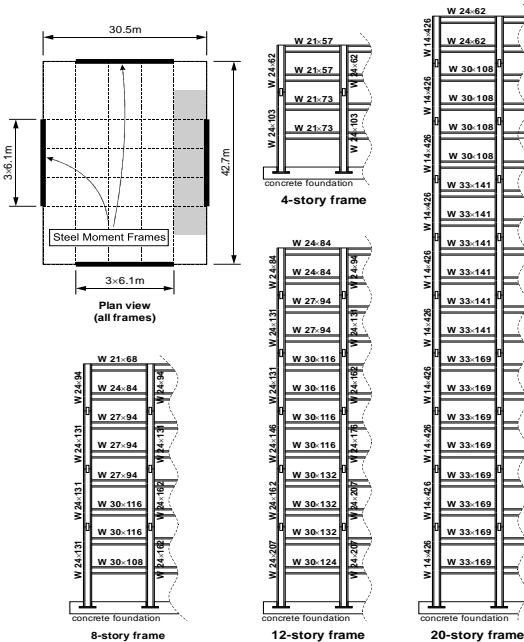
# How to achieve weak base design?

- Develop understanding of base rotation demands
- Engineer details that can meet these demands, with confidence
- Demonstrate effectiveness of these details



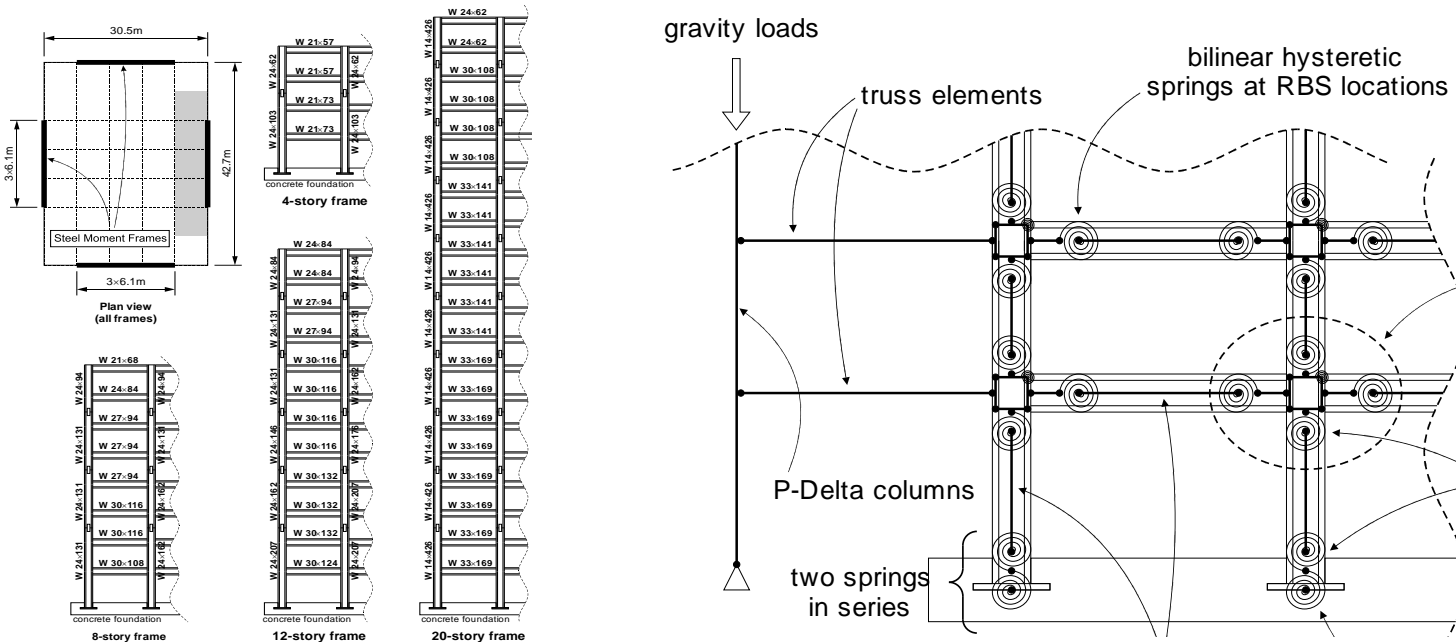
# How to achieve weak base design?

Rotation in the range of 45% provides great performance



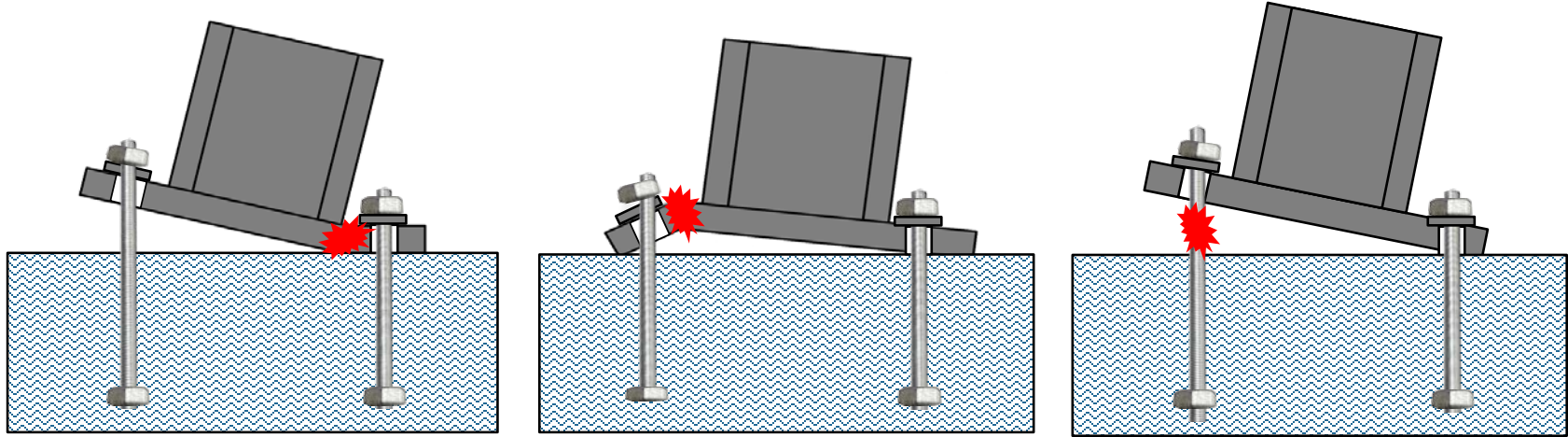
# How to achieve weak base design?

## Weak-base design is well within reach

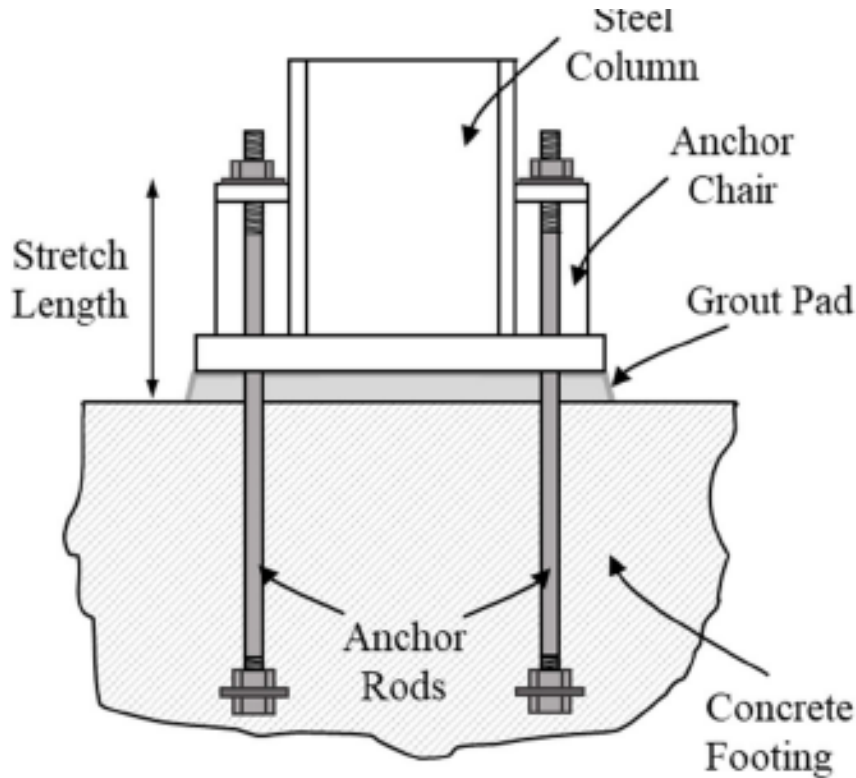


# Engineering such a connection

Which ductile mode to use?



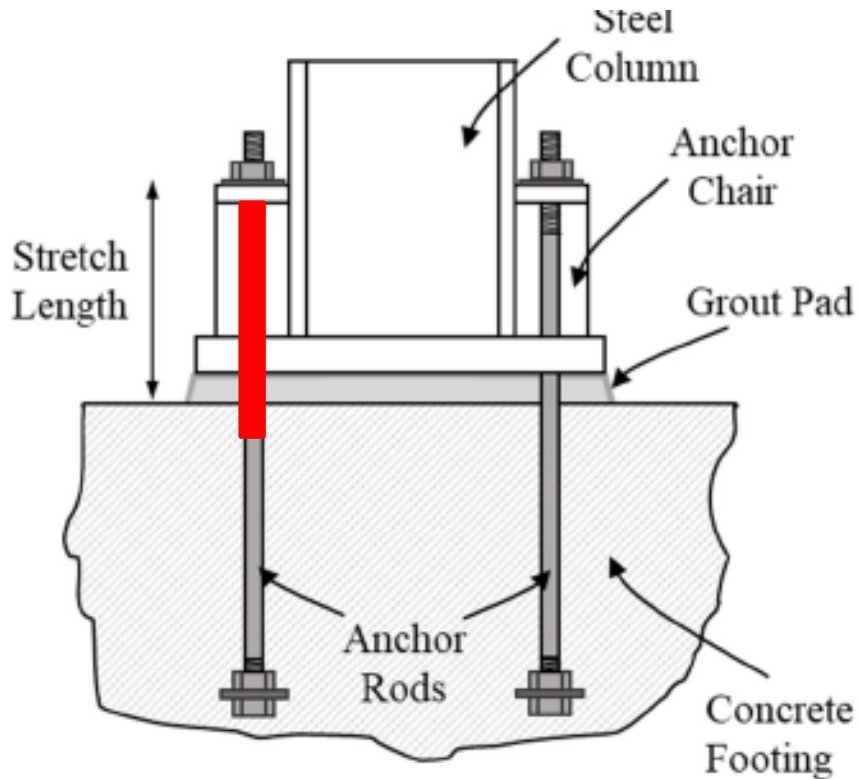
# Ductile base connections through rod elongation



- Good performance observed under high shaking
- Attributed to stretch length

Soules et al (2016)

# Ductile base connections through rod elongation



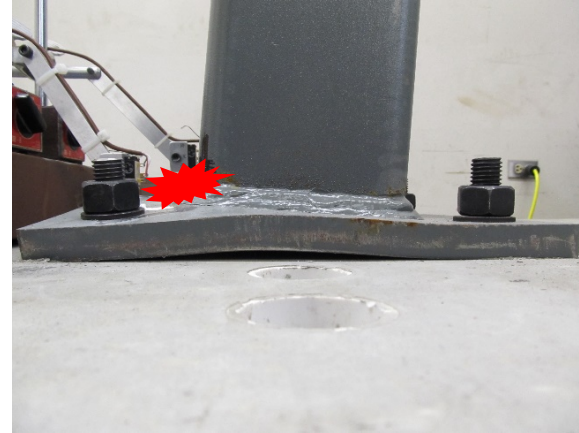
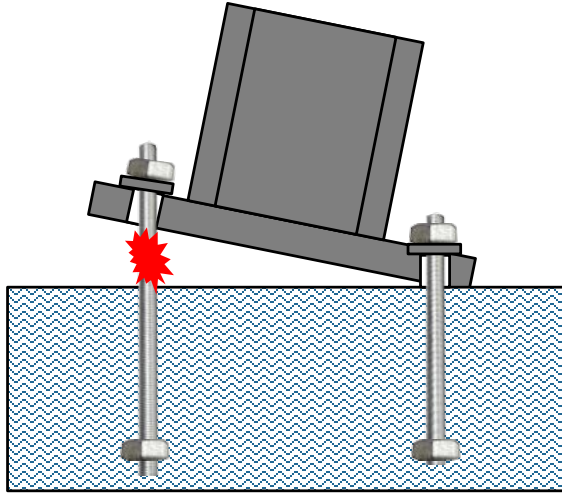
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Soules et al (2016)



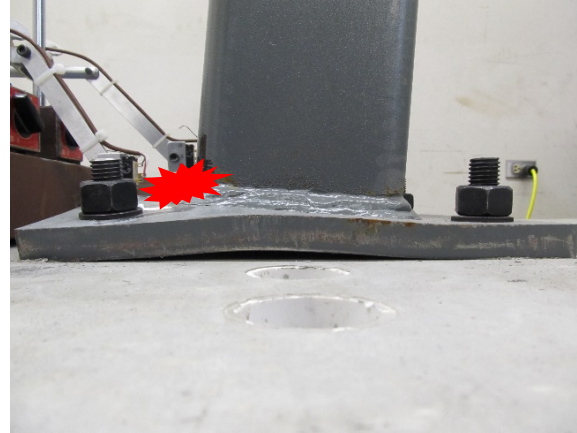
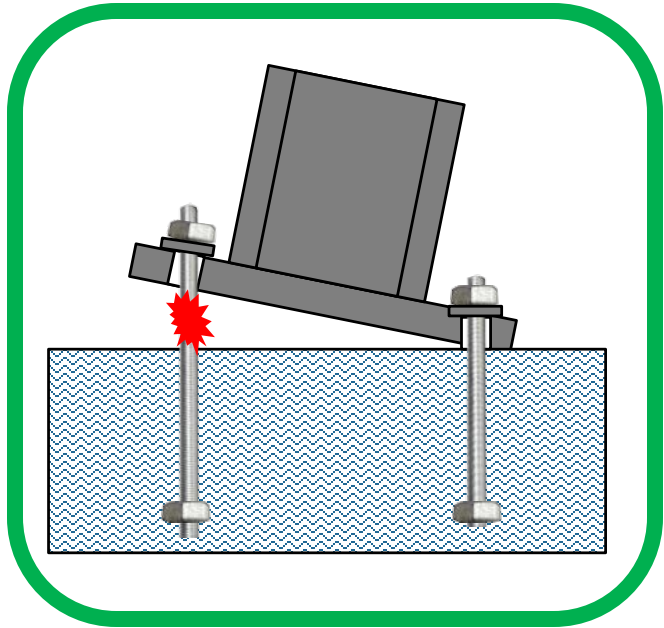
# Achieving ductility in base connections

Consensus around rod elongation vs base plate yielding

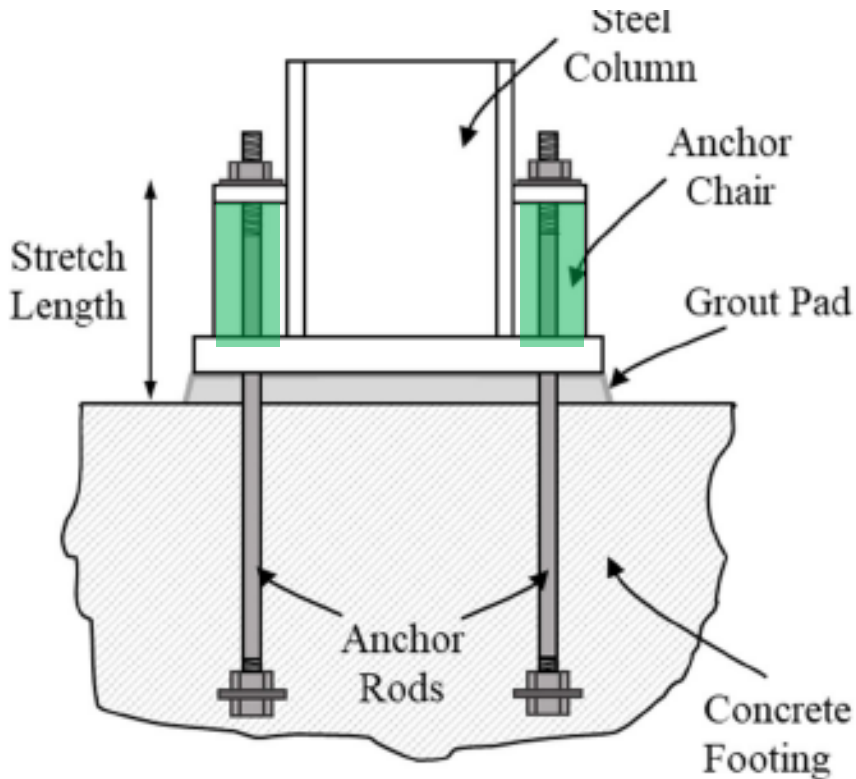


# Achieving ductility in base connections

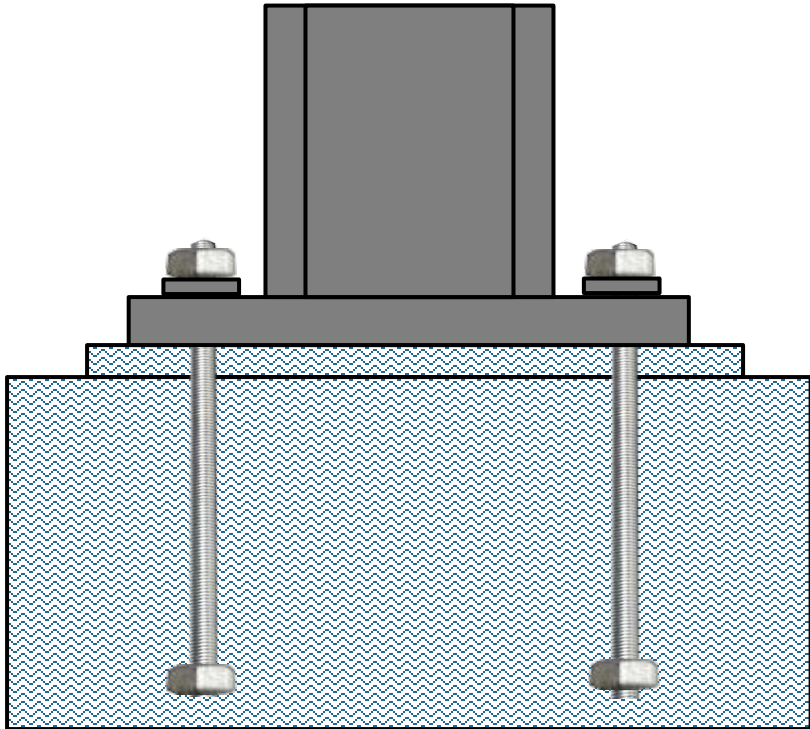
Consensus around rod elongation vs base plate yielding



# Stretchlength requires additional fabrication

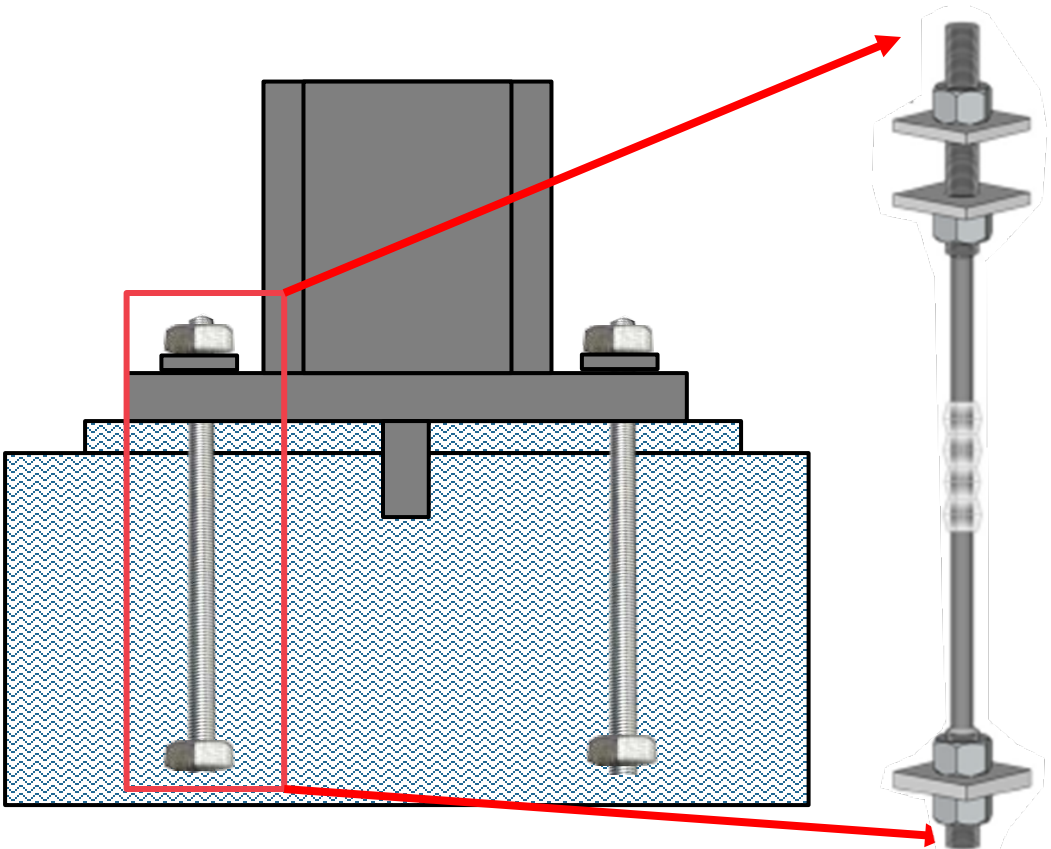


## A new “reliably ductile” detail – AISC/Pankow Project

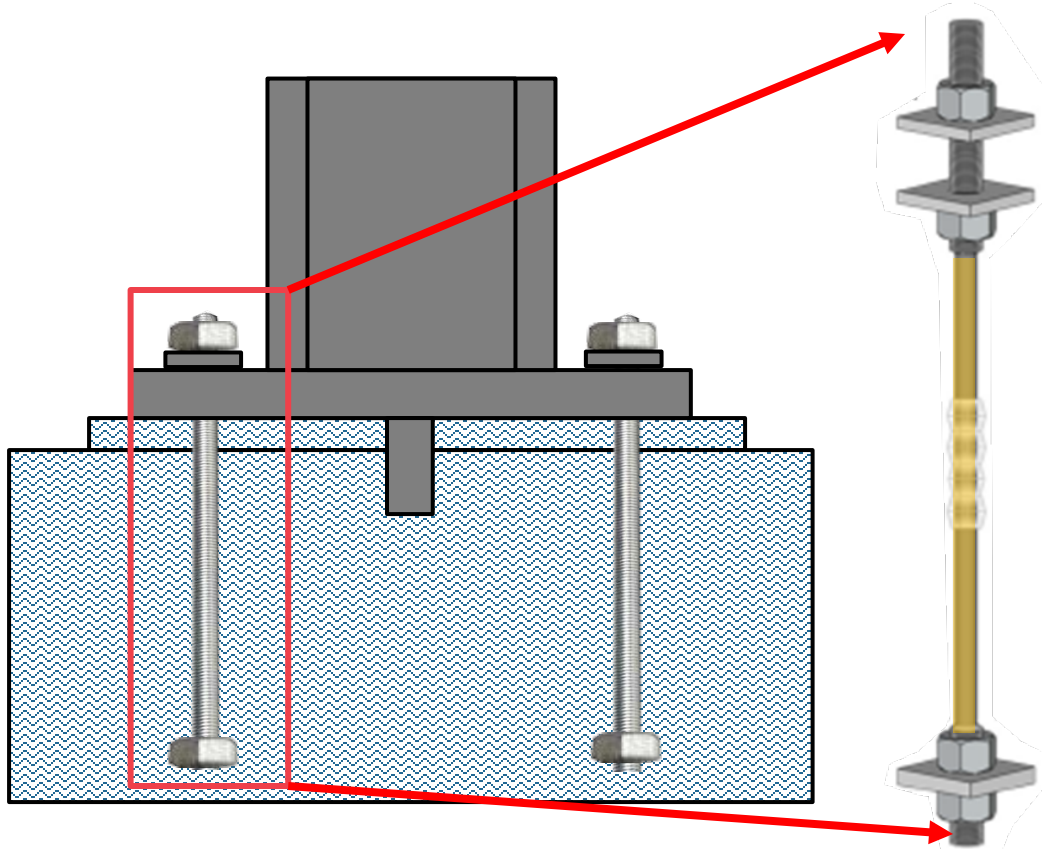


- Consultation with design engineers, fabricators
- Focus on convenience of fabrication
- Minimal changes to existing practice
- High confidence in ductile response

# The Upset Thread Detail



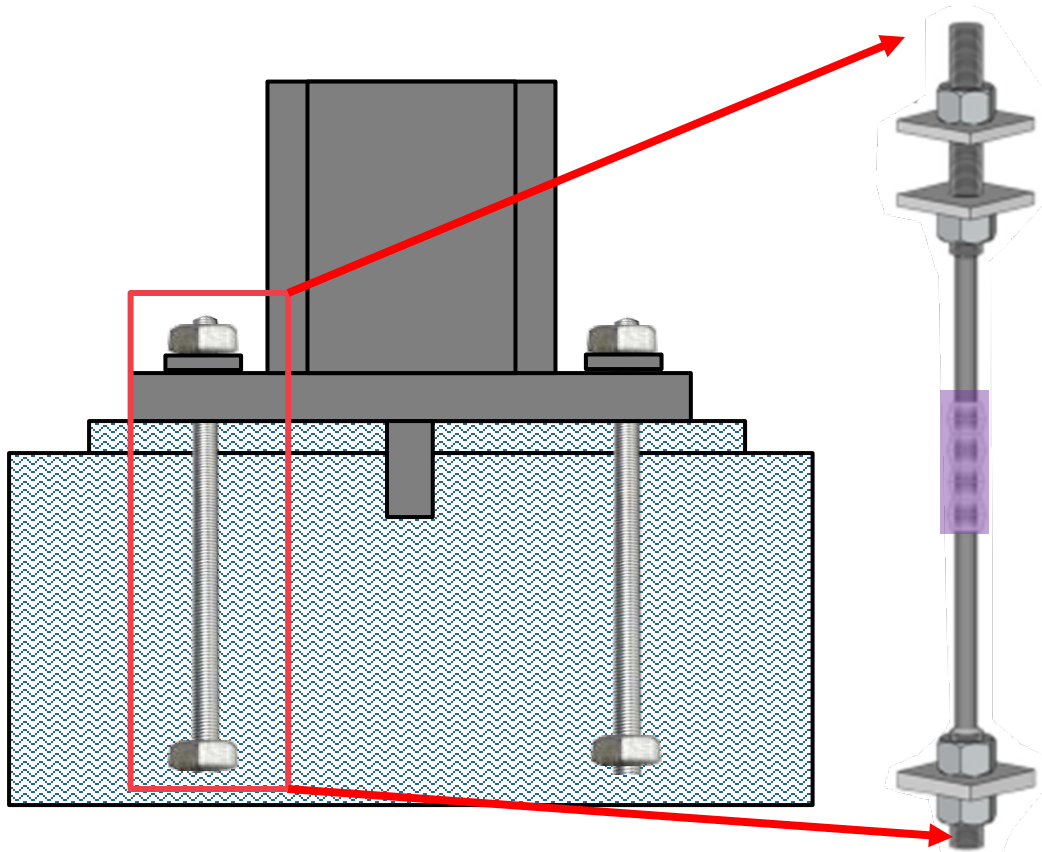
# The Upset Thread Detail



Milled down “upset” threads

- Enhance ductility
- Define yielding zone

# The Upset Thread Detail



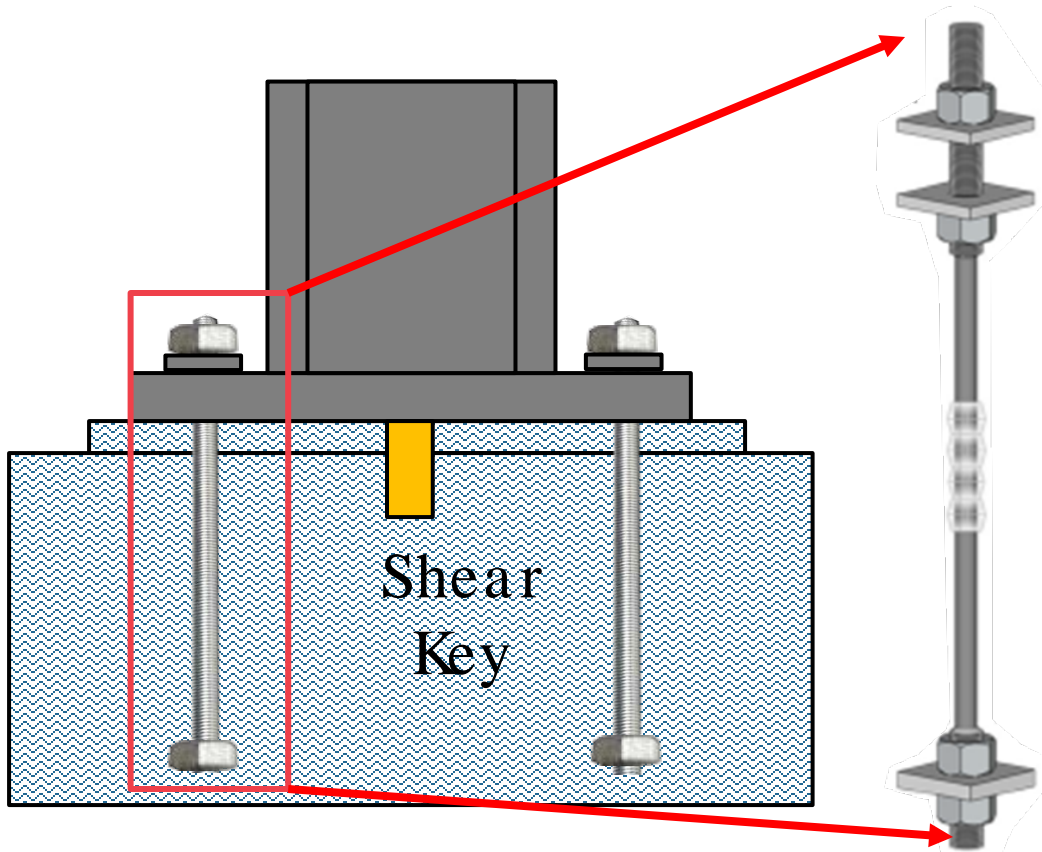
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Debonding tape

- Prevents rod catching
- Similar to BRB

# The Upset Thread Detail



Milled down “upset” threads

- Enhance ductility
- Define yielding zone

Debonding tape

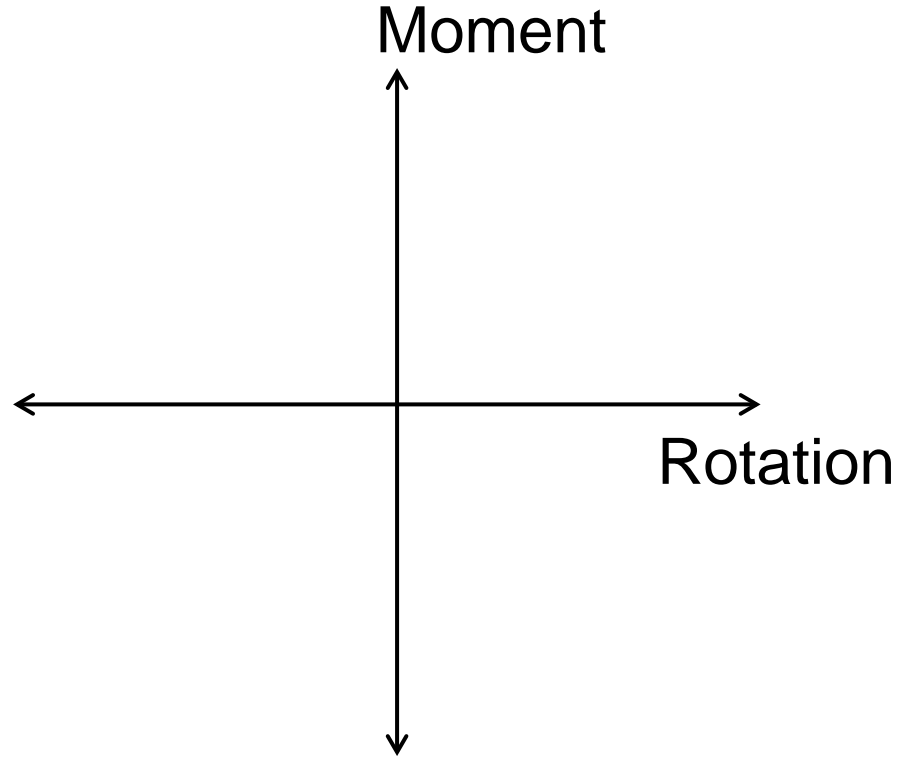
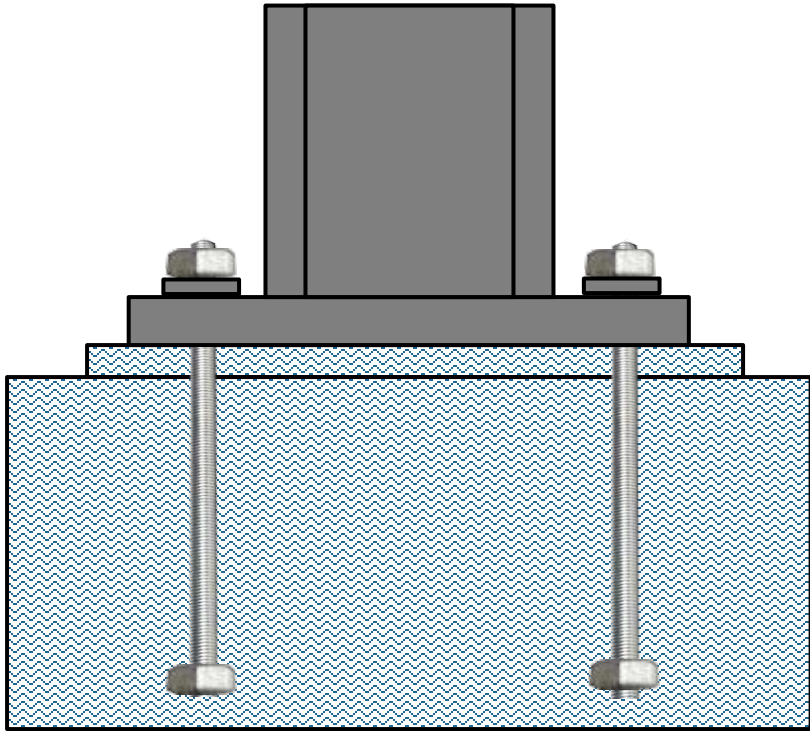
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Shear Key

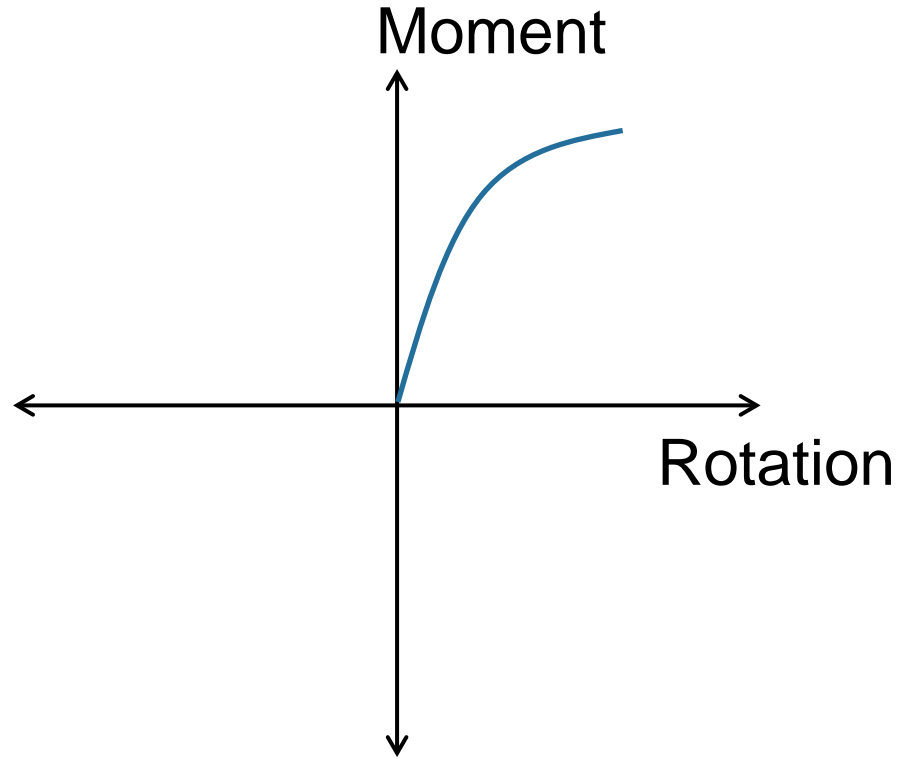
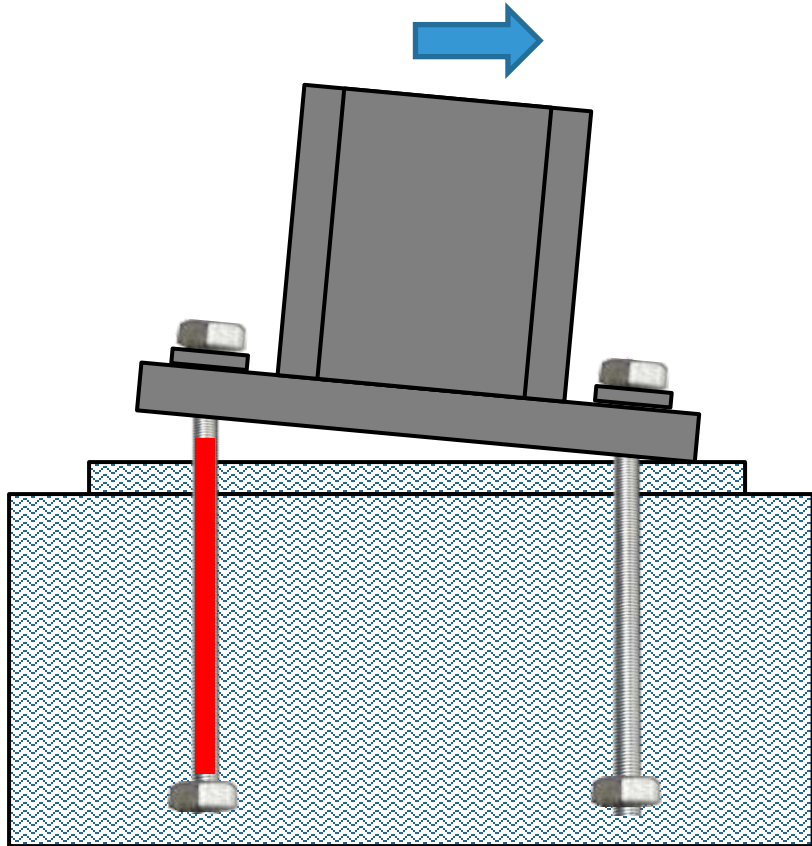
- Protects rods from shear



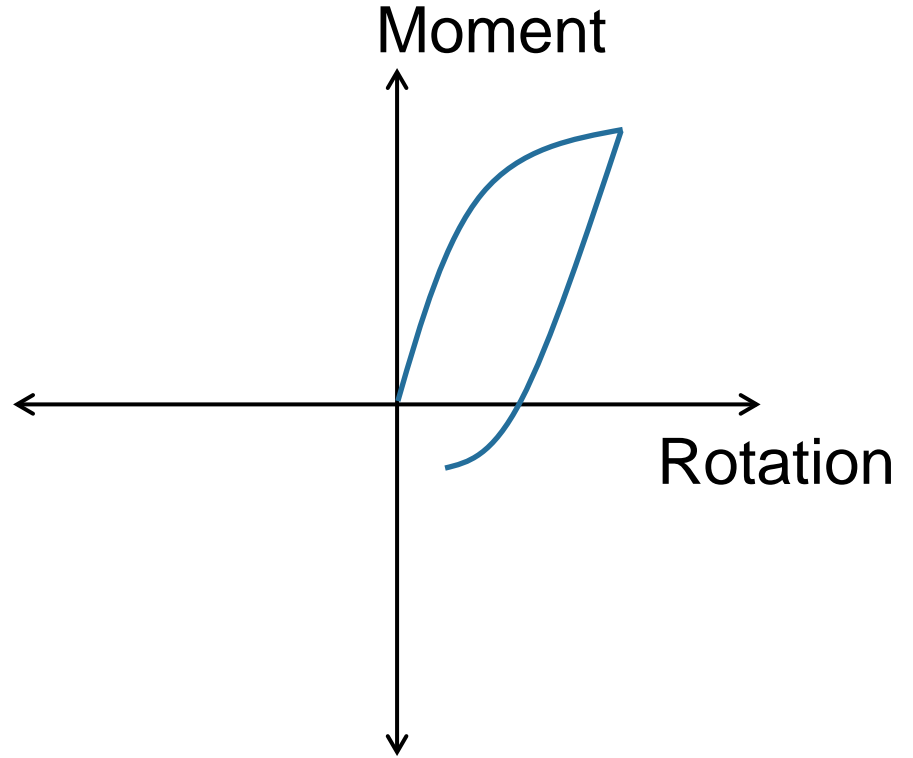
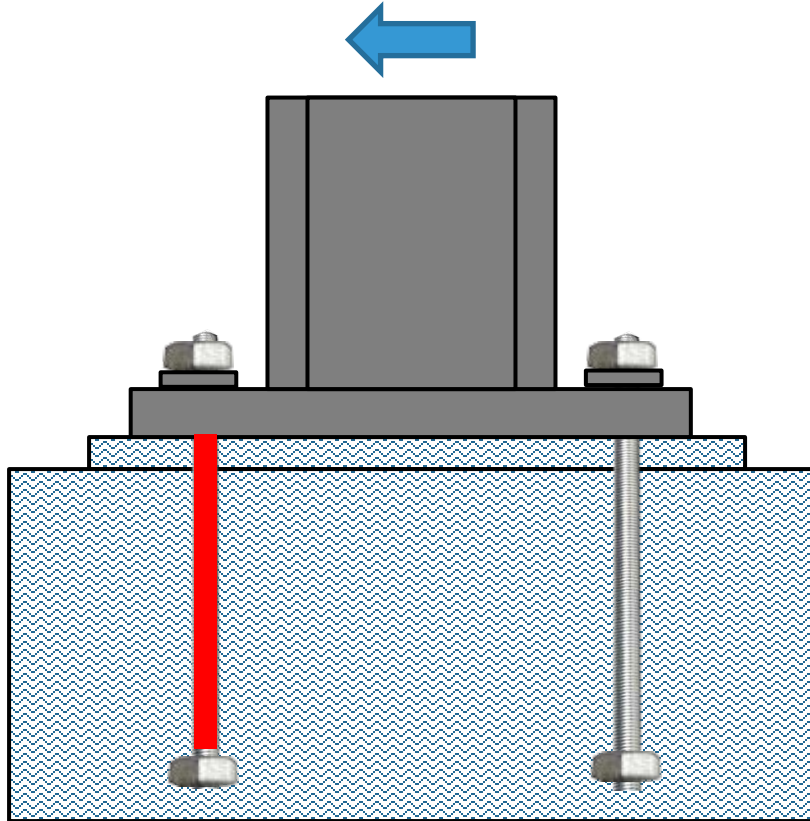
# Intended behavior



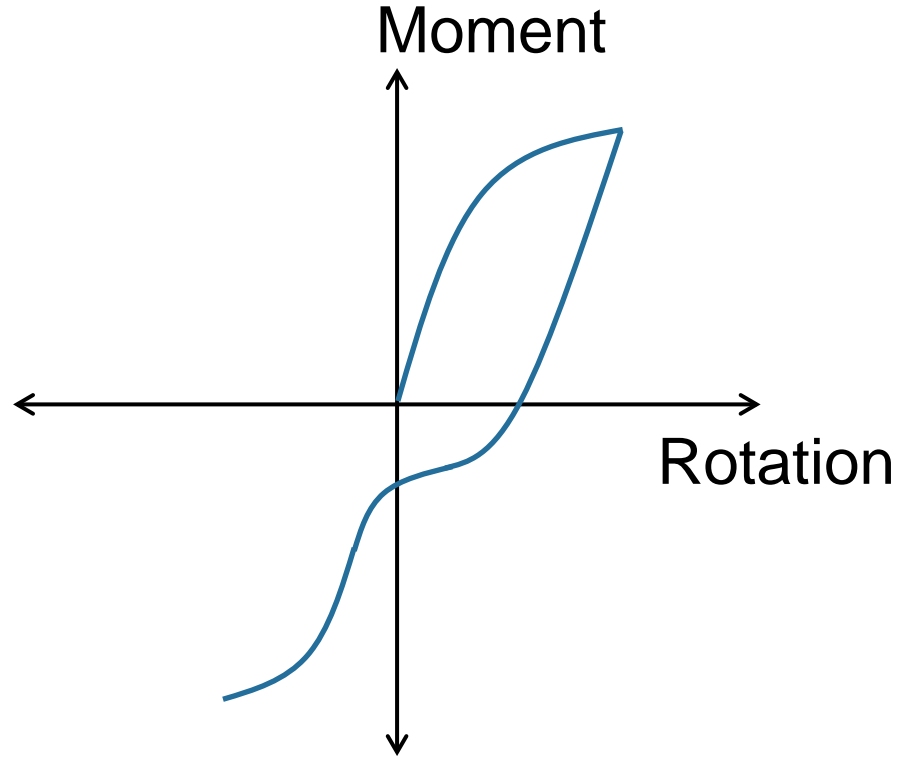
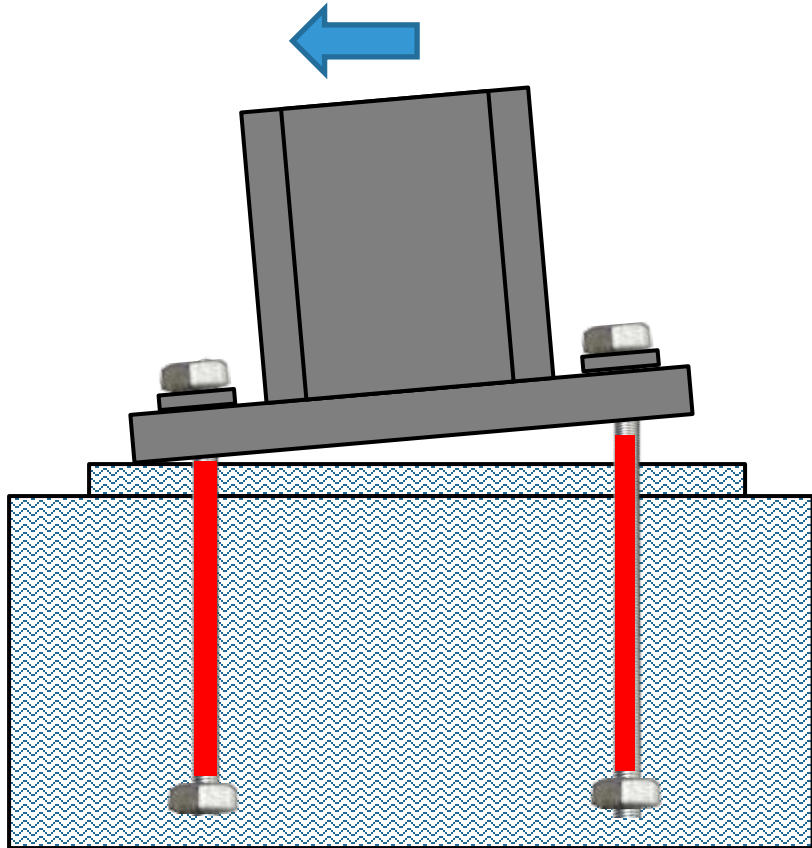
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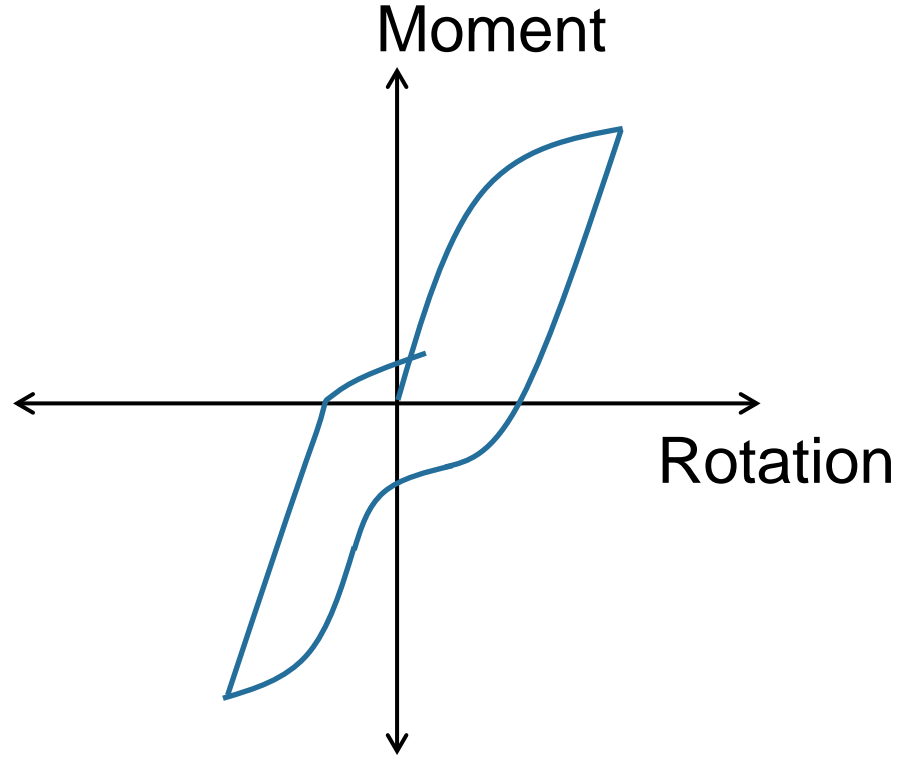
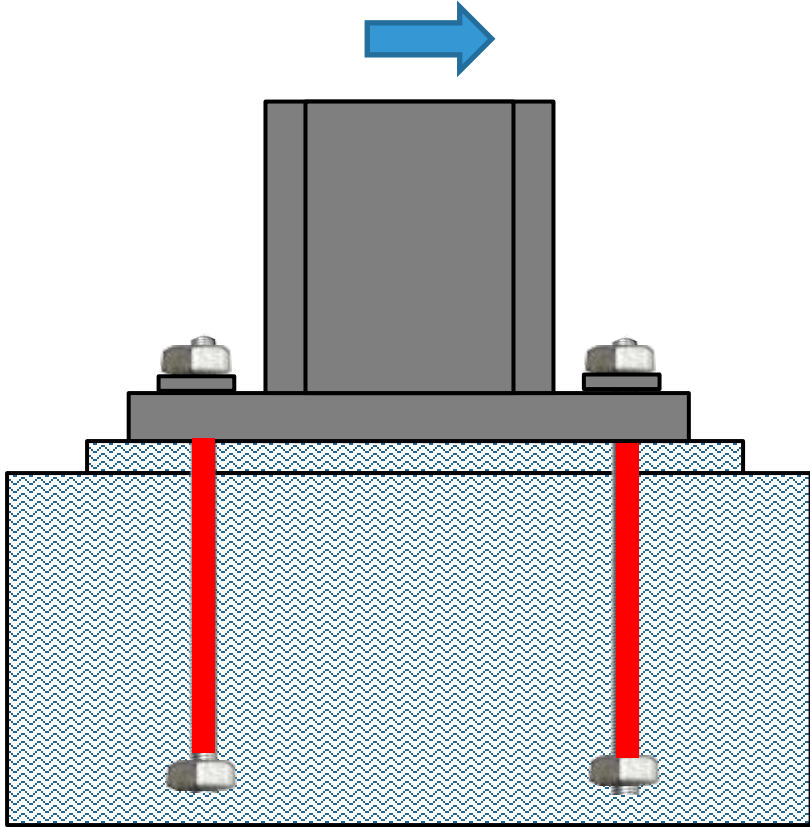
# Intended behavior



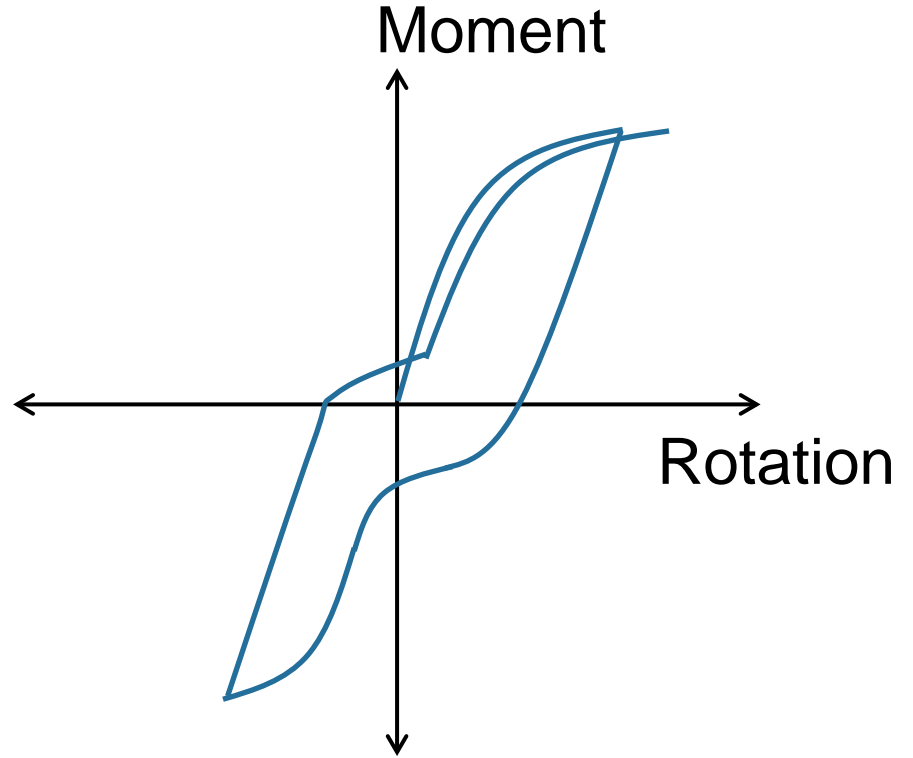
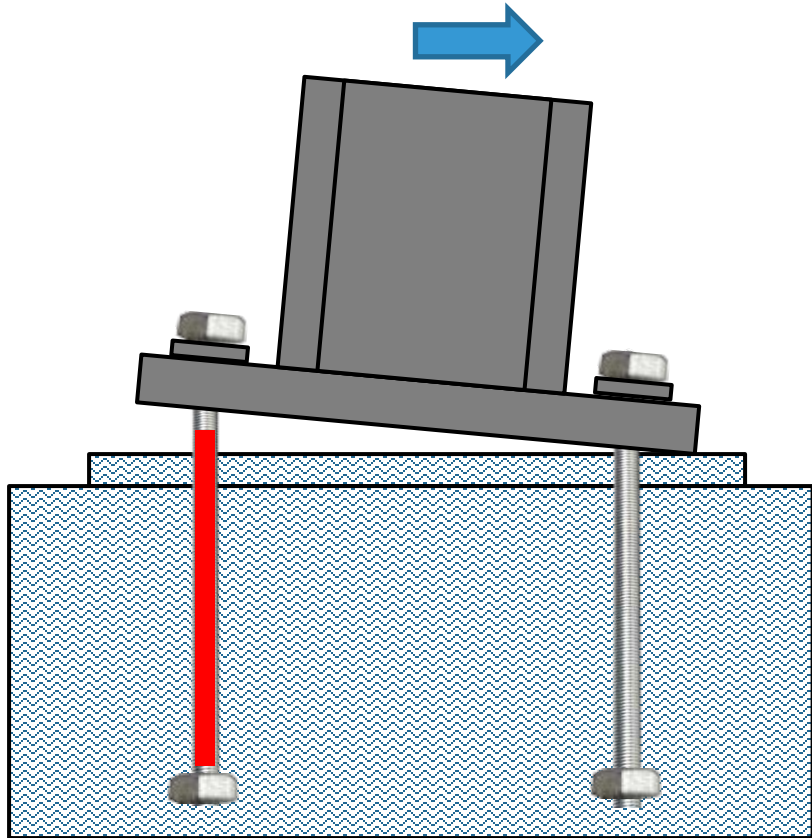
# Intended behavior



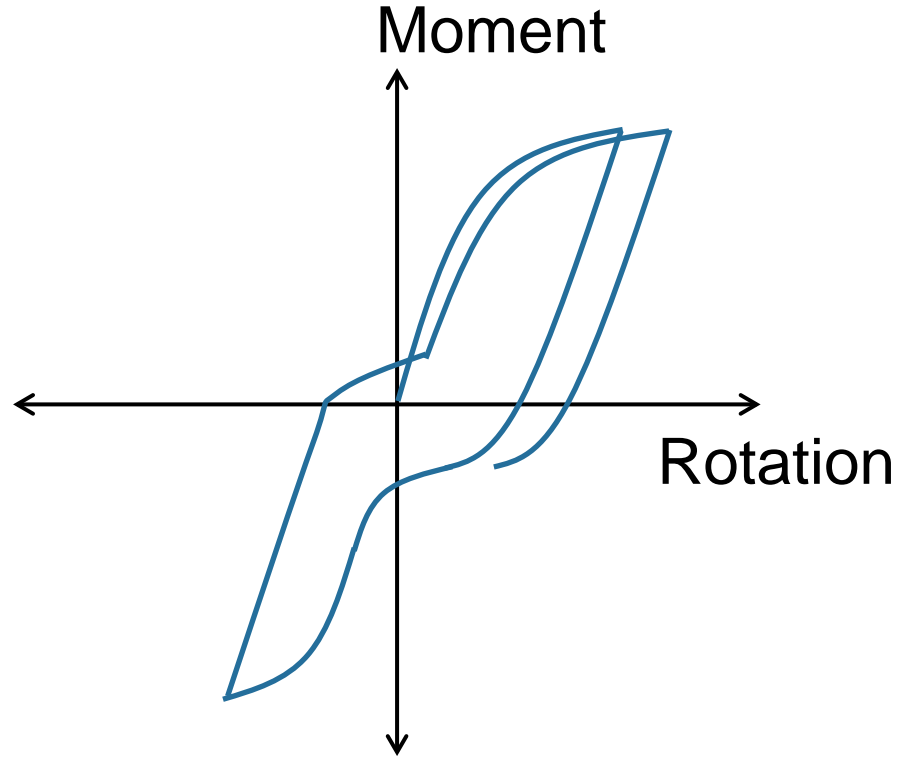
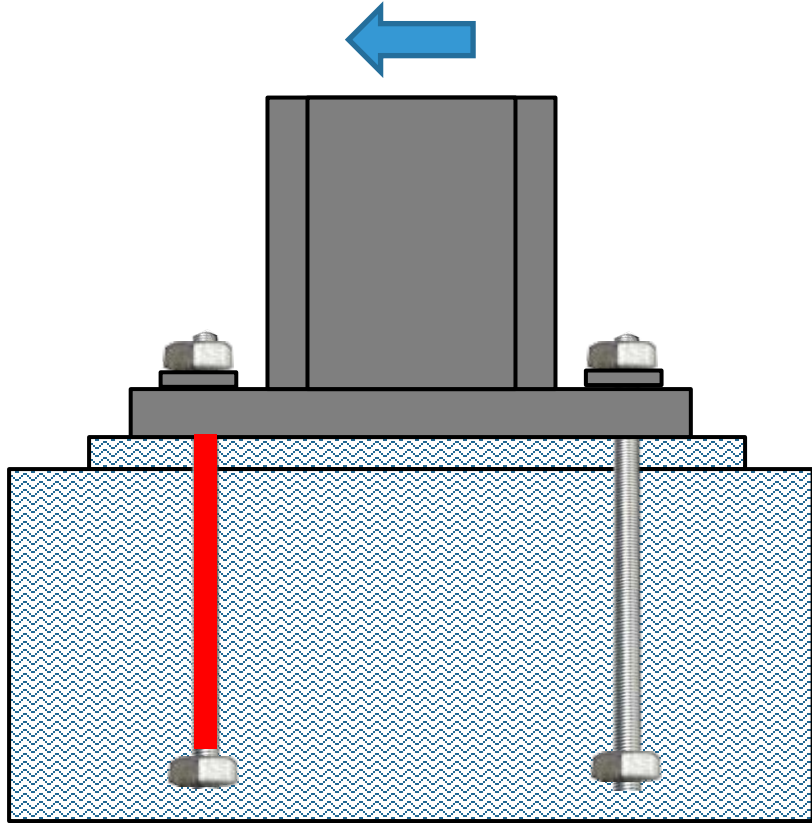
# Intended behavior



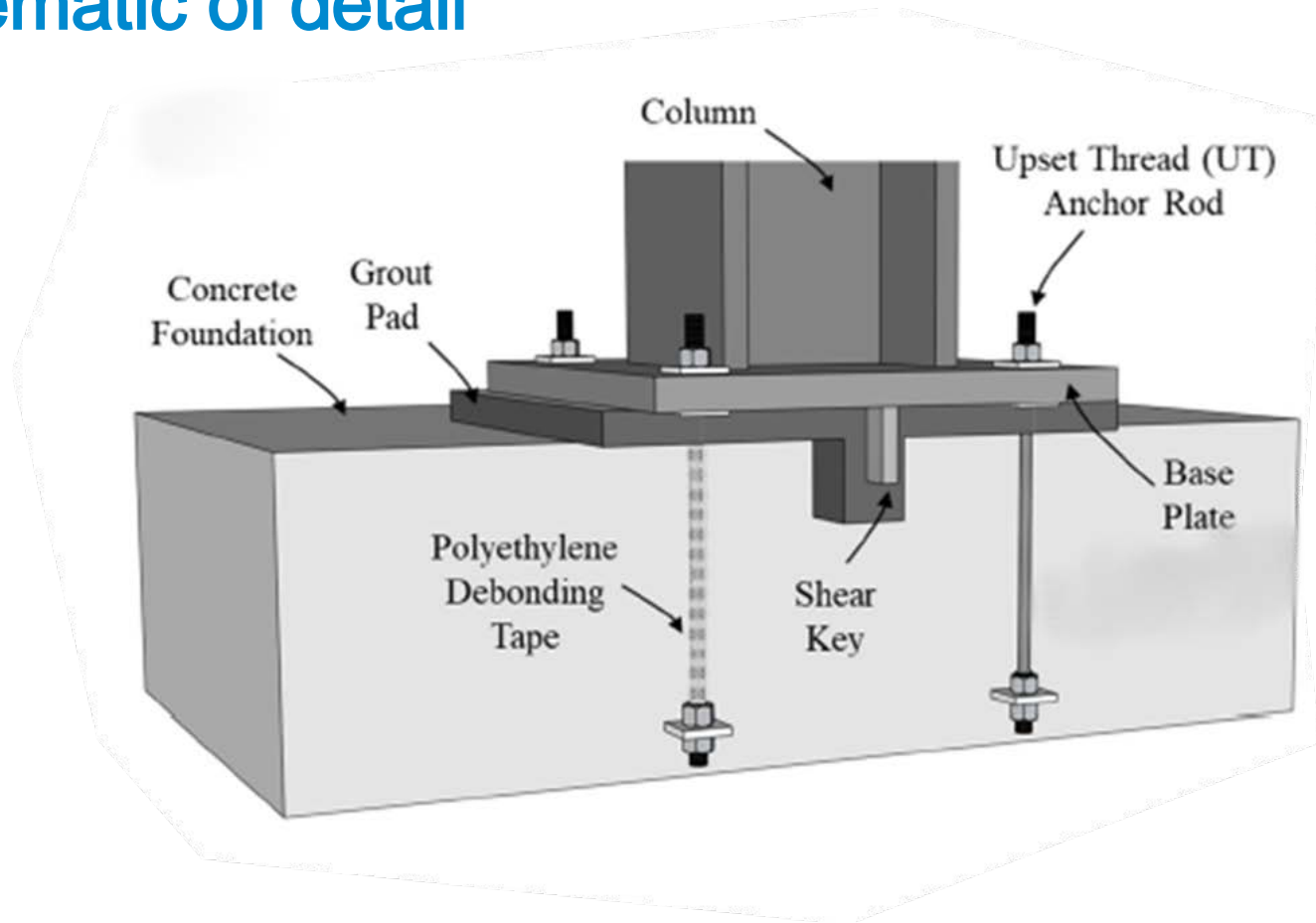
# Intended behavior



# Intended behavior



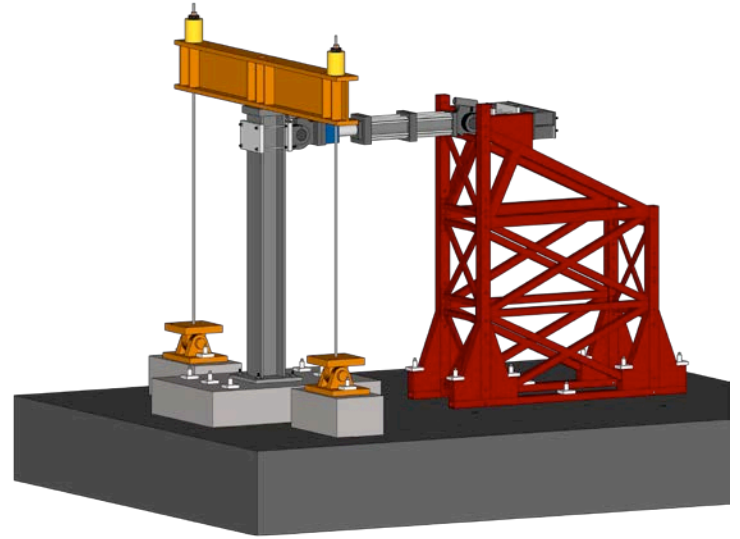
# Schematic of detail





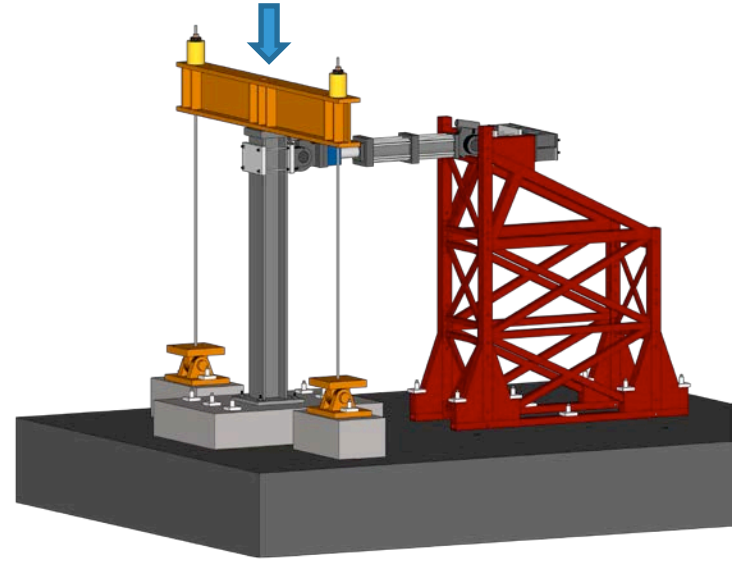
# Large scale tests and performance

Test #	Base Plate size [in]	Anchor Grade	Anchor Dia [in]	Axial Load [kip]
1	30 x 30 x 2	55	0.75	120 (C)
2			120 (C)	
3		105	1.00	120 (C)
4				0



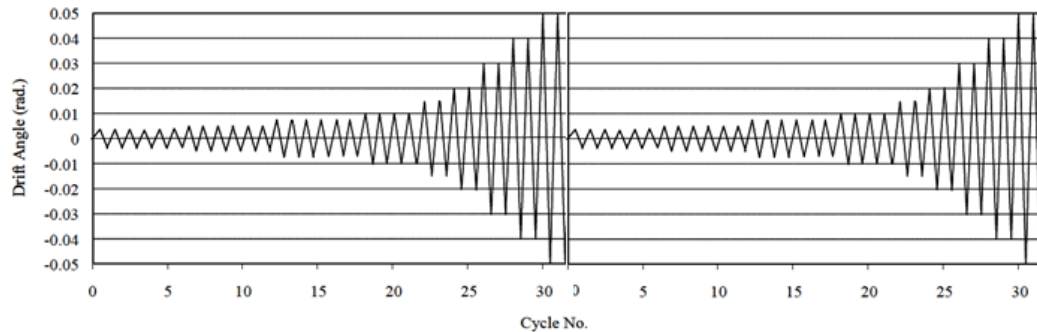
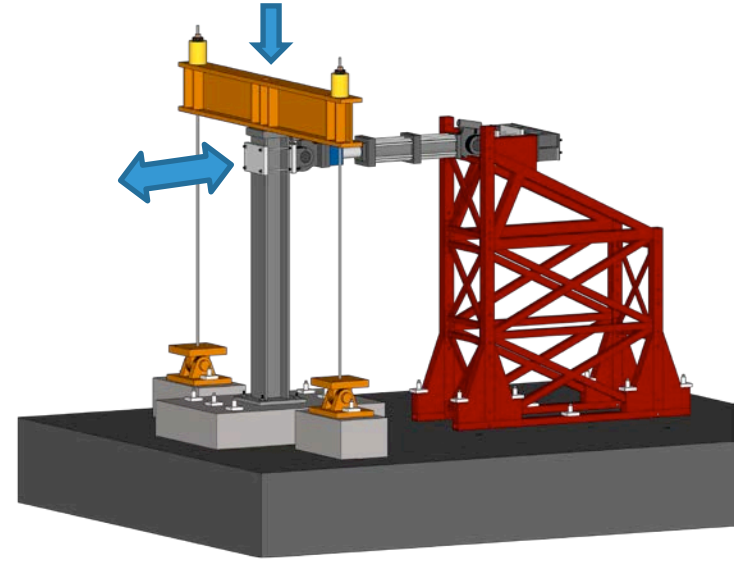
# Large scale tests and performance

Test #	Base Plate size [in]	Anchor Grade	Anchor Dia [in]	Axial Load [kip]
1	30 x 30 x 2	55	0.75	120 (C)
2			120 (C)	
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4				0



# Large scale tests and performance

Test #	Base Plate size [in]	Anchor Grade	Anchor Dia [in]	Axial Load [kip]
1	30 x 30 x 2	55	0.75	120 (C)
2			120 (C)	
3		105	1.00	120 (C)
4			0	



**ATGSAC Protocol  
applied twice  
followed by 6.5%  
cycles**

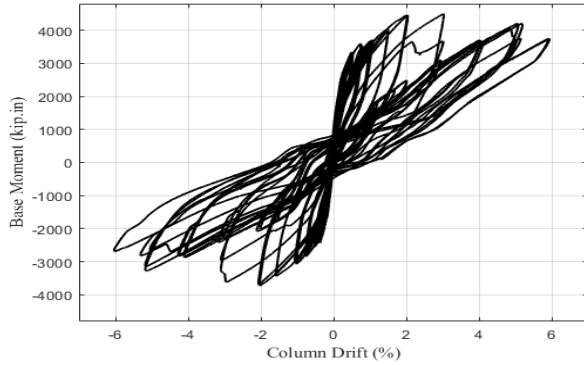
# Results



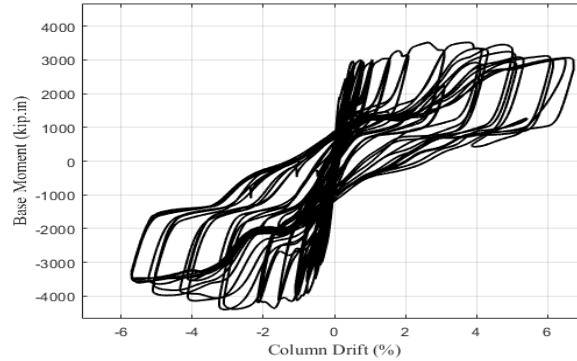
All specimens survived back to back applications of SAC protocol (to 5%) and additional cycles to 6.5% with no rod fracture

# Results

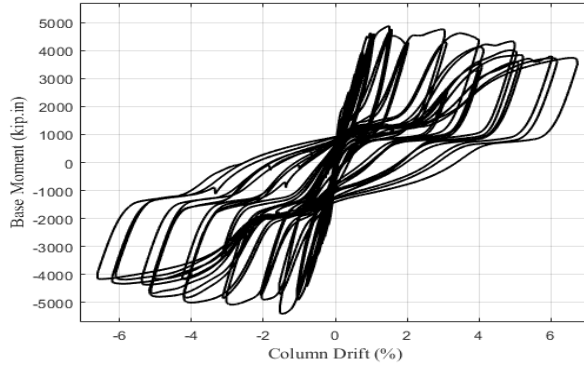
Test D1



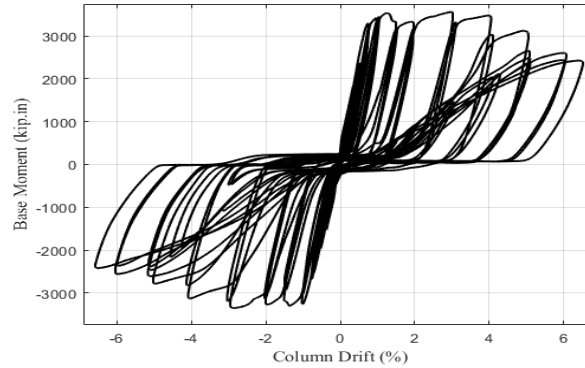
Test D2



Test D3



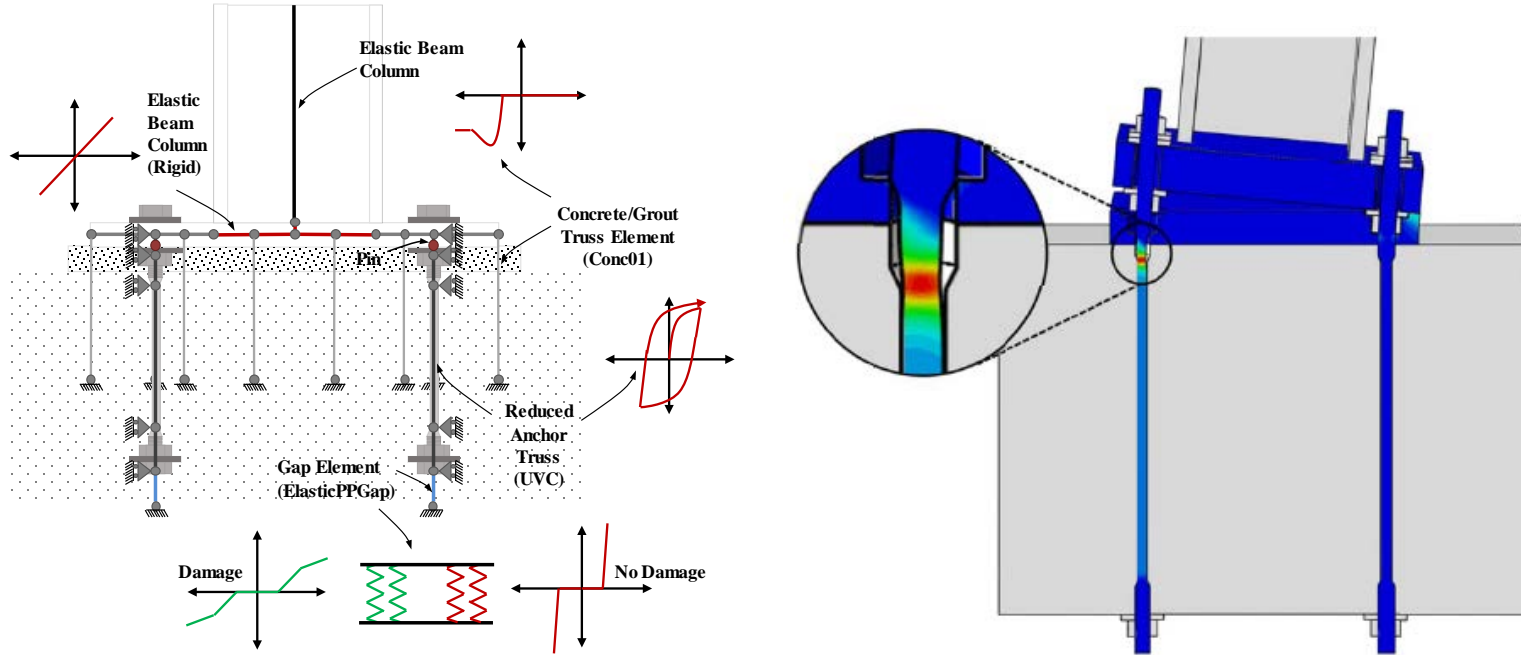
Test D4



Predominant damage – grout crushing

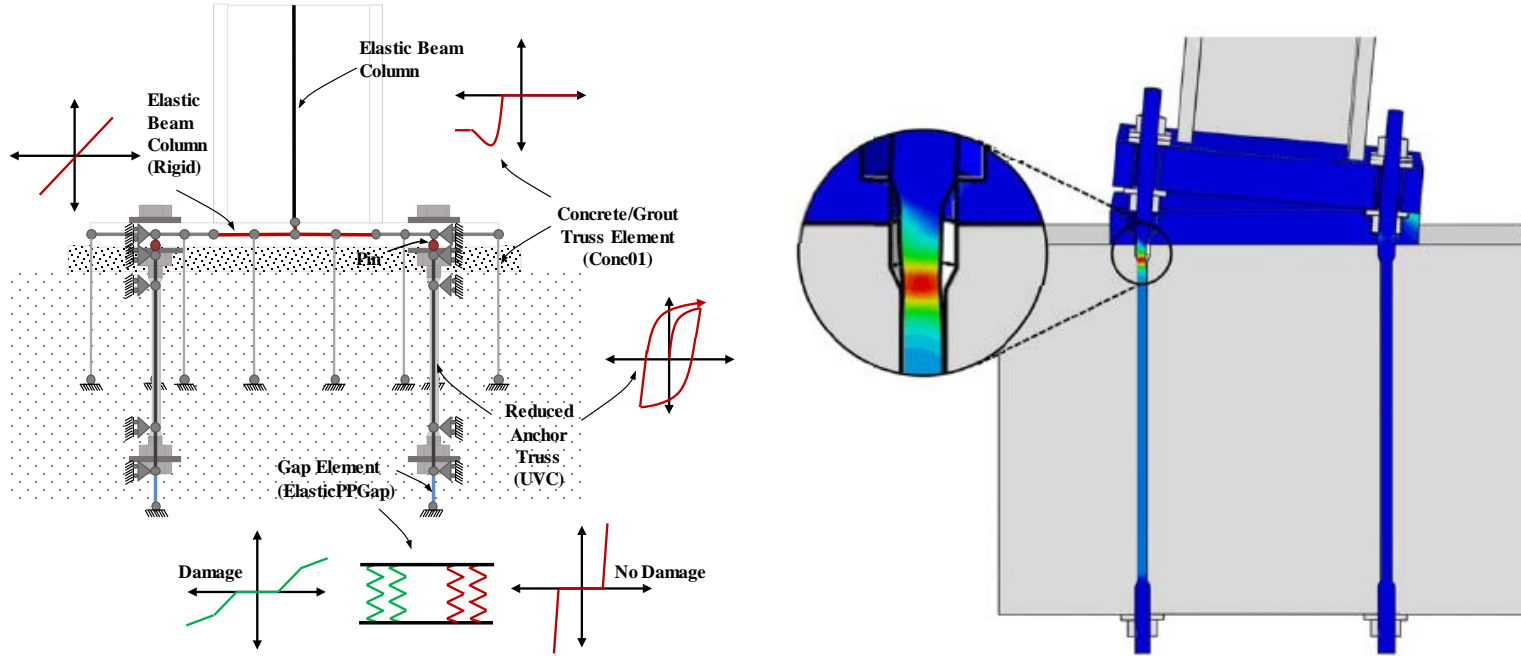


# Generalization using material testing, FEM, and line based simulations



Simulation of Necking, Ultra Low Cycle Fatigue, Bending

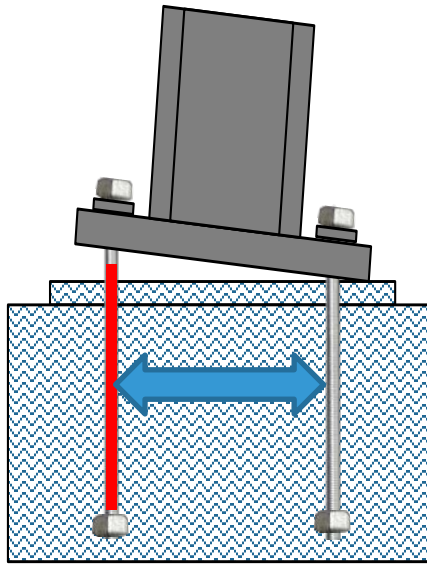
# Generalization using material testing, FEM, and line based simulations



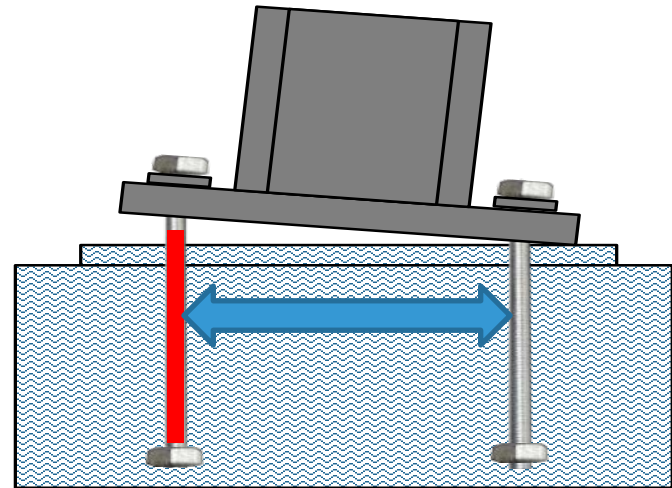
~60 parametric simulations with variations in plate and rod dimensions, rod materials, loading histories etc.

# Parametric Simulation findings

- Behavior appears to hold across a large number of configurations
- Ratio of stretch length to plate length is key



$$L_{\text{stretch}} > 0.5 \times L_{\text{plate}}$$

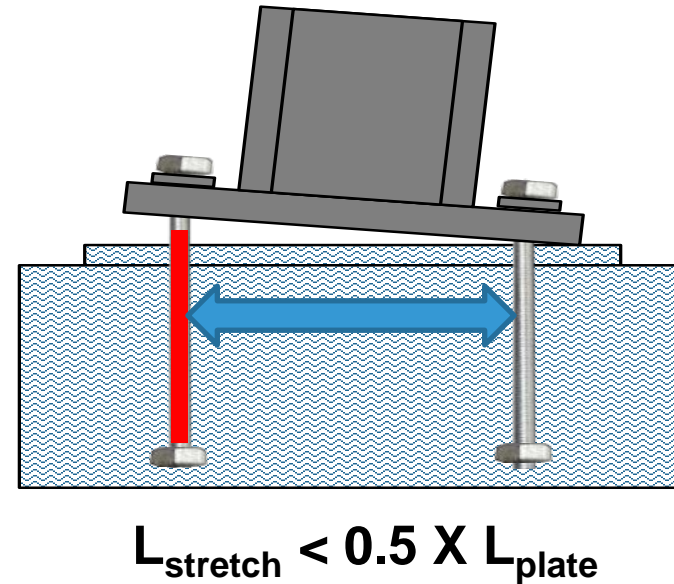
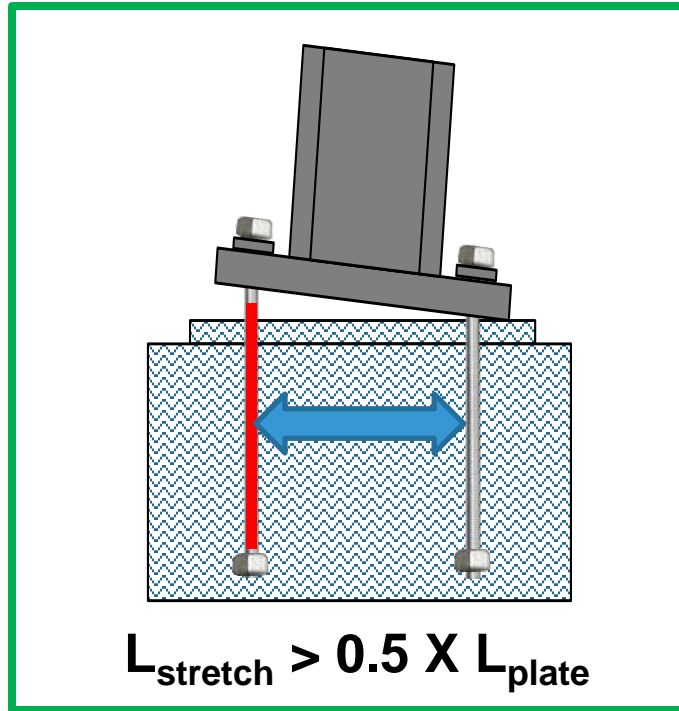


$$L_{\text{stretch}} < 0.5 \times L_{\text{plate}}$$

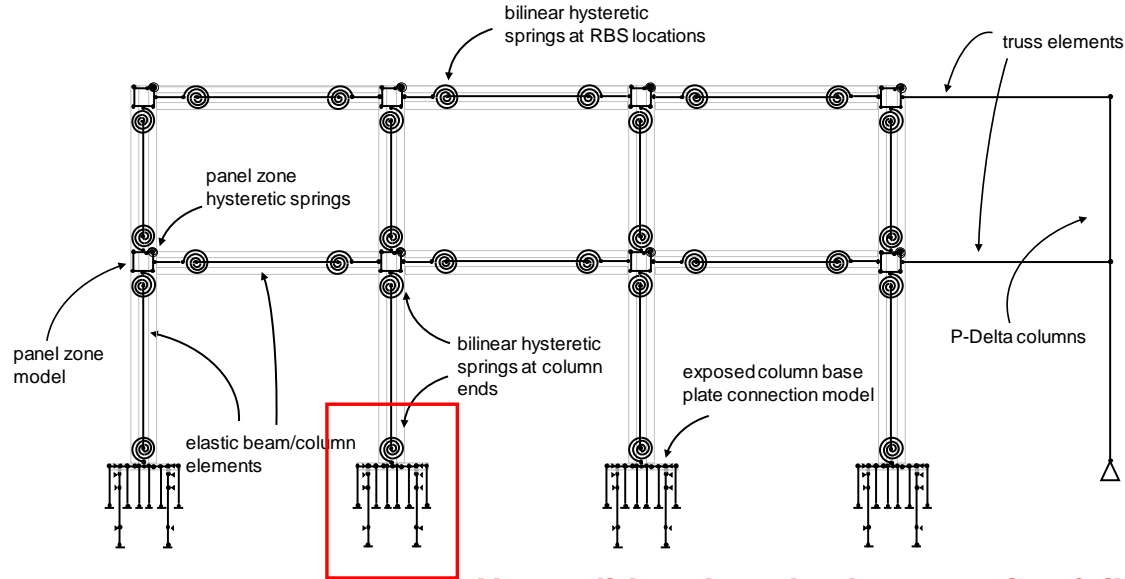


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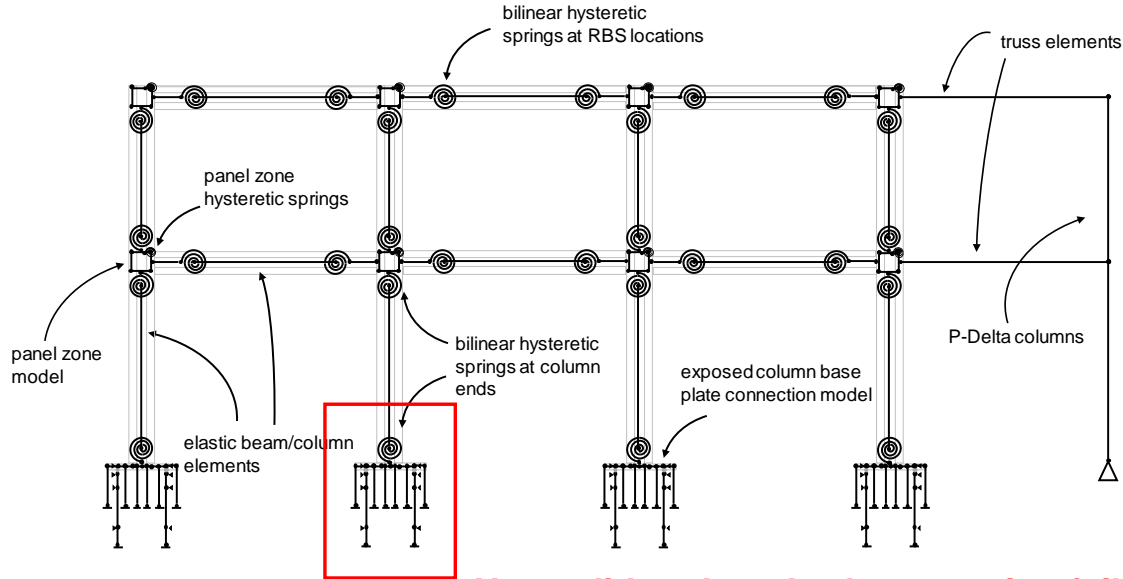


# NLTHA Results and summary



**Use validated method to examine failure**

# NLTHA Results and summary



**Use validated method to examine failure**

- Upset Thread detail with  $L_{\text{stretch}} > 0.5 \times L_{\text{plate}}$
- Design for  $\Omega_0$  or even lower forces



Excellent performance

# Organization

## Part 1

Exposed  
Base Plates

Prevailing  
understanding  
and design  
methods

New  
Developments

## Part 2

Embedded  
Bases

Prevailing  
understanding  
and design  
methods

New  
Developments

## Part 3

A look to the  
future

“Resolved”  
issues

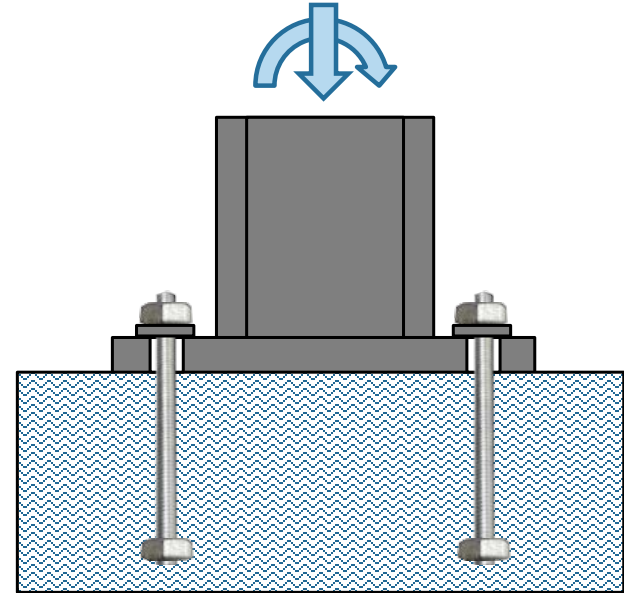
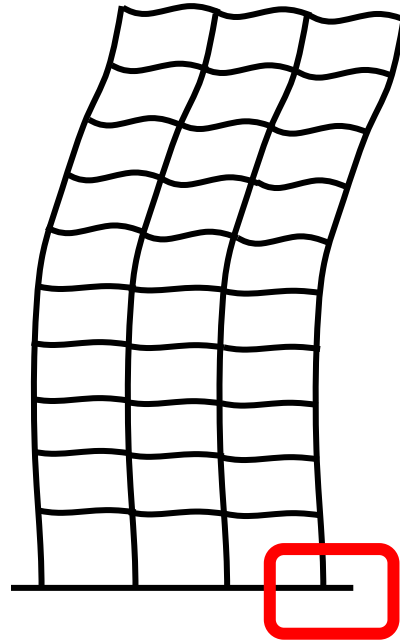
Ongoing work  
Unresolved  
issues

# Part 2 – Embedded Base Connections

## Embedded Bases

Prevailing understanding and design methods

New Developments



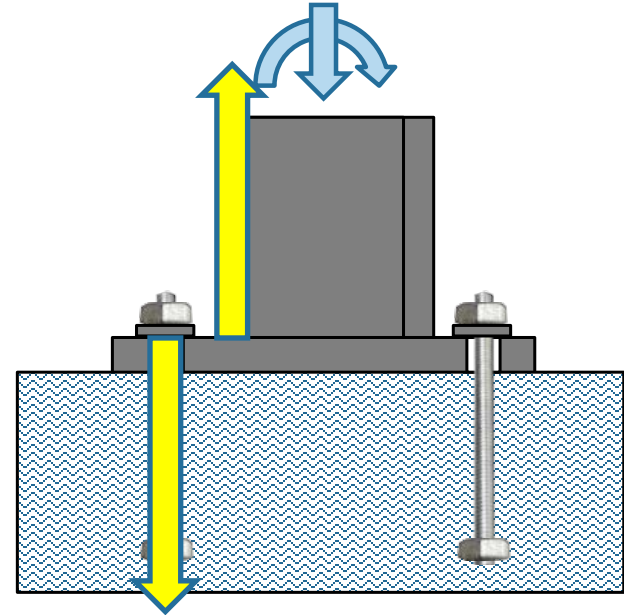
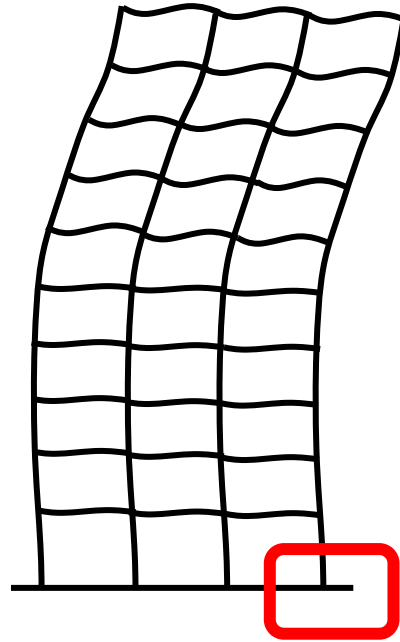
High rise buildings  
Large column moments

# Part 2 – Embedded Base Connections

## Embedded Bases

Prevailing understanding and design methods

New Developments



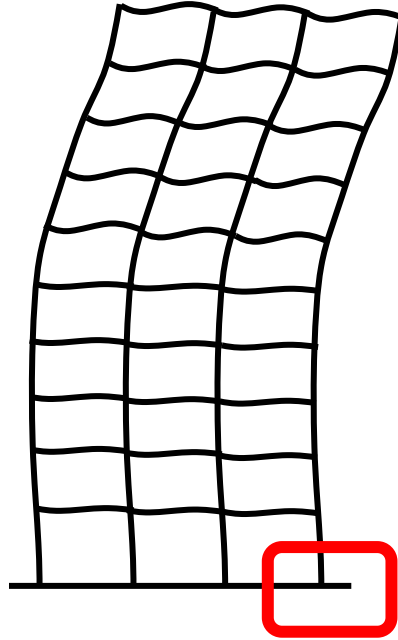
Developing column capacity is challenging

# Part 2 – Embedded Base Connections

## Embedded Bases

Prevailing understanding and design methods

New Developments



Developing column capacity is challenging

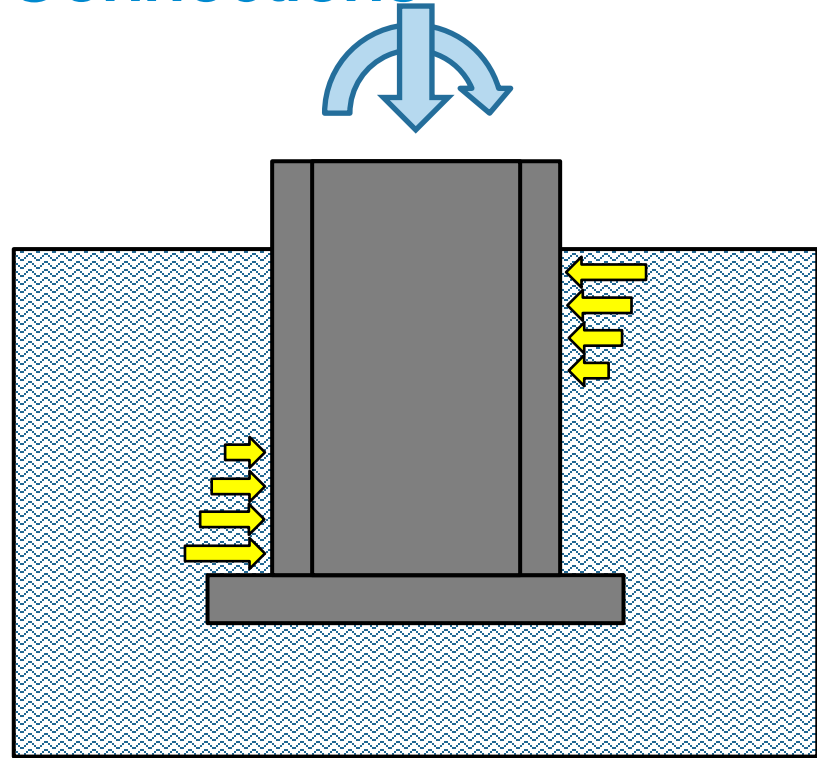
Photo credit: Josh Buckholt and Mahmoud Maamouri, CSD Engineers

# Part 2 – Embedded Base Connections

## Embedded Bases

Prevailing understanding and design methods

New Developments



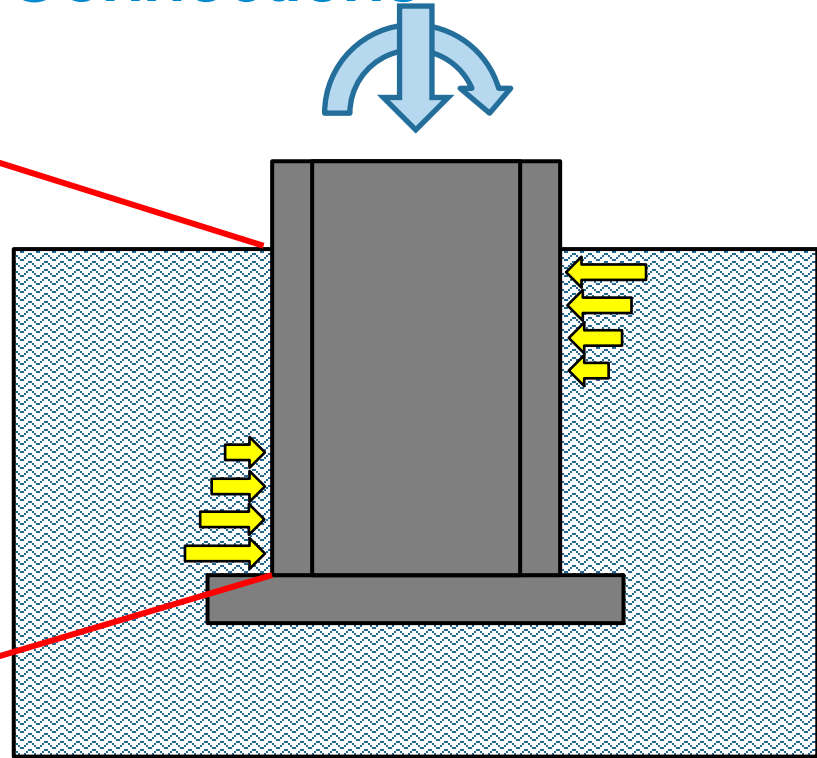
Resistance through  
concrete bearing



# Part 2 – Embedded Base Connections



Photo credit: Nabih Youssef,  
SimpsonGumpertz and Heger



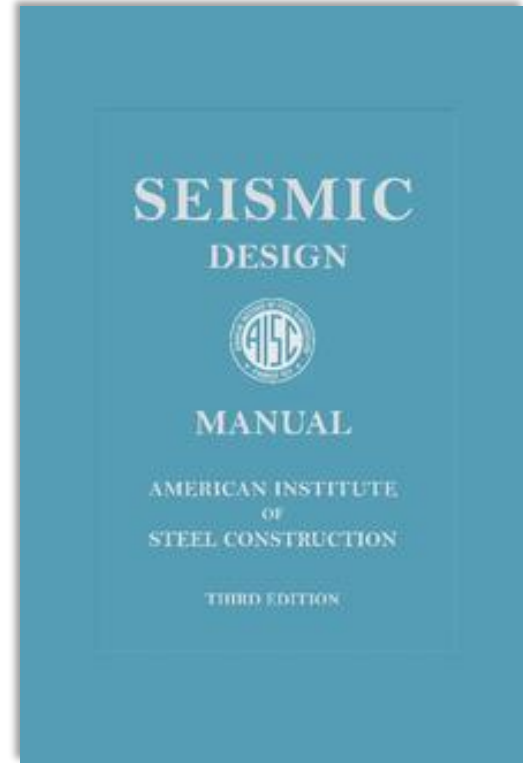
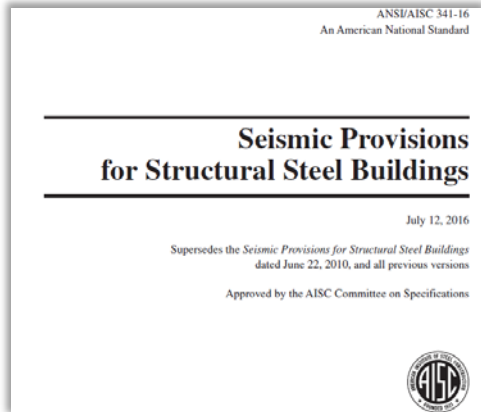
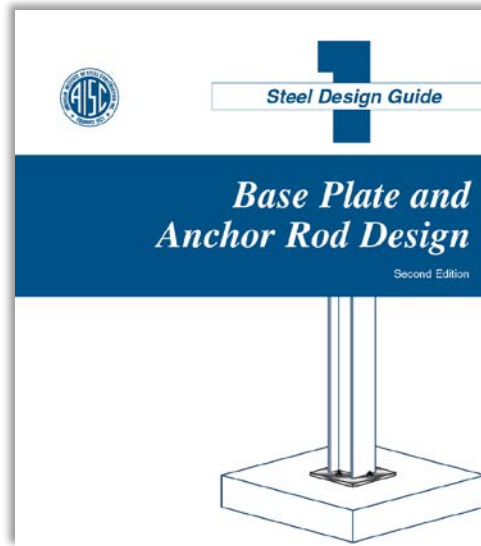
Resistance through  
concrete bearing

# Overview

## Embedded Bases

Prevailing understanding and design methods

New Developments



# Takeaways from Design Documents

- AISC 341 and Design Guide One identify embedded details
- AISC 341 – Commentary points to similar details
- SSDM uses coupling beam analogy

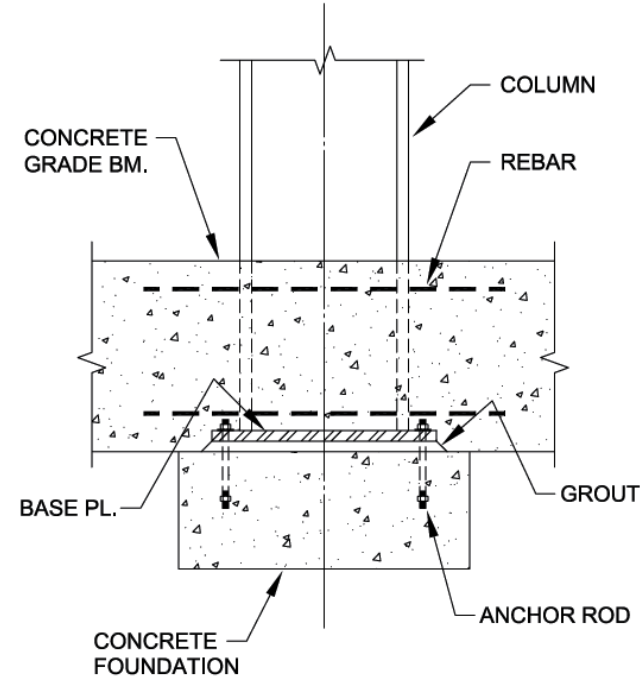
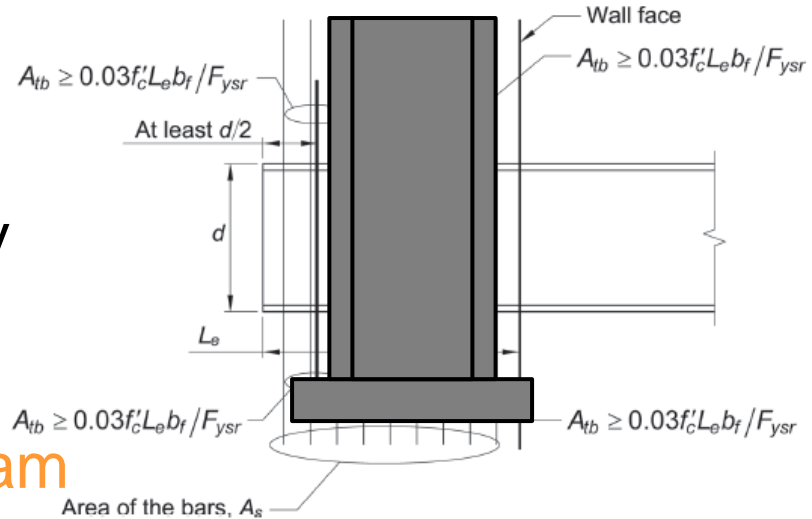


Figure 2.7. Embedded moment base detail.

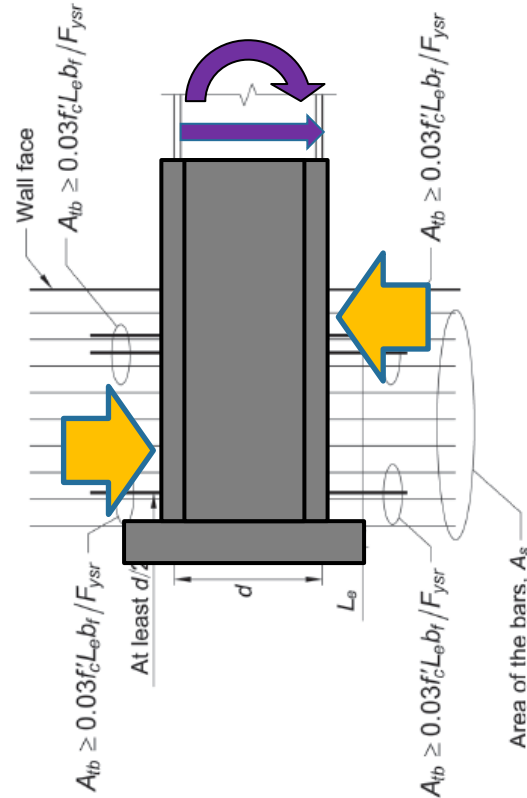
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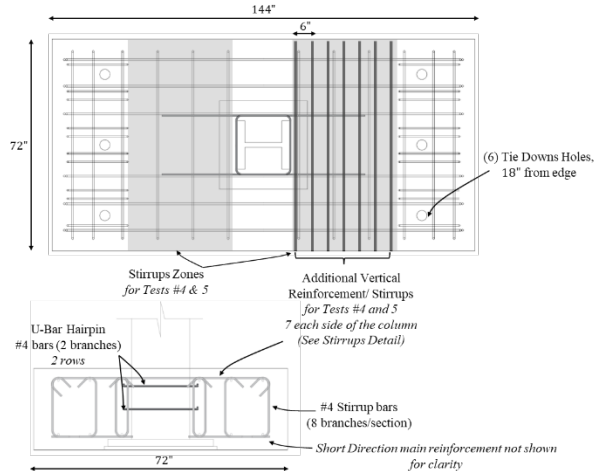
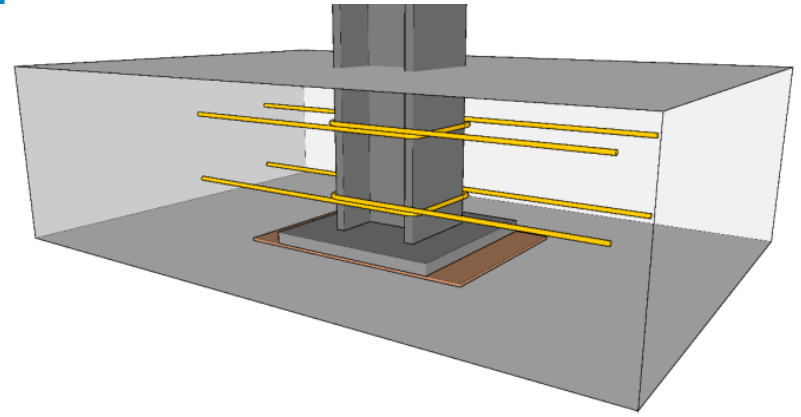
# Research in the last 15 years

- 10 Experiments
- Finite element simulations
- Strength and stiffness models

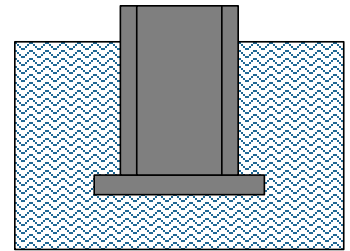
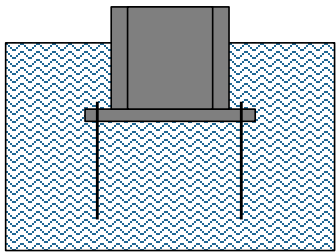
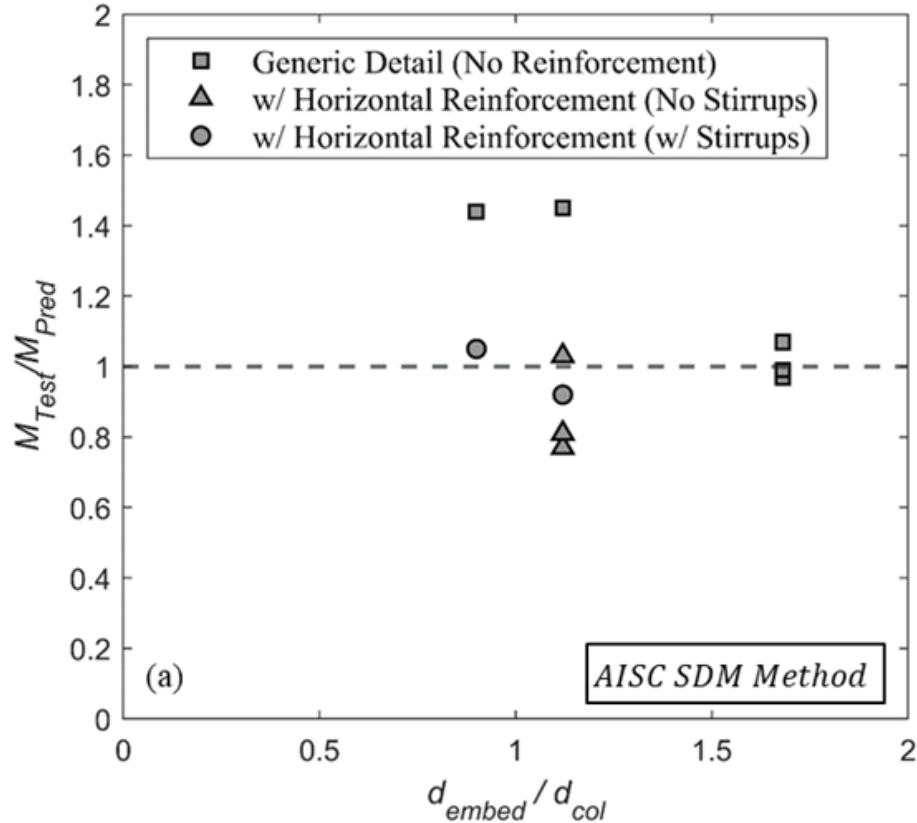


# Various variables investigated

- Embedment depth
- Axial compression
- Column size
- Reinforcement (horizontal and vertical)

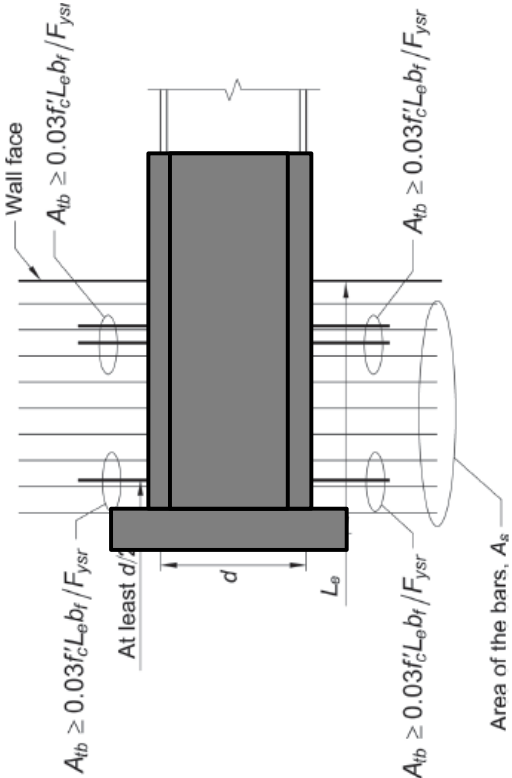
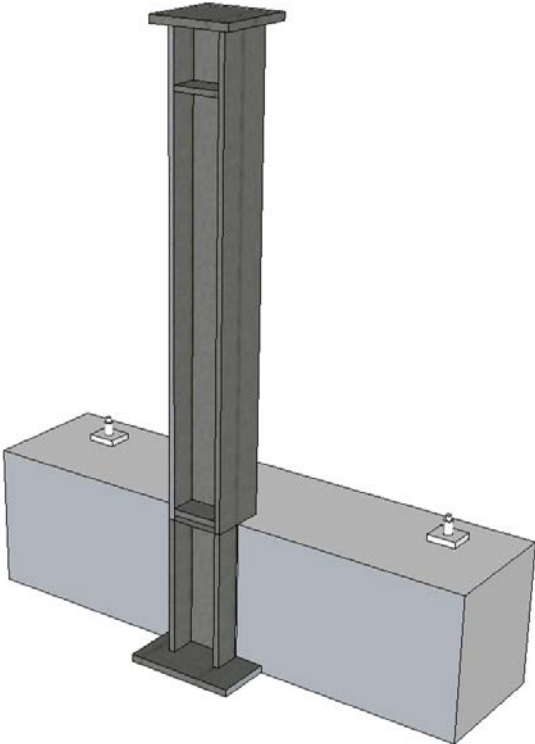


# Coupling beam approach applied to test data

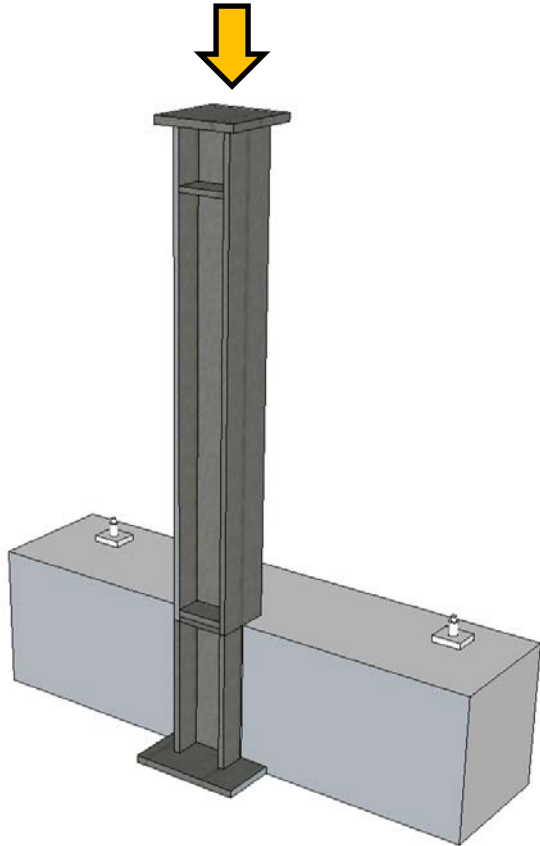




# Embedded base connections are NOT coupling beams

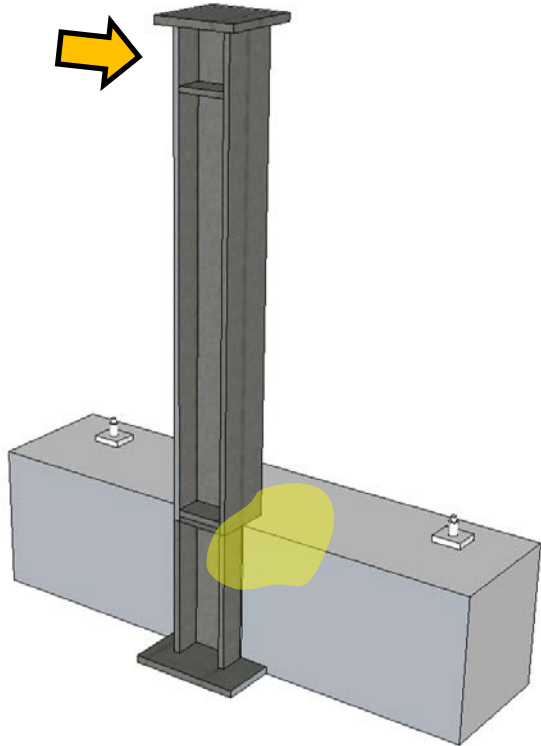


## Embedded base connections are NOT coupling beams



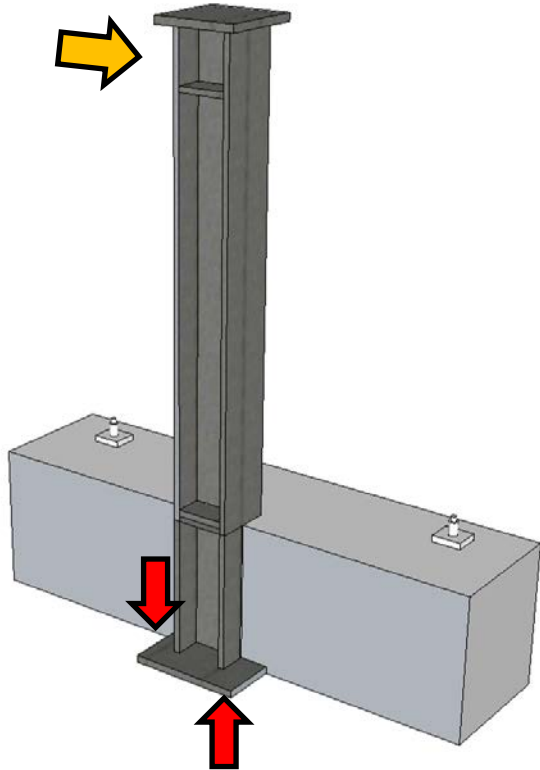
- Effect of axial force
- Additional confinement around column flanges
- Fixity and strength due to vertical bearing

## Embedded base connections are NOT coupling beams



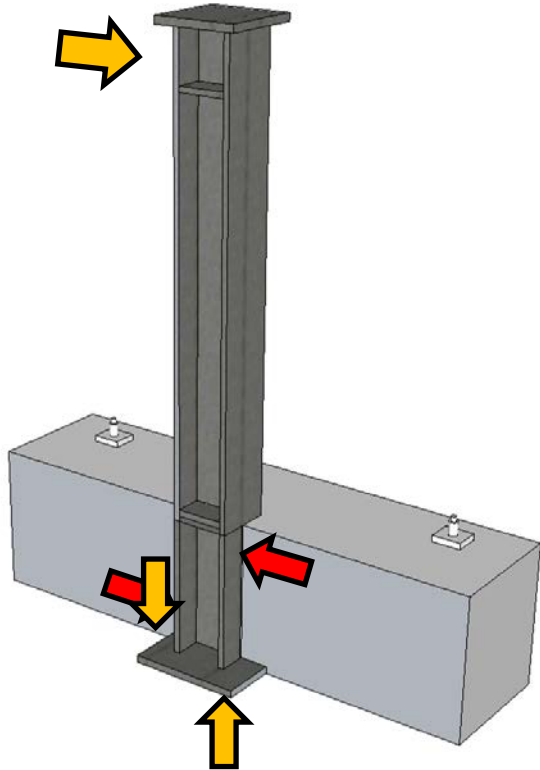
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- Effect of axial force
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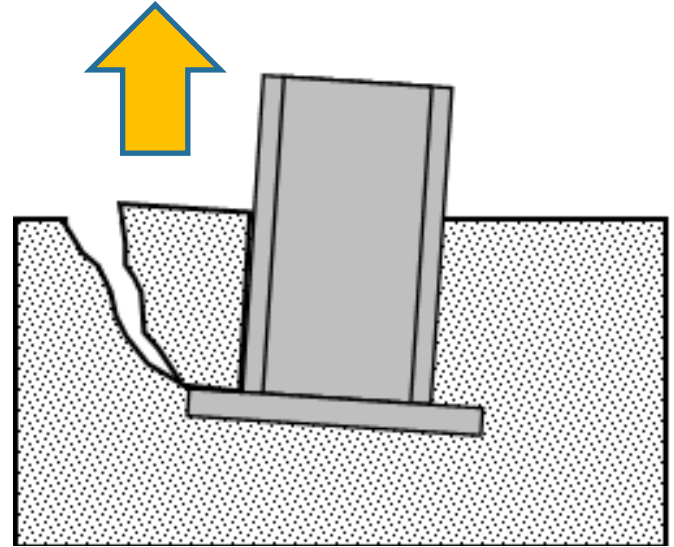
# New model for embedded base connections



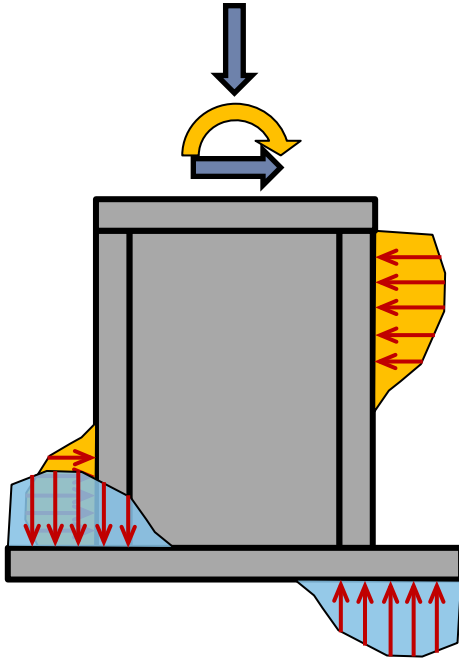
- Horizontal bearing against column flanges
- Vertical bearing against embedded plate
- Consideration of interactions and failure modes



# Vertical bearing



# Strength Model— considering both mechanisms

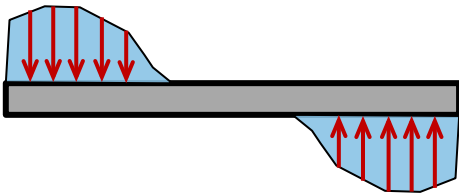
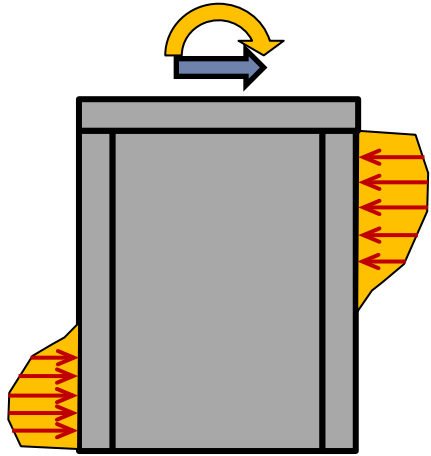


- Idealization of stress blocks
- Consideration of failure modes in each direction
- Consideration of reinforcement patterns

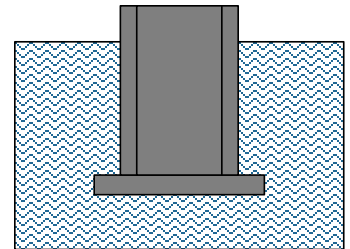
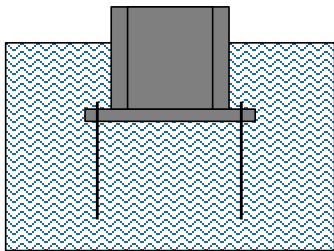
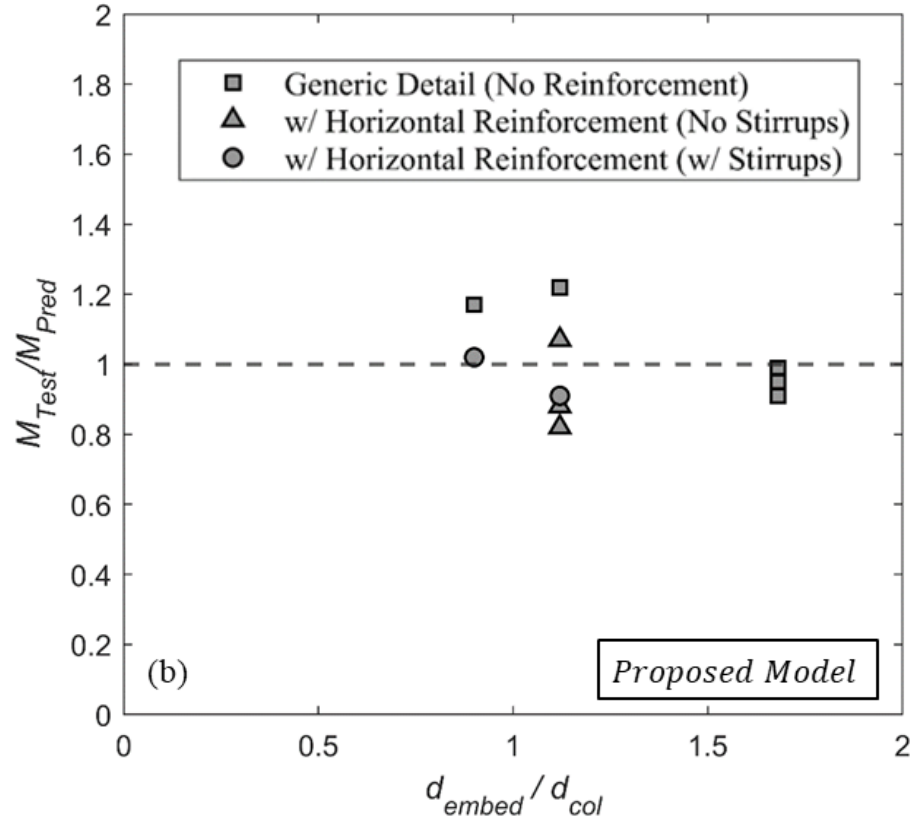


# Strength Model

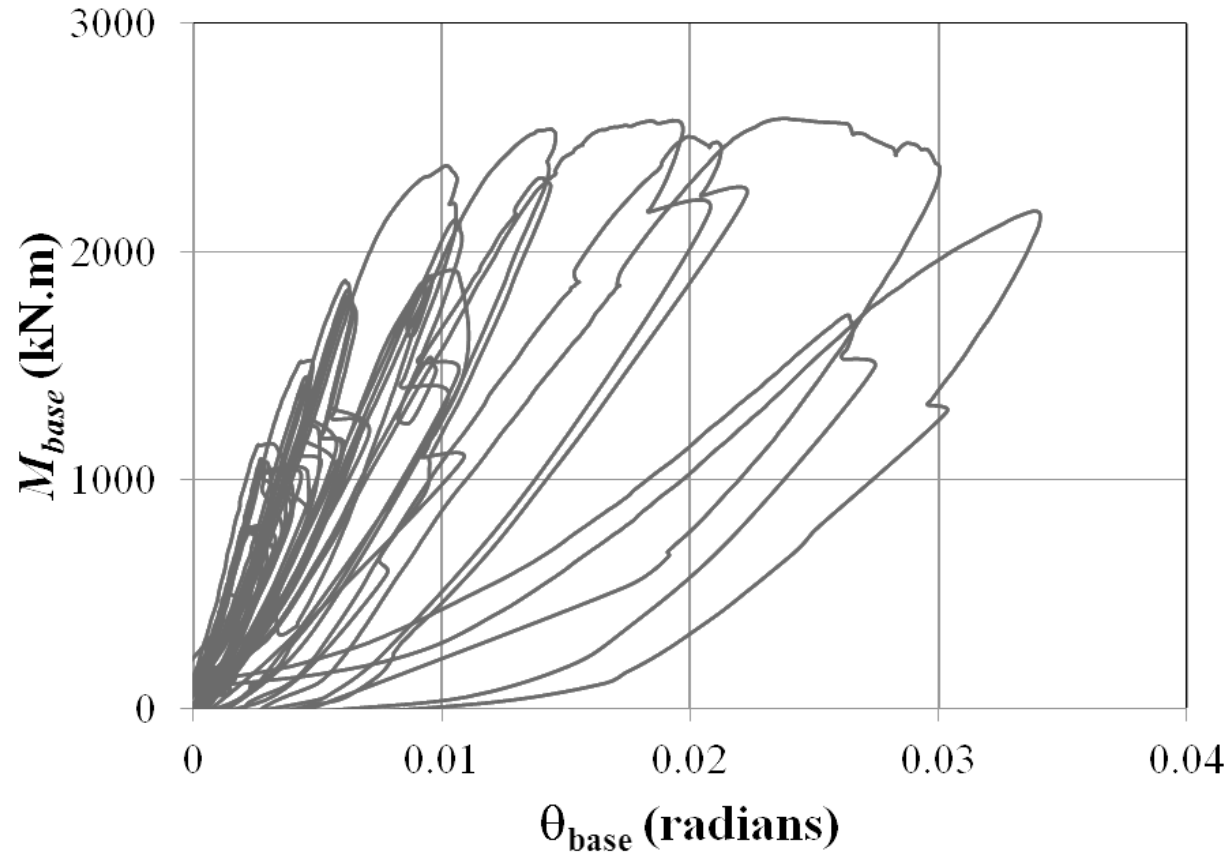
Consideration of failure modes in each direction



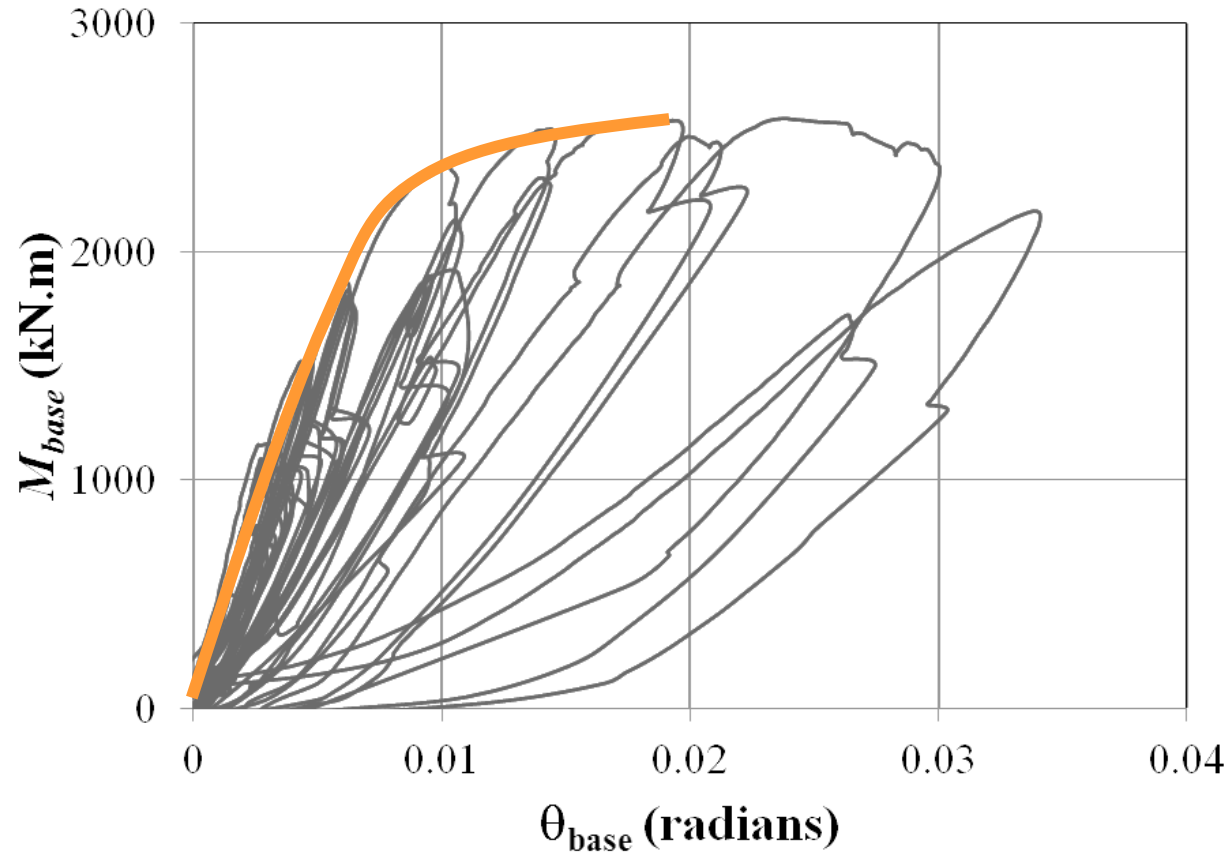
# Improved models for embedded bases



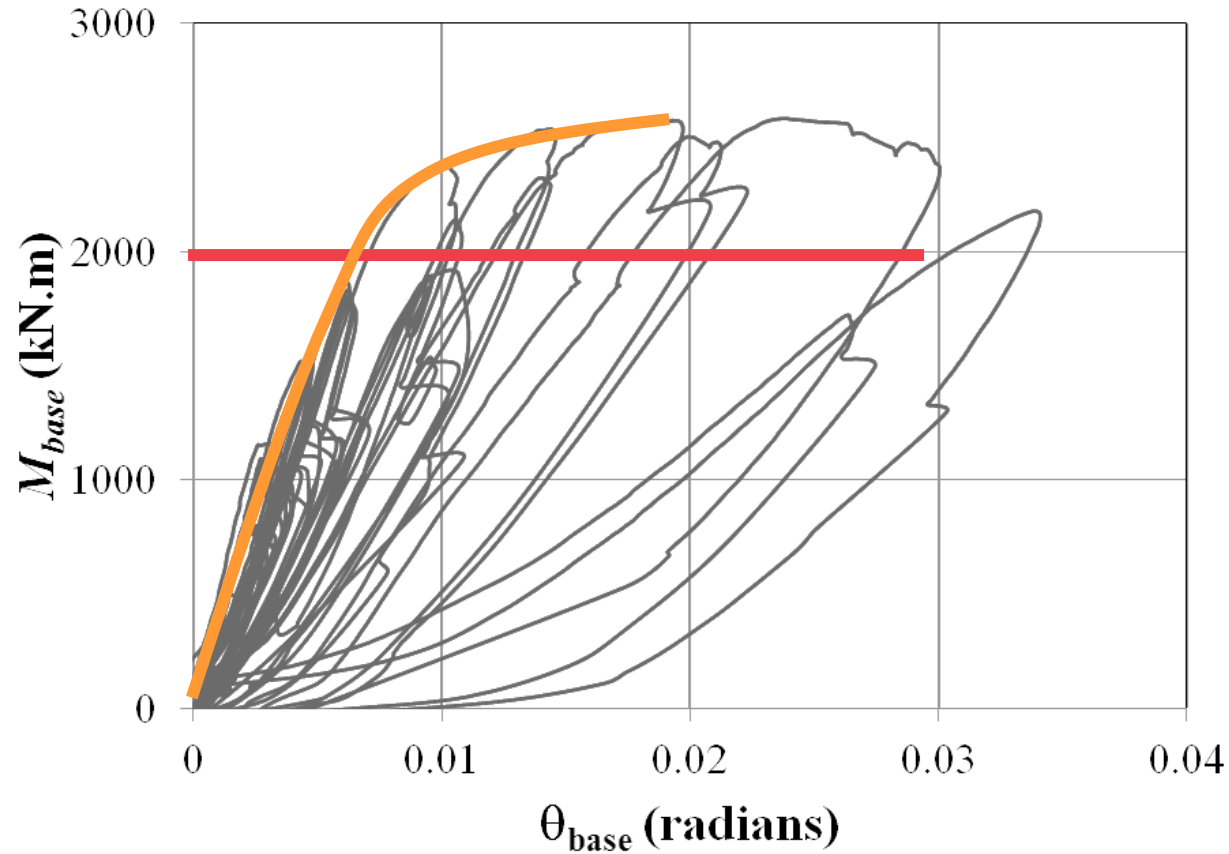
# Rotational stiffness of embedded bases



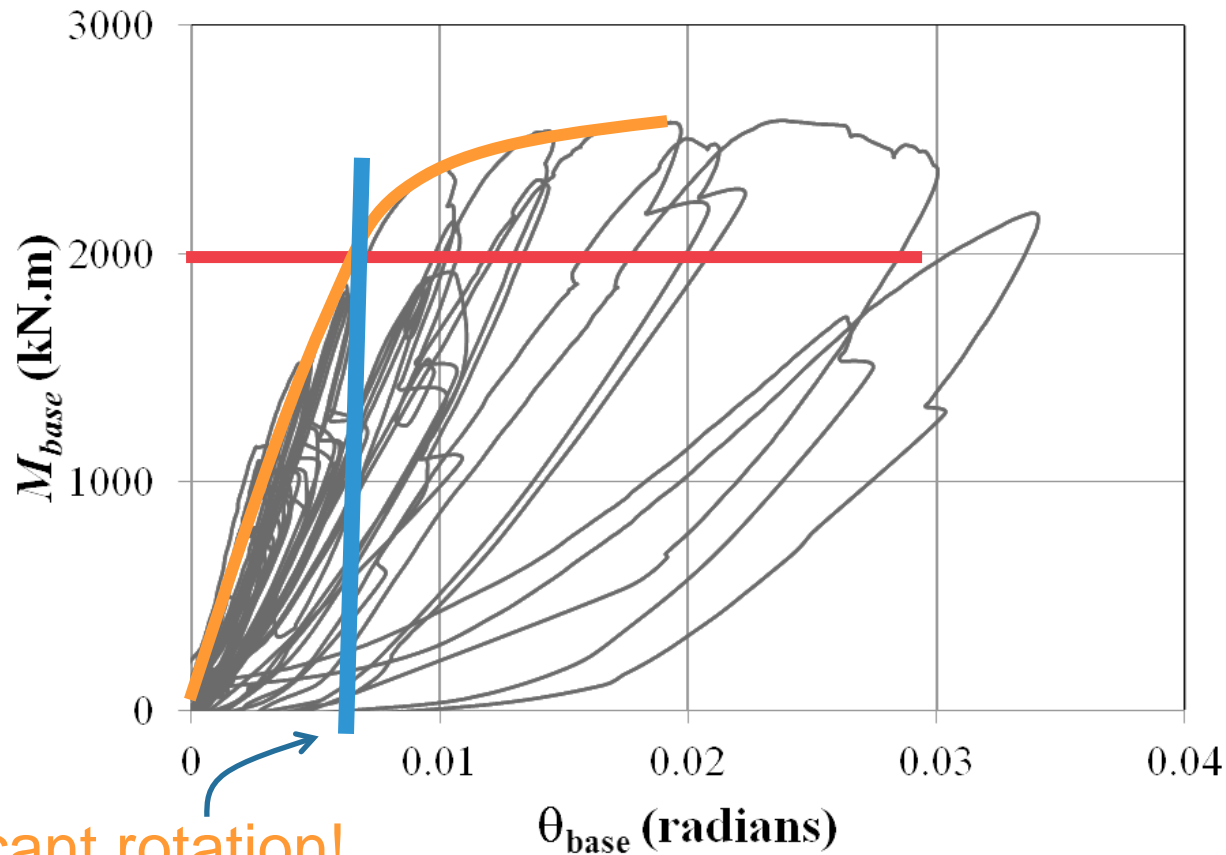
# Rotational stiffness of embedded bases



# Rotational stiffness of embedded bases



# Rotational stiffness of embedded bases



Significant rotation!

# Summary– embedded base connections

- Knowledge almost entirely new
- Existing methods do not fully capture complexity and mechanisms
- New test data has led to improved methods
- Rotational flexibility is an issue

# Organization

## Part 1

Exposed  
Base Plates

Prevailing  
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Developments

## Part 3

A look to the  
future

“Resolved”  
issues

Ongoing work  
Unresolved  
issues



# A look to the future

## Part 3

A look to the  
future

```
graph TD; A[A look to the future] --- B["Resolved issues"]; A --- C["Ongoing work Unresolved issues"]
```

“Resolved”  
issues

Ongoing work  
Unresolved  
issues

# A look to the future

## Part 3

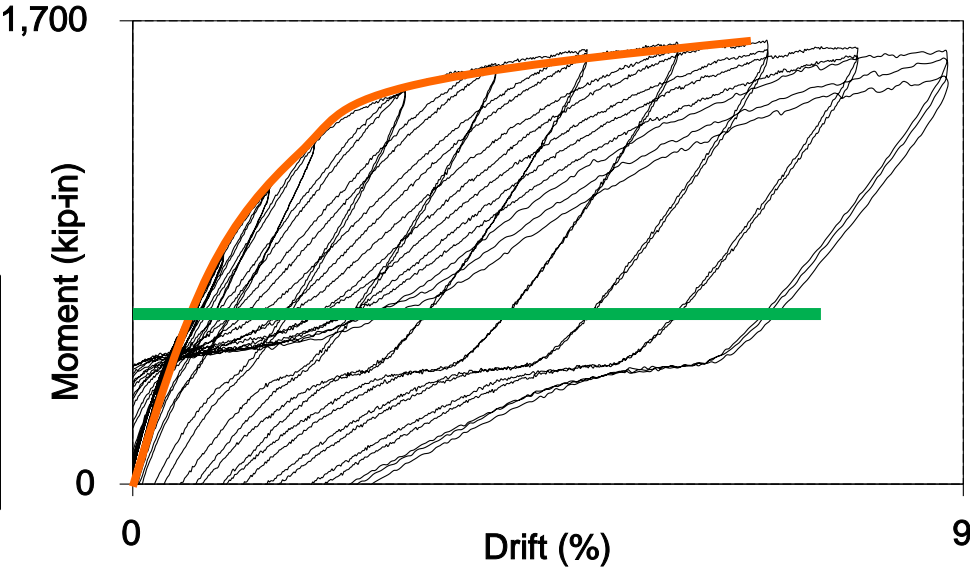
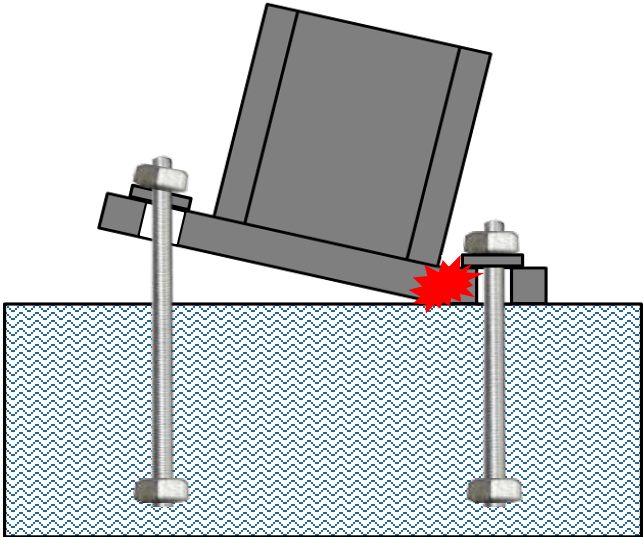
### A look to the future

“Resolved”  
issues

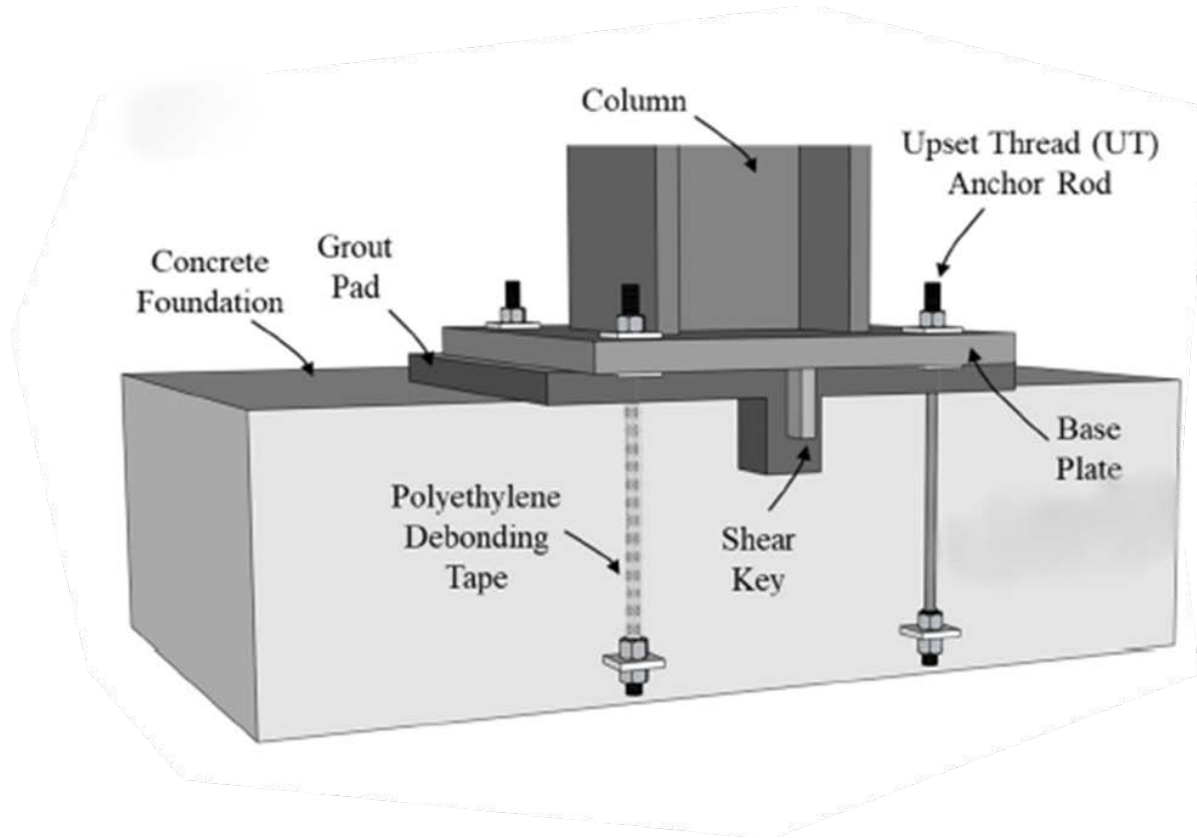
Ongoing work  
Unresolved  
issues

- Minor modifications to strength model
- Ductile details for weak base design
  - Reliability analysis
  - Biaxial bending
  - Anchorages
  - Shear transfer
- Alternate anchor rod patterns
  - Modeling tools
- Strength models for embedded details
  - Effect of slab overtopping

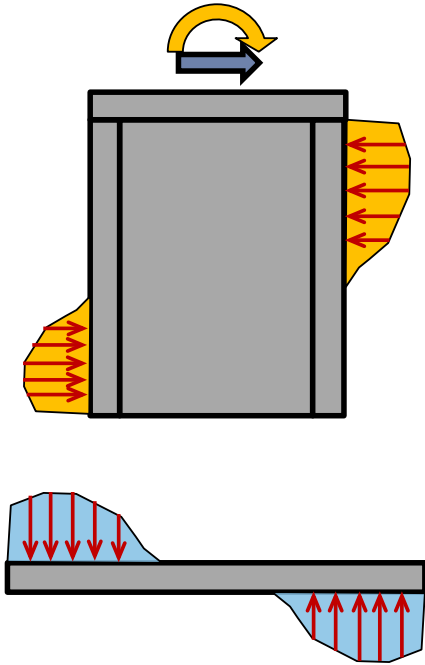
# Modifications to strength models to reduce conservatism



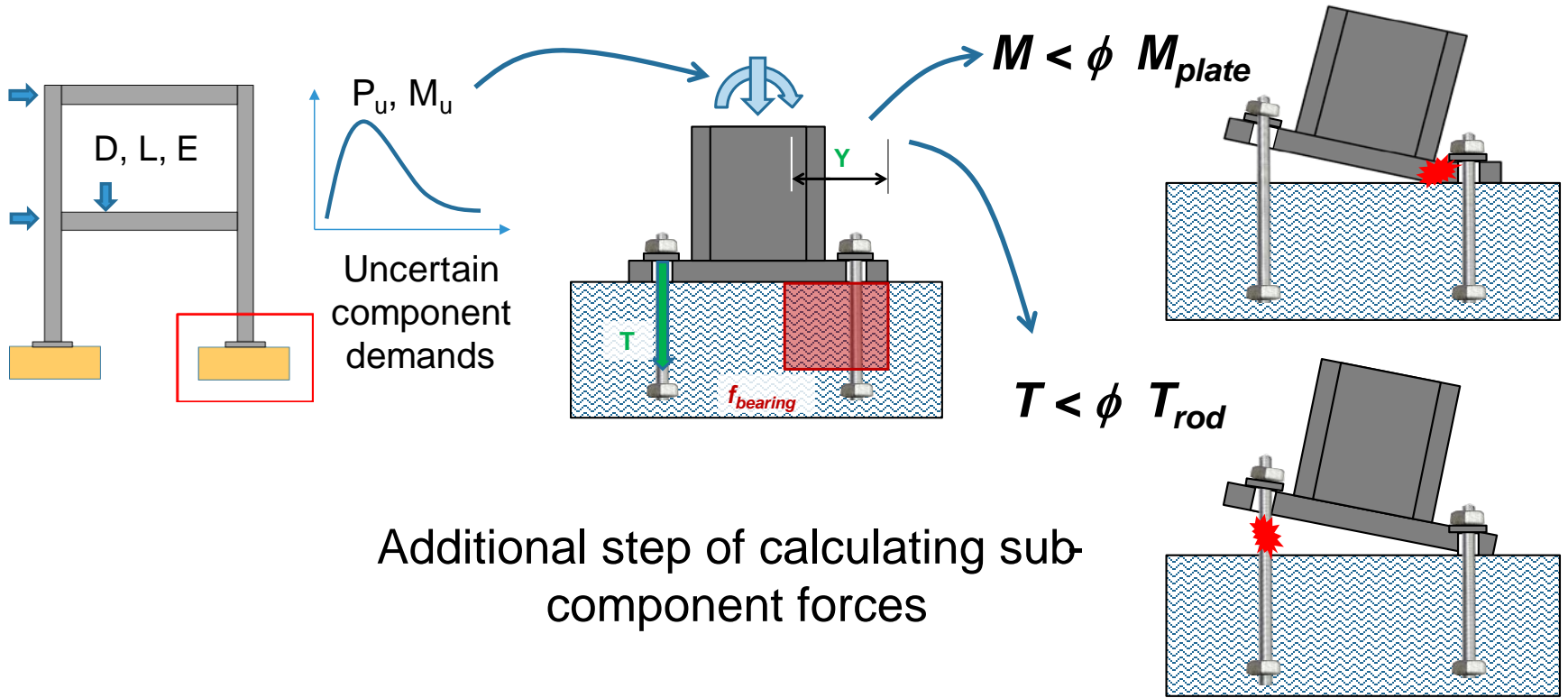
# Ductile details for weak base design



# Embedded bases— new strength models



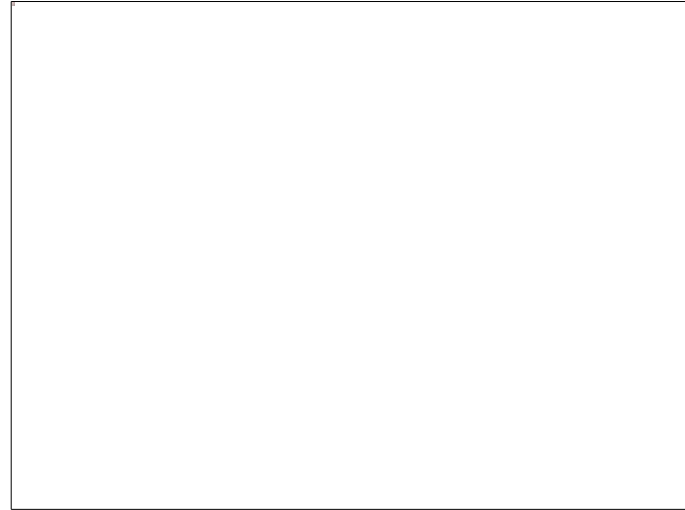
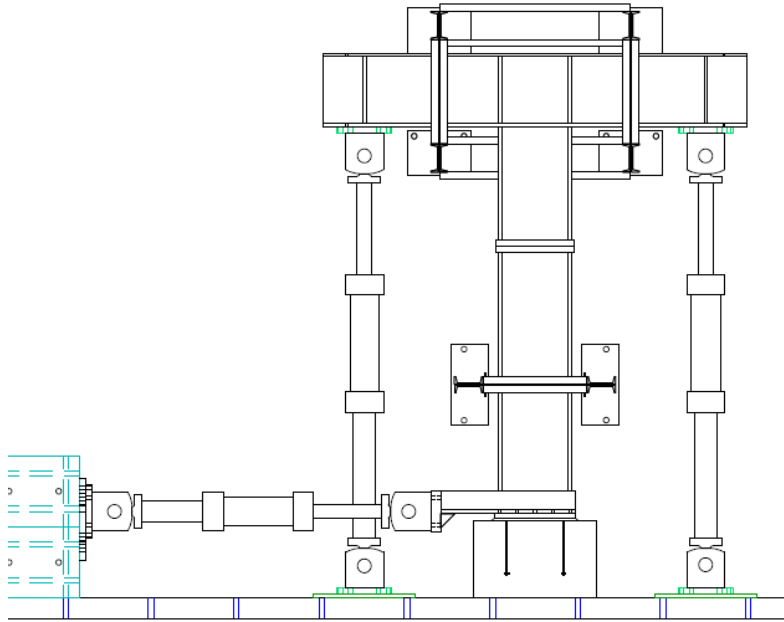
# Reliability analysis



Additional step of calculating sub-component forces



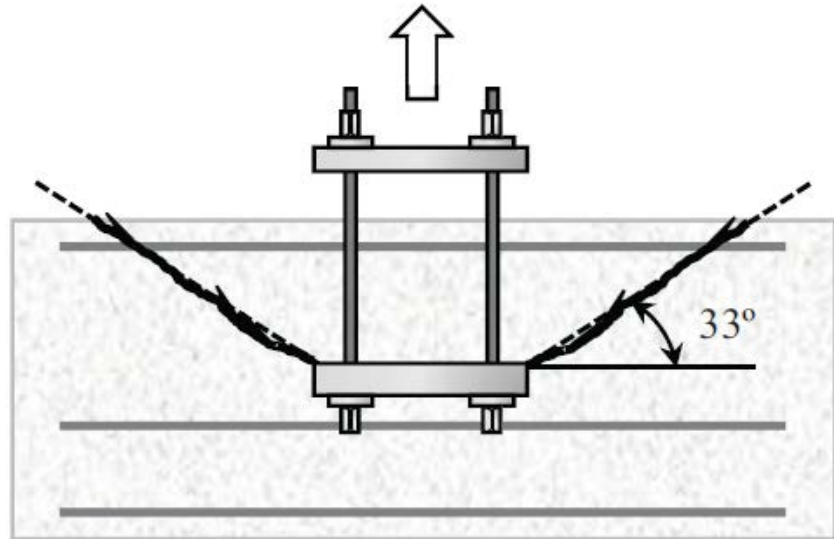
# Shear transfer



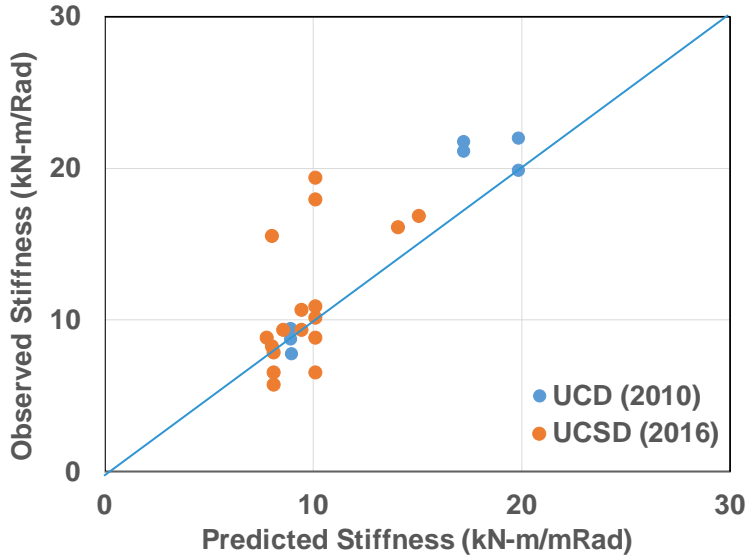
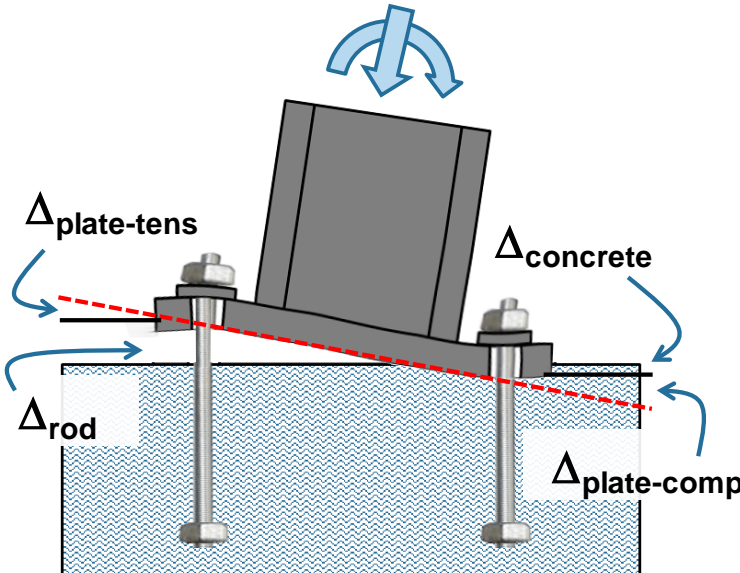


# Strength of anchorages

Differences between concrete and steel column bases

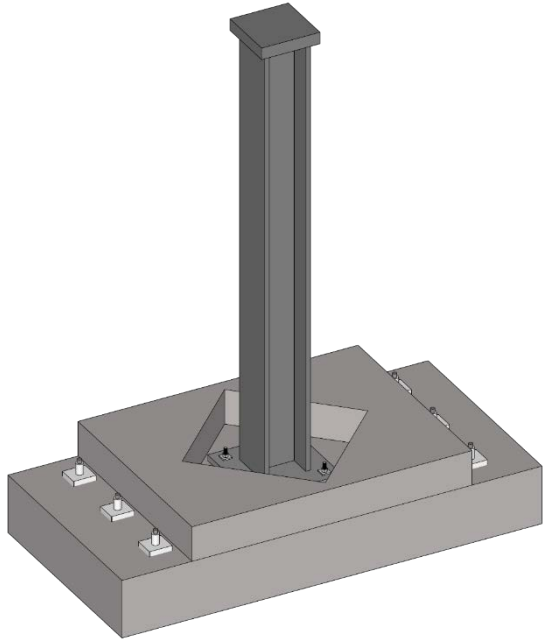


# Models for base flexibility – exposed and embedded

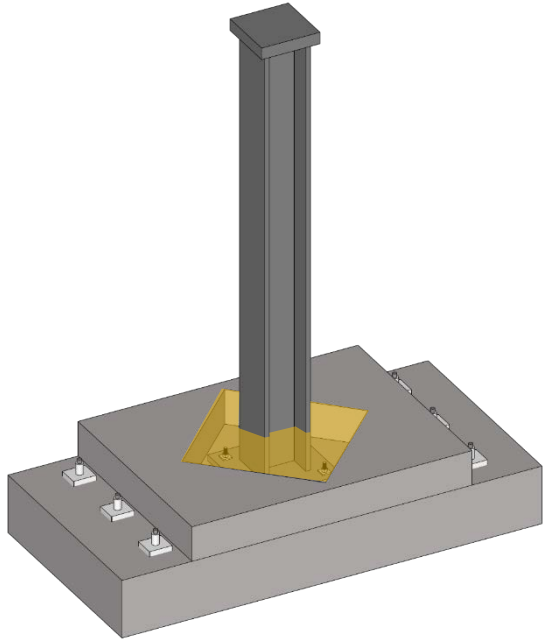


Kanvinde, A.M., Grilli, D.A., and Zareian, F (2012). "Rotational Stiffness of Exposed Column Base Connections – Experiments and Analytical Models," Journal of Structural Engineering, ASCE, 138(5), 549-560.

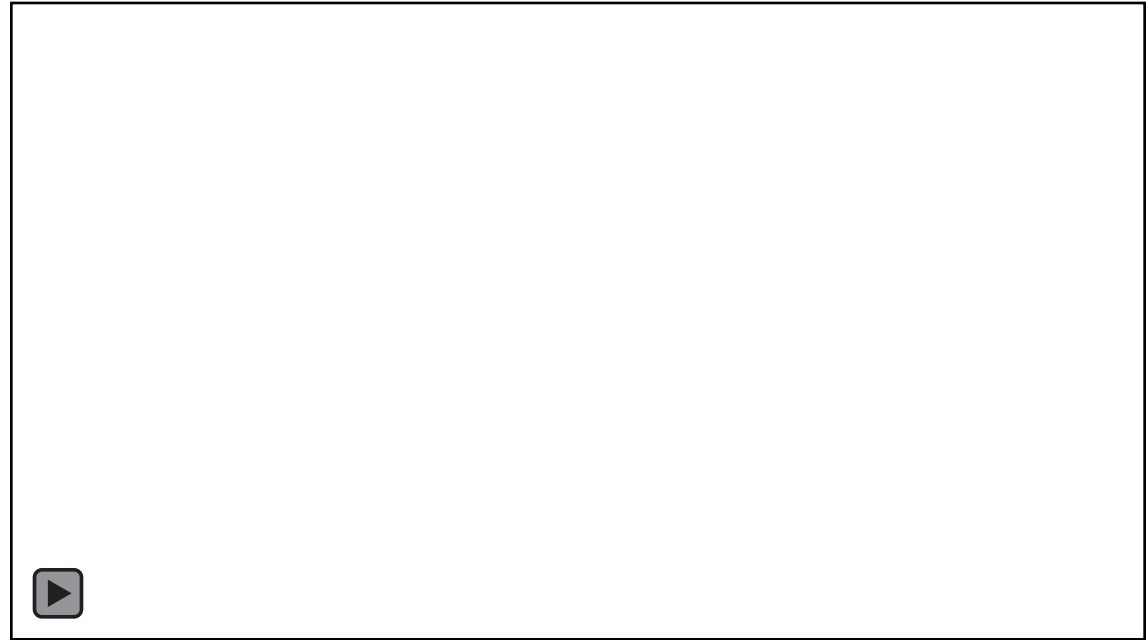
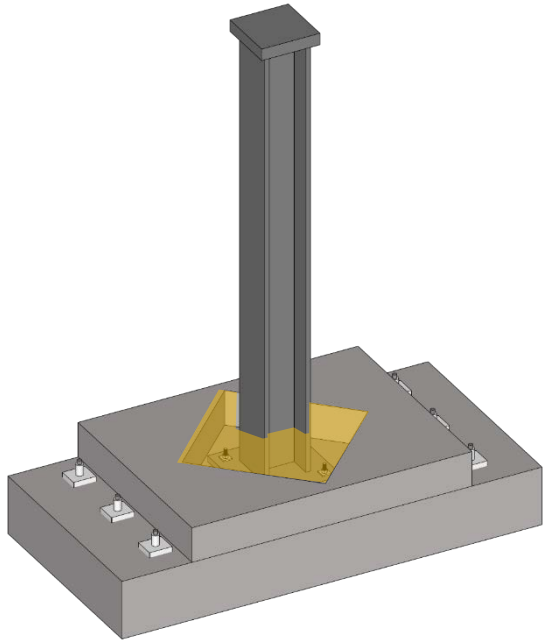
# Blockoutconnections and overtopping slab



# Blockoutconnections and overtopping slab

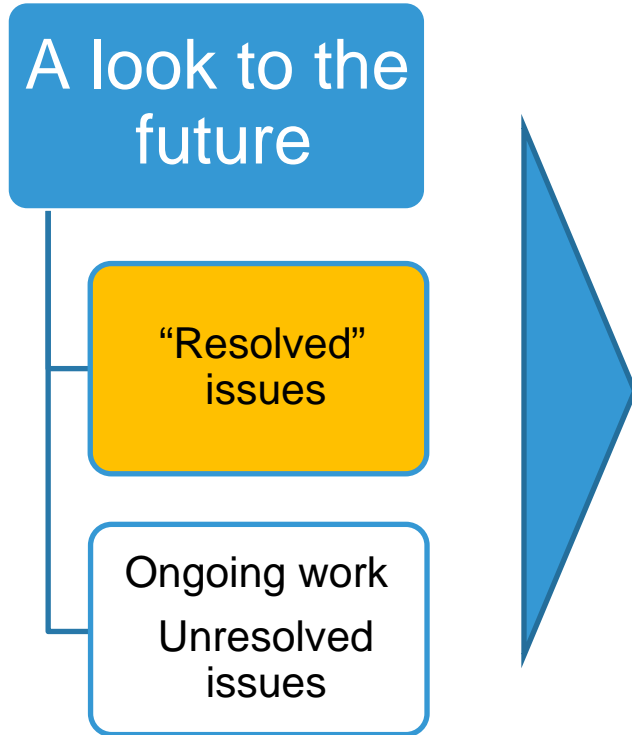


# Blockoutconnections and overtopping slab



Work done at BYU (Paul Richards) and UC Davis

# Potential proposals



- New (3<sup>rd</sup>) Edition of Design Guide One (~2024) – in progress
- AISC 341 – Next code cycle
- Seismic Design Manual

# AISC Design Guide One 3<sup>rd</sup> Ed

Amit Kanvinde, Mahmoud Maamouri, Josh Buckholt

- New chapter on embedded connections
- Detailed consideration of seismic issues (including weak base design)
- Configurations not addressed currently (rod patterns, biaxial bending)
- Stiffness models
- Guidelines for computer analysis
- Alternate methods of design to remove conservatisms
- Web tools for strength and stiffness models!

# A look to the future

## A look to the future

“Resolved”  
issues

Ongoing work  
Unresolved  
issues

- Braced frame base plates
- Overall foundation response and soil structure interaction
  - Base frame interactions
  - Resilience, design for repair



# Braced frame base plates

A look to the future

“Resolved”  
issues

Ongoing work  
Unresolved  
issues

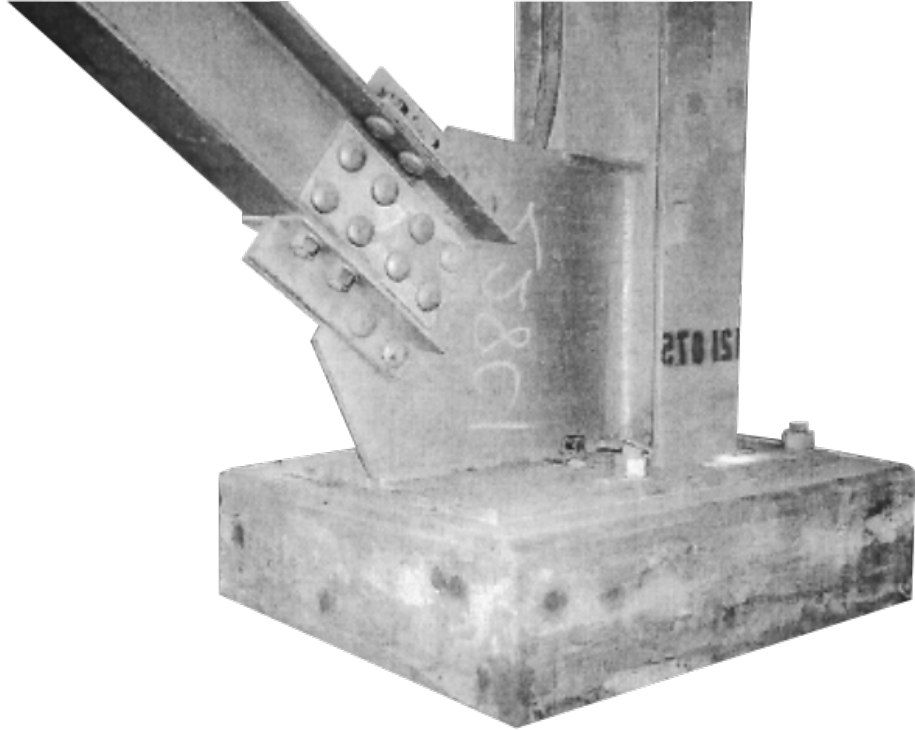


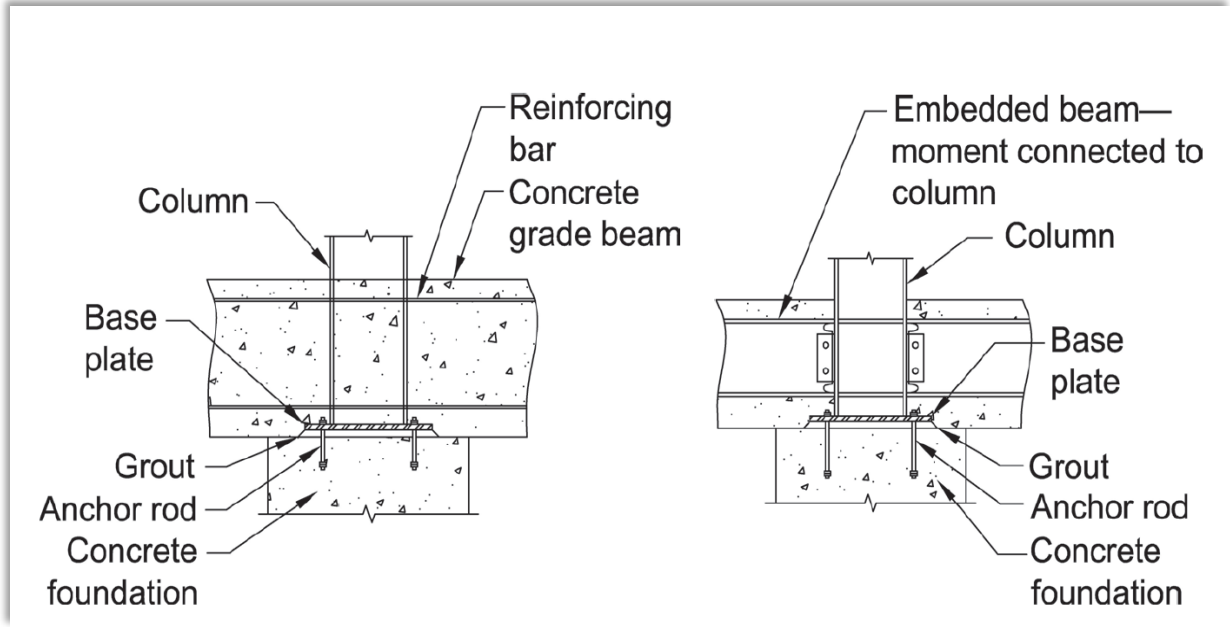
Photo credit: Rick Drake (2003)

# Overall foundation response

A look to the future

“Resolved” issues

Ongoing work  
Unresolved issues



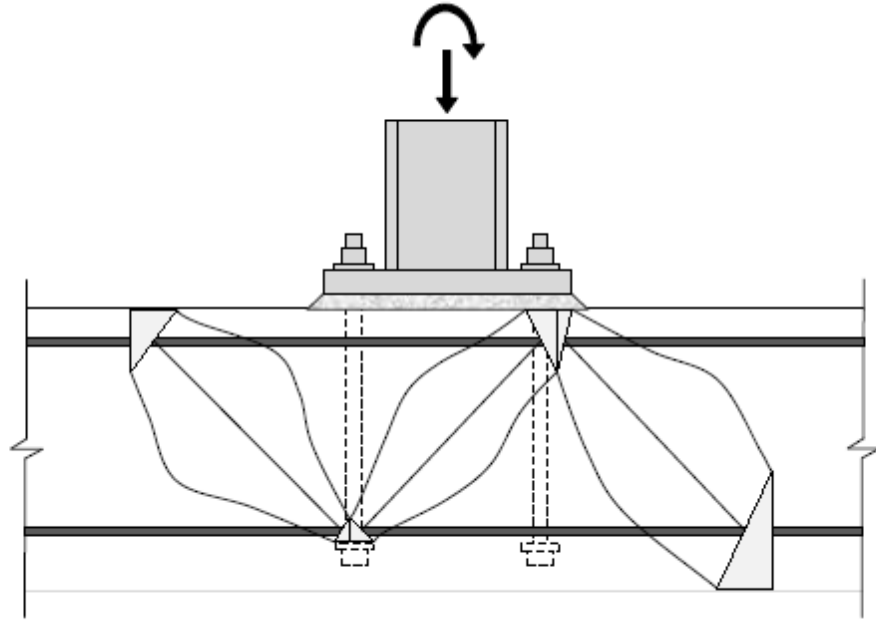
Grade beams

# Overall foundation response

A look to the future

“Resolved”  
issues

Ongoing work  
Unresolved  
issues



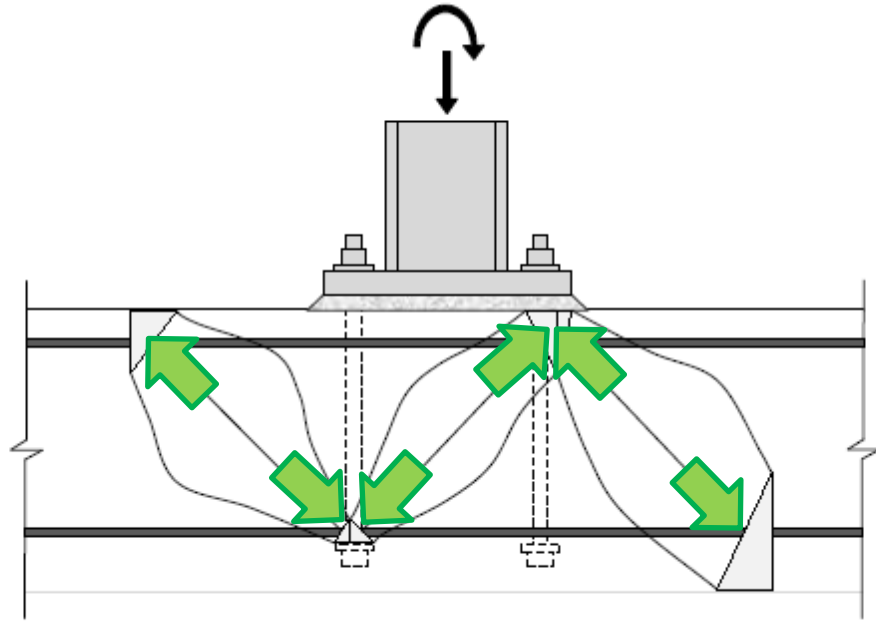
Grade beams and overall  
foundation response

# Overall foundation response

A look to the future

“Resolved”  
issues

Ongoing work  
Unresolved  
issues



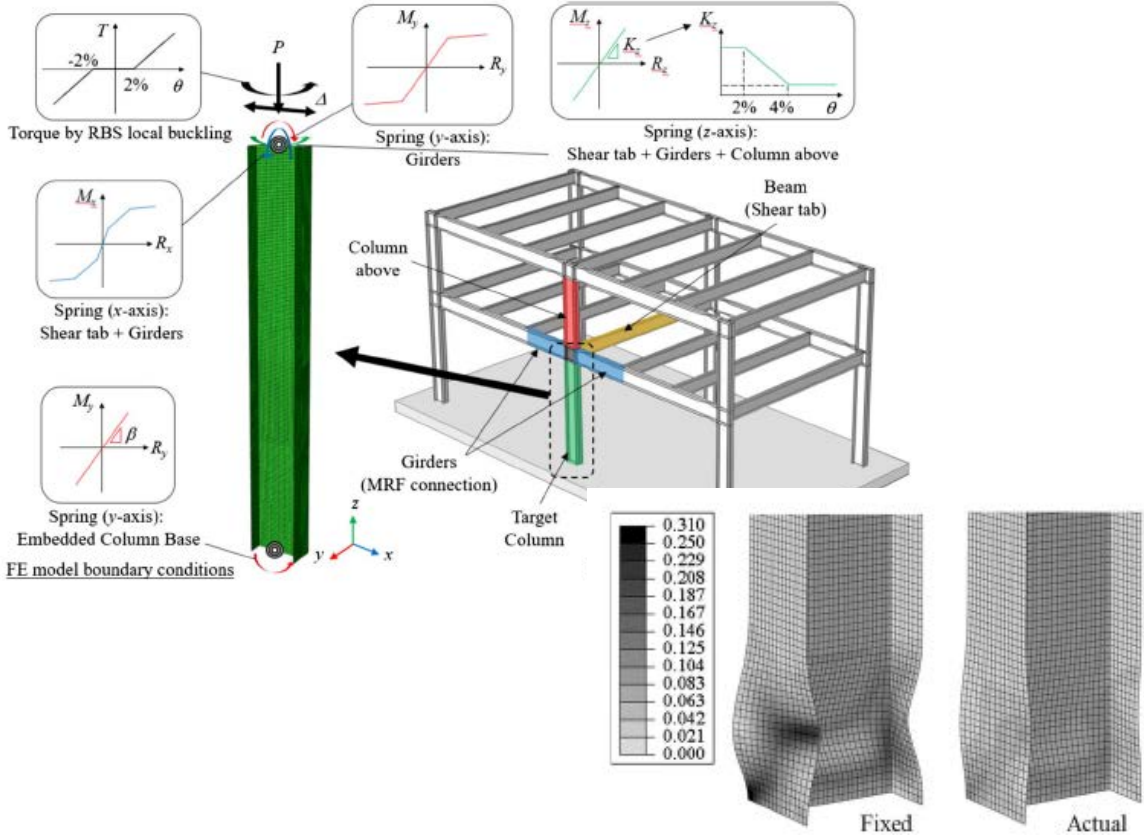
...all the way to soil structure  
interaction

# Base frame interactions

A look to the future

“Resolved” issues

Ongoing work  
Unresolved issues



Inamasu, I., Kanvinde, A.M., and Lignos D., (2019). “Seismic Stability of Wide Flange Steel Columns Interacting with Embedded Column Base Connections,” Journal of Structural Engineering, American Society of Civil Engineers, 145 (12), 04019151.

# Still an exciting area with many opportunities

A look to the future

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graph TD; A[A look to the future] --- B["Resolved issues"]; A --- C["Ongoing work Unresolved issues"]
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“Resolved”  
issues

Ongoing work  
Unresolved  
issues

- Resilience and remaining life
- Design to minimize damage
- Design for repair

**UCDAVIS**

**CIVIL AND ENVIRONMENTAL  
ENGINEERING**

Thank you!

<https://faculty.engineering.ucdavis.edu/kanvinde/>